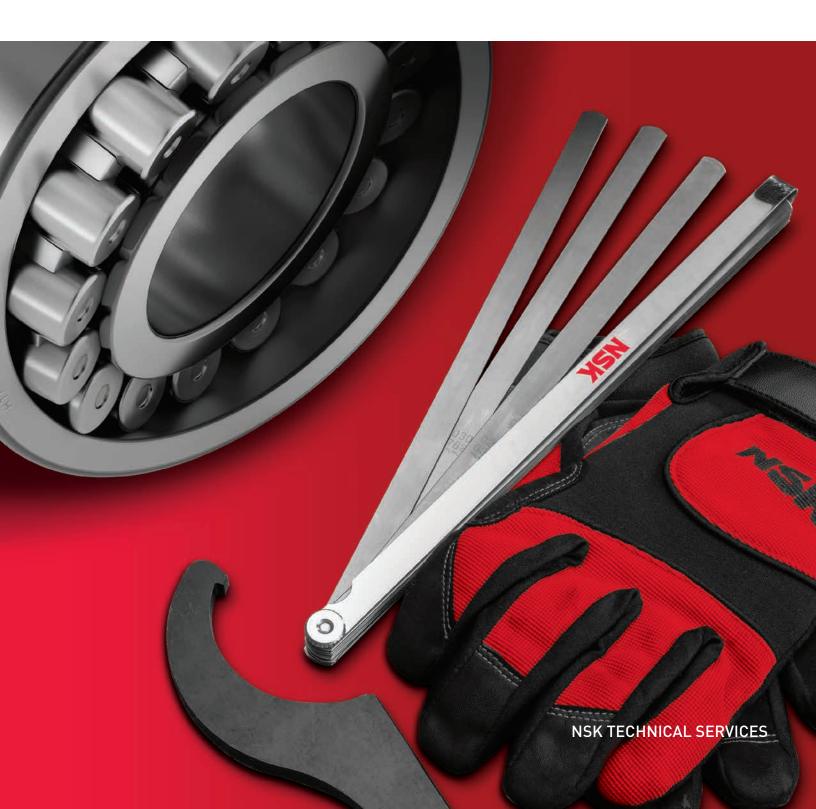


BEARING MAINTENANCE GUIDE

MOUNTING AND HANDLING PRACTICES FOR OPERATIONAL RELIABILITY





BEARING MAINTENANCE GUIDE

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A GLOBAL PARTNER AND SOLUTIONS PROVIDER

As a leading manufacturer of rolling bearings and linear technology components, NSK can be found on almost every continent – with production facilities, sales offices and technology centers – providing our customers with responsive design and decision-making, effective logistics and dedicated local service.

CONTENTS

- A BEARING TYPES AND CHARACTERISTICS
- **B** MOUNTING AND DISMOUNTING
- C SHAFT AND HOUSING FITS
- **D** LUBRICATION
- **E** TROUBLESHOOTING / BEARING DAMAGE
- F MAINTENANCE TOOLS / TECHNICAL SUPPORT

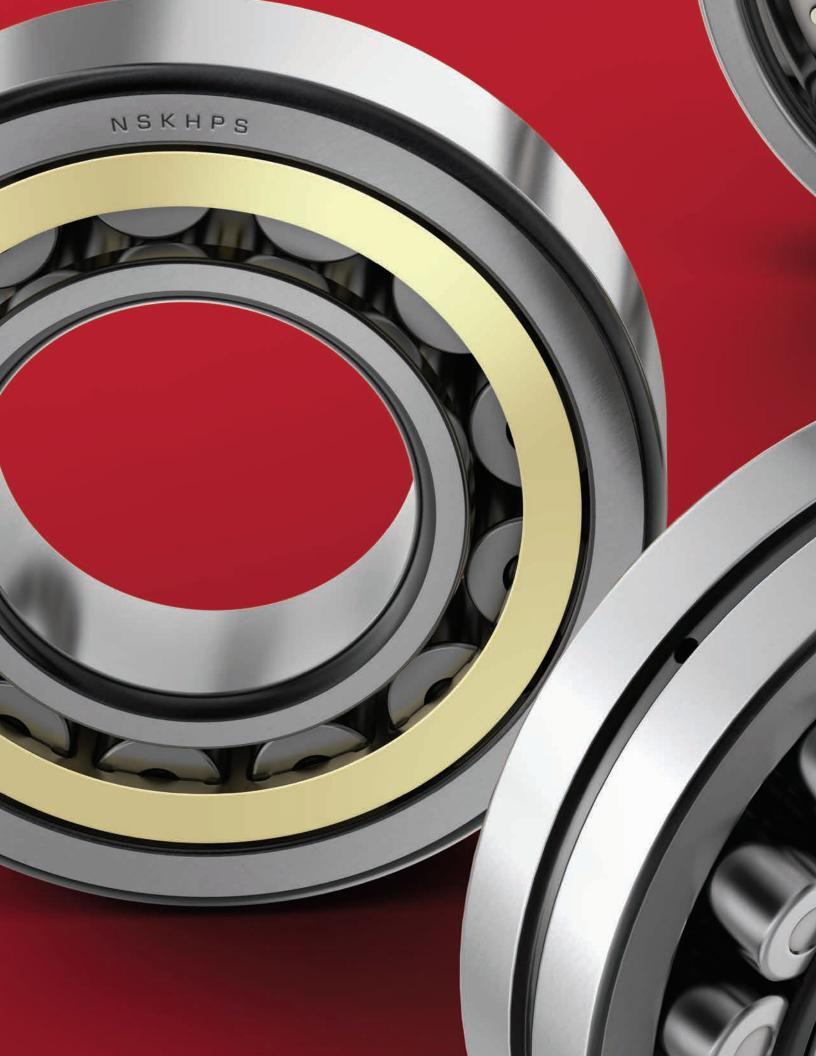




THE NSK COMPANY

NSK commenced operations as the first Japanese manufacturer of rolling bearings in 1916. From the outset, we have been continuously expanding and improving not only our product portfolio but also our range of services for various industrial sectors. In this context, we develop technologies in the fields of rolling bearings, linear systems, components for the automotive industry and mechatronic systems. Our research and production facilities in the Americas, Europe, and Asia are linked together in a global technology network. Here we concentrate not only on the development of new technologies, but also on the continuous optimization of quality – at every process stage.

At the core of our research activities is the development of advanced material and lubricant technologies, simulation applications using a variety of analytical systems, and technological innovation in the field of mechatronics.





SECTION A:

BEARING TYPES AND CHARACTERISTICS

NSKHPS



COMMON BEARING TYPES AND COMPONENTS



Deep groove ball bearing, sealed

Angular contact ball bearing, single row Thrust ball bearing, single direction

ROLLING BEARING DESIGN AND CLASSIFICATION

Rolling bearings generally consist of two rings, rolling elements, and a cage, and they are classified into radial bearings or thrust bearings depending on the direction of the main load. In addition, depending on the type of rolling elements, they are classified into ball bearings or roller bearings, and they are further segregated by differences in their design or specific purpose.

A selection of representative bearing types and naming of components is shown above. A general classification of ball and roller bearing types available from NSK and an overview of their operating characteristics can be found on the pages that follow.

1	inner ring
2	seal (similarly shield)
3	outer ring
4	ball
5	cage
6	inner ring front face
7	outer ring back face
8	outer ring front face





Cylindrical roller bearing, single row

Spherical roller bearing

Tapered roller bearing, single row

9	inner ring back face
10	shaft washer
11	housing washer
12	aligning seat washer
13	inner ring flange
14	outer ring flange
15	outer ring raceway
16	cylindrical roller

17	inner ring raceway
18	spherical roller
19	lubrication feature - groove, holes
20	cone front face flange
21	cup
22	tapered roller
23	cone back face flange
24	cone

ROLLING BEARING TYPES AND CHARACTERISTICS

		DEEP GROO	VE BALL BEARIN	GS	ANGULAR CO	ONTACT BALL B	EARINGS		SELF-	THRUST BAL	L BEARINGS	
BEARING TY	PE	Single row	Magneto	Double row	Single row	Double row	Duplex	Four-point	ALIGNING BALL BEARINGS	with flat seat	with aligning seat	Double direction thrust
CHARACTER	ISTICS											
	Radial	fair	poor	good	good	good	good	poor	fair	not possible	not possible	not possible
Load Capacity	Axial	fair - two directions	poor - one direction only	fair - two directions	good - one direction only	good - two directions	good - two directions	good - two directions	poor - two directions	good - one direction only	good - one direction only	good - two directions
	Combined	fair	poor	fair	good	good	good	fair	poor	not possible	not possible	not possible
High Speed	s	excellent	good	fair	excellent	fair	good	good	good	not possible	not possible	fair
High Accura	ю	excellent			excellent		excellent	good		good		excellent
Rigidity							good					good
Angular Mis	salignment	good	poor	poor	poor	poor	poor	poor	excellent	not possible	excellent	not possible
Self-alignin	g Capability											
Ring Separa	ability									•		
Fixed-end E	Bearing	•				•	•		•			
Free-end Be	earing	\bigcirc				\bigcirc	\bigcirc	\bigcirc	\bigcirc			
Tapered Bo	re Option											
Remarks			Two bearings are usually mounted in opposition		Contact angles of 15, 25, 30 and 40° Two bearings are usually mounted in opposition Clearance adjustment is necessary	Contact angles of 25, 30 and 32°	DF and DT combinations cannot be used as free-end bearings	Contact angle of 35°				



SPHERICAL	CYLINDRICA	L ROLLER BEARI	NGS		TAPERED RO	LLER BEARINGS	NEEDLE	THRUST ROL	LER BEARINGS			
ROLLER BEARINGS	Single Row	with inner ring rib	with thrust collar	Double Row	Single Row	Double / multi-row	ROLLER BEARINGS	Spherical	Cylindrical	Tapered	BEARING TYF	E
											CHARACTERI	STICS
excellent	good	good	good	excellent	good	excellent	good	poor	not possible	not possible	Radial	
fair - two directions	not possible	fair - one direction only	fair - two directions	not possible	good - one direction only	good - two directions	not possible	excellent - one direction only	excellent - one direction only	excellent - one direction only	Axial	Load Capacity
good	not possible	fair	fair	not possible	good	excellent	not possible	poor	not possible	not possible	Combined	
fair	excellent	good	good	good	fair	fair	good	poor	poor	poor	High Speeds	
	excellent			excellent	good						High Accura	cy
	good	good	good	excellent	good	excellent	good		excellent	excellent	Rigidity	
excellent	fair	fair	fair	poor	fair	poor	poor	excellent	not possible	not possible	Angular Mis	alignment
•								•			Self-aligning) Capability
	•					٠					Ring Separa	bility
•			•			•					Fixed-end B	earing
\bigcirc	•					\bigcirc					Free-end Be	aring
											Tapered Bor	e Option
	Inclusive of NU and N types	Inclusive of NJ and NF types	Inclusive of NH and NUP types	Inclusive of NN and NNU types	Two bearings are usually mounted in opposition Clearance adjustment is necessary	KH and KV types cannot be used as free-end bearings			Including needle roller thrust bearings		Remarks	

applicable
 opplicable, but it is necessary to allow shaft contraction / elongation at fitting surfaces

COMMON BEARING TYPES AND COMPONENTS

LOAD CAPACITY AND BEARING TYPES

Depending upon the application, rolling bearings may be subjected to the various types of loads listed below:

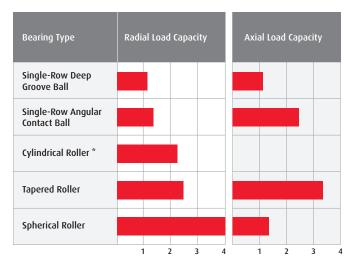
- › Radial load
- › Axial load
- Combined radial and axial loads
- › Moment loads

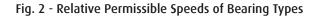
When considering bearing selection, it is critical that the bearing type possesses performance characteristics suited to the type and magnitude of the load. The axial load carrying capacity of a bearing is closely related to the radial load capacity in a manner that depends on the bearing type as shown in **Figure 1**. When bearings of the same dimension series are compared, roller bearings have a higher load capacity than ball bearings and are superior if shock loads exist.

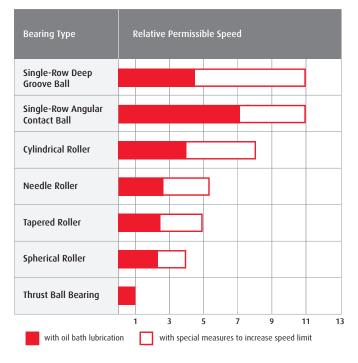
PERMISSIBLE SPEED AND BEARING TYPES

The maximum speed of rolling bearings varies depending, not only the type of bearing, but also its size, type of cage, loads, lubricating method, heat dissipation, etc. Using the assumption of employing a common oil bath lubrication method, the relative speed characteristics for common bearing types are approximately ranked in **Figure 2**.

Fig. 1 - Relative Load Capacities of Bearing Types









MISALIGNMENT OF INNER/OUTER RINGS

Because of deflection of a shaft caused by applied loads, dimensional error of the shaft and housing, and mounting errors, the inner and outer rings are slightly misaligned. The permissible misalignment varies depending on the bearing type and operating conditions, but usually it is a small angle less than 0.0012 radian (4 minutes). When the misalignment is expected to be greater than this value, bearings having a self-aligning capability, such as self-aligning ball bearings, spherical roller bearings, and certain bearing units, should be selected.

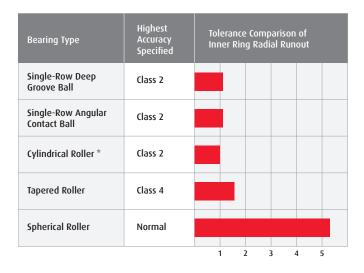
RIGIDITY

When loads are imposed on a rolling bearing, some elastic deformation occurs in the contact areas between the rolling elements and raceways. The rigidity of the bearing is determined by the ratio of bearing load to the amount of elastic deformation of the inner and outer rings and rolling elements. Consequently, since roller bearings are deformed less by load, they are more often selected than ball bearings. When extra high rigidity is required, bearings are given a preload, which means that they have a negative clearance. Angular contact ball bearings and tapered roller bearings are sometimes preloaded.

NOISE AND TORQUE

Since rolling bearings are manufactured with very high precision, noise and torque are minimal. For deep groove ball bearings and cylindrical roller bearings particularly, the noise level is sometimes specified depending on their purpose. For high precision miniature ball bearings, the starting torque is specified. Deep groove ball bearings are typically recommended for applications in which low noise and torque are required, such as motors and instruments.

Fig. 3 - Relative Inner Ring Radial Runout of Highest Accuracy Class of Bearing Types



RUNNING ACCURACY AND BEARING TYPES

The running accuracy of rolling bearings is specified in various ways, and the specified accuracy classes vary depending on the bearing type. For applications that require high running accuracy or high speeds, high precision bearings of Class 5, 4 or 2 are used. For comparison purposes, inner ring radial runout for the highest running accuracy specified for common bearing types is shown in **Figure 3**. Deep groove and angular contact ball bearings and cylindrical roller bearings are most suitable for applications requiring high running accuracy.

BALL BEARING TYPES



DEEP GROOVE BALL BEARINGS

Single Row (4.1)

- > open, with contact seals, non-contact seals, shields
- > with a snap ring groove, with or without a snap ring

Max Type with filling slot (4.2)

> open, with shields

Magneto type (4.3)

Creep-Free[™] type (4.4)

> open, with contact seals, shields

Double Row

ANGULAR CONTACT BALL BEARINGS

Single Row (4.5)

- > for single mounting or universal matching
- > with 15°, 25°, 30° or 40° contact angle

Single Row, high precision

- > for single mounting or universal matching
- in duplex, triplex and quadruplex sets (4.6)
- > with non-contact seal (4.7)
- > with 15°, 25° or 30° contact angle

Single Row Ultra High-Speed, high precision

- > for single mounting or universal matching
- > in duplex, triplex and quadruplex sets
- > with non-contact seal
- > with 18° or 25° contact angle

Double Row (4.8)

- > open, with contact seals, non-contact seals, shields
- > with a snap ring groove, with or without a snap ring
- > with 25° or 32° contact angle

Four-Point contact (4.9)



SELF-ALIGNING BALL BEARINGS

- > with a cylindrical or tapered bore (4.10)
- > open, with contact seals
- > with an extended inner ring

THRUST BALL BEARINGS

Single Direction

- > with flat seat (4.11)
- with aligning seat, with or without aligning seat washer (4.12)

Double Direction

- > with flat seat (4.13)
- with aligning seat, with or without aligning seat washer (4.14)

ANGULAR CONTACT THRUST BALL BEARINGS

Single Row (Direction), high precision (4.15)

- > for single mounting or universal matching
- > in duplex, triplex and quadruplex sets
- > with 30° or 40° contact angle

Single Direction, high precision (4.16)

- > for universal matching
- > with 50° contact angle

Double Direction, high precision (4.17)

> with 60° contact angle

ANGULAR CONTACT BALL SCREW SUPPORT BEARINGS

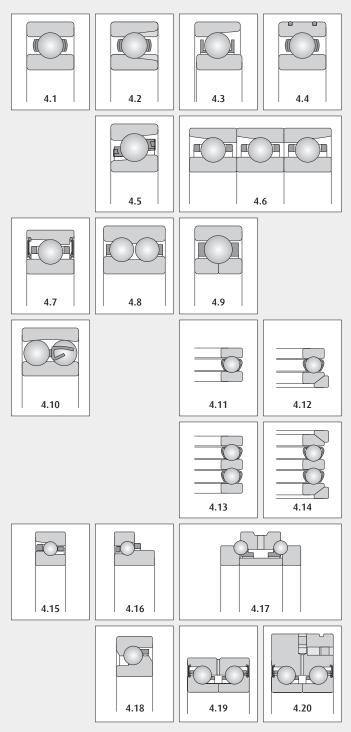
Single Row, high precision (4.18)

- > for single mounting or universal matching
- > open, with contact seals
- > with 60° contact angle

Double Row, high precision

- > for single mounting or universal matching
- > with contact seals
- > for housing (4.19) or direct face-mounting (4.20)
- > with 60° contact angle

Fig. 4 - Ball Bearing Types



ROLLER BEARING TYPES



SPHERICAL ROLLER BEARINGS

Open type (5.1)

> with cylindrical or tapered bore

With integral contact seal (5.2)

> with cylindrical or tapered bore

With removable seal (5.3)

> with cylindrical or tapered bore

CYLINDRICAL ROLLER BEARINGS

Single Row

- > NU type no flange on inner ring (5.4)
- > NJ type one flange on inner ring (5.5)
- > N type no flange on outer ring (5.6)
- > NF type one flange on outer ring (5.7)
- > NUP type one flange on inner ring + locating ring (5.8)
- > NH type one flange on inner ring + thrust collar (5.9)

CYLINDRICAL ROLLER BEARINGS

Double Row, cylindrical or tapered bore

- > NNU type no flange on inner ring (5.10)
- > NN type no flange on outer ring (5.11)

Four-Row (5.12)

- > with cylindrical or tapered bore
- with or without inner / outer ring flanges

FULL COMPLEMENT CYLINDRICAL ROLLER BEARINGS

Single Row

> NCF type - flanges on inner ring + retaining ring (5.13)

Double Row

- > NNCF type flanges on inner ring + retaining ring (5.14)
- crane sheave type corrosion resistant, lubricating features, closures and snap rings



NEEDLE ROLLER BEARINGS DRAWN CUP NEEDLE ROLLER BEARINGS (5.15)

- solid needle roller bearings (5.16)
- > cage and roller assemblies (5.17)
- thrust needle roller bearings
- > cam followers
- > roller followers (5.18)
- > components

TAPERED ROLLER BEARINGS

Single Row (5.19)

> for single mounting or duplex arrangement

Double Row

- > double cup / single cone TDO configuration (5.20)
- > double cone / single cup TDI configuration
- > with normal or steep angle

Four Row

- > KV type TQO configuration
- > KVE / KVS type KV sealed-clean design (5.21)

ROLLER THRUST BEARINGS

Spherical Roller Thrust Bearings (5.22)

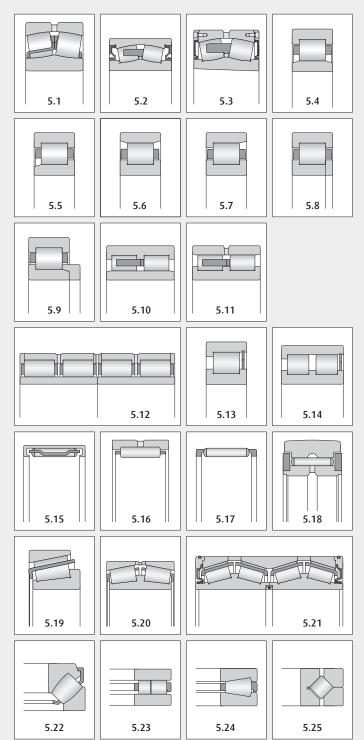
- single direction
- Cylindrical Roller Thrust Bearings (5.23)
- single direction

Tapered Roller Thrust Bearings

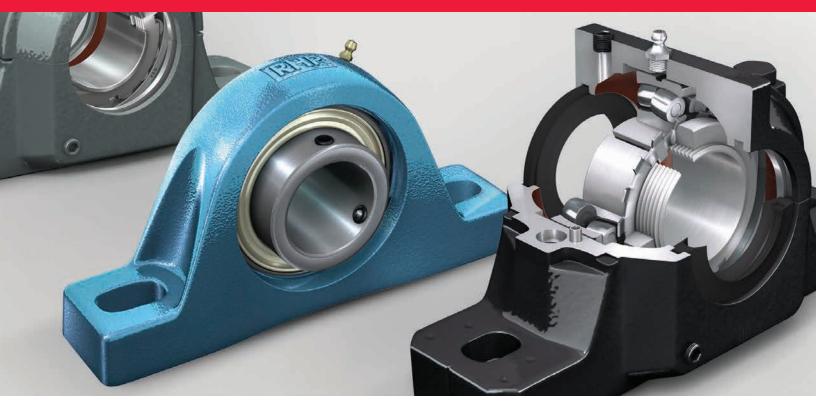
- > single direction (5.24)
- > double direction

CROSSED ROLLER BEARINGS (5.25)

Fig. 5 - Roller Bearing Types



PILLOW BLOCKS AND BEARING UNITS



SPLIT PILLOW BLOCKS

SAF Series (6.1)

- > general duty
- > in cast iron, ductile iron and cast steel material
- > for self-aligning ball bearings or spherical roller bearings
- > with contact and non-contact triple seal rings, or special labyrinth seals for contaminated environments

SDAF Series (6.2)

- > heavy duty
- > in cast iron, ductile iron and cast steel material
- > for spherical roller bearings
- > with contact and non-contact triple seal rings, or special labyrinth seals for contaminated environments

SNN Series (6.3)

- > light to medium duty
- > in cast iron
- > for self-aligning ball bearings or spherical roller bearings
- > with contact and non-contact seal



BALL BEARING UNITS

Pillow Block Units, cast iron

- > normal base (6.4) *
- > short base (6.5)

Flange Units, cast iron

- four bolt, square type (6.6) *
- > four bolt, round type (6.7) *
- > three bolt *
- > two bolt (6.8, 6.9) *

Cartridge Units, cast iron (6.10, 6.11) Take-up Units, cast iron (6.12) Belt Tensioner Units, cast iron (6.13) Hanger Units, cast iron (6.14) Pillow Block Units, pressed steel (6.15) Flange Units, pressed steel

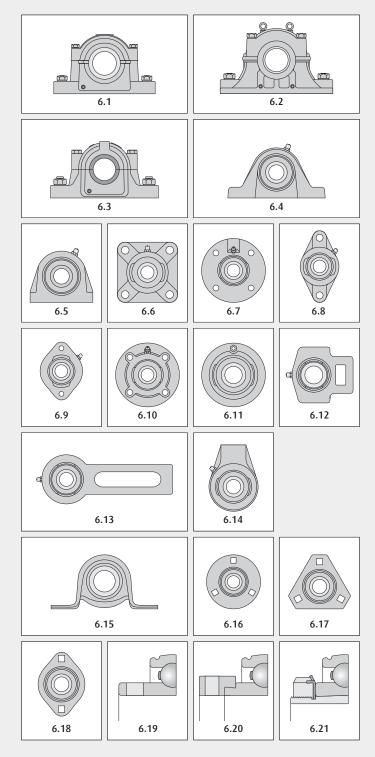
- > three bolt (6.16, 6.17)
- > two bolt (6.18)

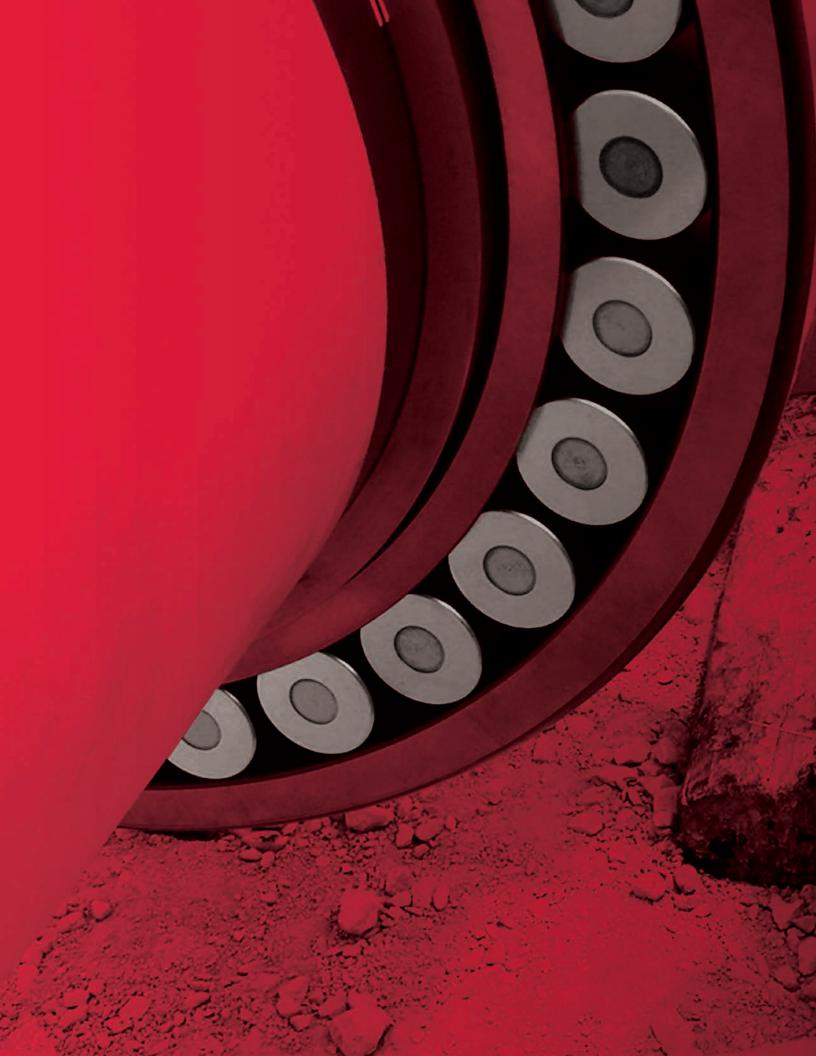
* also available in corrosion resistant stainless steel or thermoplastic

INSERT BEARINGS

- > with set screw lock (6.19)
- > with eccentric collar lock (6.20)
- with taper sleeve lock (6.21)
- > with single lip, flinger, triple lip seals

Fig. 6 - Pillow Blocks and Bearing Units







SECTION B:

MOUNTING AND DISMOUNTING



TH WITHDRAWAL SLEEVE	B29
Lock Nut Method	B29
Hydraulic Nut Method	B31

Oil Injection Method	B33
MOUNTING SPHERICAL ROLLER BEARINGS ON TAPERED SHAFTS	B35
Lock Nut Method	
Hydraulic Nut Method	B38
MOUNTING SELF-ALIGNING BALL BEARINGS	B39
MOUNTING PILLOW BLOCKS AND SEALS	B43
MOUNTING BALL BEARING UNITS	
METHODS OF DISMOUNTING	B49
CHECKING SHAFTS AND HOUSINGS	B51
CHECKING SLEEVES AND LOCK NUTS	
CHECKING DAMAGED BEARINGS	B54

MOUNTING ROLLING BEARINGS - GETTING STARTED

The approach to mounting rolling bearings warrants careful consideration as it significantly impacts their performance. Bearings are high precision components, regardless of size. To ensure optimal performance and long operating life, a high standard for handling and mounting every bearing is critical. This includes establishing a clean environment equipped with the correct tools and an understanding of the bearing's characteristics to determine the correct mounting method.

PROPER HANDLING OF BEARINGS

Since rolling bearings are high precision machine parts, they must be handled accordingly. Even if high quality bearings are used, their expected performance cannot be achieved if they are not handled properly. The main precautions to be observed are as follows:

Keep Bearings and Surrounding Area Clean

Dust and dirt have harmful effects on bearings. It is necessary to keep bearings and their environment, including worktables, handling equipment, and tools, as clean as possible. Leave the bearings in their packaging until ready to use.

Careful Handling

Dropping or mishandling the bearing can result in brinelling, cage damage, ring fracture, seal damage and other damage detrimental to the life and quiet running of the bearing.

Use Proper Tools

Always use the proper equipment when handling bearings and avoid general purpose tools.

Prevent Corrosion

Keep the bearings in the packaging until ready to use. Store in a temperature and humidity controlled room. Handle with clean, dry hands or wear gloves. Bearings should NOT be cleaned of rust preventative oil (RP) unless specifically instructed.





BEARING STORAGE

To prevent rusting, each bearing is treated and packed with an anticorrosive agent, but depending on the environment of the storing place, the effectiveness of the corrosion countermeasures varies greatly. Careful attention is necessary to select a suitable place to keep and stock replacement bearings.

General recommended practices for optimal bearing storage include:

- > Keep the bearing stored in its original packaging
- > Lay the bearing on its side
- > The storage room should be temperature controlled with variation of no more than 5 degrees F (3 degrees C)
- > The storage room should be humidity controlled with a relative humidity of less than 60% at all times
- > The storage room should be free of external vibration
- Bearings should be stored on a shelf with appropriate load capacity at least 12 inches from the floor

Bearing Storage Duration

Storage duration is affected by the environment (temperature, humidity, vibration, etc.). The following storage times assume an appropriate environment and unopened packaging.

- > Ungreased, individually packaged bearings: up to 5 years
- > Ungreased, bulk packaged bearings: up to 3 years
- Greased, individually packaged bearings: from 1 to 10 years depending on the grease type. Consult NSK for more details.
- Greased, bulk packaged bearings: up to 2 years depending on the grease type. Consult NSK for more details.

WORK SITE, TOOLS AND EQUIPMENT

Select or prepare a clean work site where a working table, surface plate, cleaning tank, and bearing heater or oil heating tank are provided and where heavy material such as the bearing, sleeve, shaft, etc. can be freely and safely moved. Jigs, tools, measuring instruments and environment of work site shall always be kept clean in order to prevent introducing dust or contamination into the bearing and its operating environment.

Prior to the start of bearing mounting work, examine the steps involved in the mounting method by referring to the drawing and confirming that all necessary jigs and tools required for installation are in order. Depending on the work, preparation of a special jig may be necessary; therefore, preliminary examination and assessment is recommended.

METHODS OF MOUNTING

SELECTION OF MOUNTING METHODS

The method of mounting rolling bearings strongly affects their accuracy, life, and performance, so their mounting deserves careful attention. Their characteristics should first be thoroughly studied, and then they should be mounted in the proper manner. It is recommended that the handling procedures for bearings be fully investigated by the design engineers and that standards be established with respect to the following items:

- > Cleaning the bearings and related parts
- > Checking the dimensions and finish of related parts
- Mounting
- Inspection after mounting
- Supply of lubricants

Bearings should not be unpacked until immediately before mounting. When using ordinary grease lubrication, the grease should be packed in the bearings without first cleaning them. Even in the case of ordinary oil lubrication, cleaning the bearings is not required. However, bearings for instruments or for high speed operation must first be cleaned with clean filtered oil in order to remove the anti-corrosion agent. After the bearings are cleaned with filtered oil, they should be protected to prevent corrosion. Do not clean prelubricated bearings.

Bearing mounting methods depend on the bearing type and type of fit. As bearings are usually used on rotating shafts, the inner rings require a tight fit. Bearings with cylindrical bores are usually mounted by pressing them onto the shafts (press fit) or heating them to expand their diameter (shrink fit). Bearings with tapered bores can be mounted directly on tapered shafts or cylindrical shafts using tapered sleeves.

BEARING INNER RING SHAPE	SHAFT SHAPE AND FEAT	URES	MOUNTING PARTS AND	WORKING METHOD		
JUAL	Shape	Features	Parts	Features		
cylindrical bore	cylindrical	 shaft with shoulder with or without oil duct 	 with or without spacer 		 dead-blow mallet press oil heating tank induction heater 	
tapered bore	tapered	 shaft with shoulder with or without oil duct 	 with or without spacer 		 lock nut hydraulic nut 	
tapered bore	cylindrical	> shaft with shoulder	 > adapter sleeve > with or without spacer 	 with or without oil duct 	 lock nut hydraulic nut oil injection pump 	
tapered bore	cylindrical	> shaft with shoulder	> withdrawal sleeve	 with or without oil duct 	 lock nut hydraulic nut oil injection pump 	

Table 1 - Methods of Bearing Mounting



MOUNTING BEARINGS WITH CYLINDRICAL BORES

Press Fits

Fitting with a press requires large force and is therefore widely used for small to medium sized bearings. A mounting tool is placed on the inner ring as shown in **Figure 1.1** and the bearing is slowly pressed onto the shaft with a press until the side of the inner ring rests against the shoulder of the shaft. The mounting tool must not be placed on the outer ring for press mounting, as it may cause the rolling elements to create brinelling indentations on the raceway surfaces as a result of the force applied to the outer ring.

The mounting method using a dead-blow mallet should only be used for small ball bearings with minimally tight fits when a press is not available or cannot be accommodated. In the case of tight interference fits or for medium and large bearings, this method should not be used. Any time a hammer is used, a mounting tool must be placed on the inner ring.

When both the inner and outer rings of non-separable bearings require a tight fit, a mounting tool is placed on both rings as shown in **Figure 1.2**, and both rings are fitted at the same time using a screw or hydraulic press. Since the outer ring of self-aligning ball bearings may misalign, a mounting tool such as that shown in **Figure 1.2** should always be used.

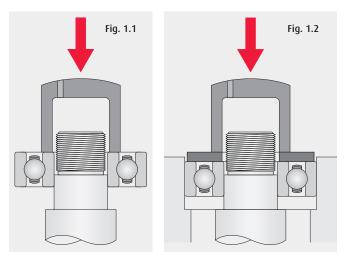
In the case of separable bearings, the inner and outer rings may be mounted separately. In this case, assembly of the inner and outer rings should be done carefully to align the inner and outer rings correctly. Careless or forced assembly may cause scratches on the rolling contact surfaces.

A light oil can be applied to the bearing seat in the case of a tight fit. Anti-fretting paste can be applied to the bearing seat in the case of a loose fit. Do not use molybdenum disulfide (MoS2) paste on any surface.

A light oil added onto the bore and shaft is sufficient. MoS2 paste may introduce lube compatibility or other issues such as potential slipping on the journal.



Fig. 1 - Press Fitting of Inner / Inner and Outer Rings



METHODS OF MOUNTING

Shrink Fits

Since press fitting large bearings requires a large force, a shrink fit is widely used. This method prevents an excessive force being imposed on the bearings and allows for relatively quick mounting. Primary methods employed are heating via an oil bath or with an induction heater.

For the oil bath method, the bearings are first heated in a high-quality mineral oil (**Figure 2**) to expand them before mounting. The oil bath should be large enough to accommodate two to five bearings, with a sufficient amount of oil to completely cover the bearings.

Precautions to follow when making shrink fits include:

- > Do not heat bearings to more than 120°C
- > Suspend bearings, or place them on a wire net at the bottom of an oil tank

- Heat the bearings to a temperature 20 to 30°C higher than the lowest temperature required for mounting without interference to compensate for cooling during mounting
- After mounting, the bearings will shrink axially and radially; press the bearing firmly against the shaft shoulder using locating methods to avoid a clearance between the bearing and shoulder.

The expansion of inner rings for various temperature differences and bearing sizes is illustrated in **Figure 3**.

After mounting a bearing in place, cool it and apply lubricant to its inner and outer surfaces. At that point, make sure the bearing is free of any dirt. Except when preload is applied to a bearing, a clearance is usually needed for the bearing after mounting; therefore, confirm that the bearing rotates smoothly. For roller bearings, clearance can be measured using a feeler gauge.

Fig. 2 - Oil Bath Heating Method

Fig. 3 - Temperature and Thermal Expansion of Inner Ring

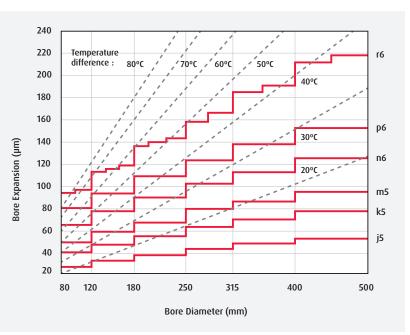
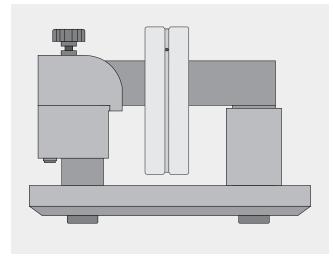




Fig. 4 - Induction Heater Method



An alternative to heating bearings in oil is the use of bearing heaters and electromagnetic induction (**Figure 4**). With induction heating, electricity in a coil produces a magnetic field that induces a current inside the bearing, generating heat. Uniform heating of the bearing is possible, making shrink fitting efficient and clean. Many induction heaters include an automatic demagnetization cycle. Always demagnetize bearings to ensure that they do not attract metallic particles.

A bearing mounted on a shaft cools rapidly, and after heating, an expanded bearing shrinks in a crosswise direction. In some cases, therefore, in order to avoid a clearance between the inner ring and shoulder, press the bearings firmly against the shoulder by means of a shaft nut or other appropriate tool. After mounting a bearing in place, cool it and apply lubricant to its inner and outer surfaces. At that point, make sure the bearing is free of any dirt. Except when preload is applied to a bearing, a clearance is usually needed for the bearing after mounting; therefore, confirm that the bearing rotates smoothly. For roller bearings, clearance can be measured using a feeler gauge.

MOUNTING BEARINGS WITH TAPERED BORES

Bearings with tapered bores are mounted in place using adapter or withdrawal sleeves or mounted directly onto tapered shafts. The degree of fit is determined by reduction in clearance and push-in amount of the sleeves (or bearings). For spherical roller bearings, a decrease in clearance during mounting is usually measured by a feeler gauge.

Spherical roller bearings with tapered bores have generally been manufactured considering the reduction in clearance. Traditionally the method of radial internal clearance reduction is used, but in some cases the push-in amount (axial movement) of the inner ring or withdrawal sleeve is measured instead of directly measuring the reduction in clearance. The angular drive-up by lock nut method is another method used for a select series of spherical roller bearings.

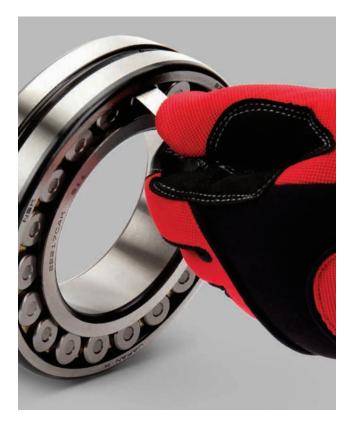
When a feeler gauge cannot be used for small roller bearings because of the small clearance after mounting them in position, the amount of axial movement must be measured instead of the reduction in clearance. Also, in cases where a large bearing is heated in oil to expand it for facilitating mounting, axial movement must also be measured. In this case, the bearing should be initially mounted on the shaft before it is heated, and this initial position measured, then the final mounting position can be determined by the amount of axial movement from the initial mounting position after the bearing has been heated. At this stage, the intended reduction in clearance must be confirmed by measuring the initial clearance prior to heating and the final clearance after cooling.

Supporting information and data for radial clearance reduction, axial drive-up and angular drive-up methods can be found on **pages B11-18.** Step by step mounting instructions utilizing the various methods for bearing and shaft types described in **Table 1,** as well as handling sleeves, lock nuts and hydraulic nuts follow.

The internal clearance in rolling bearings during operation influences bearing performance, including fatigue life, rigidity, vibration, noise, and heat generation. Consequently, measuring the internal bearing clearance during mounting is critical to ensure designed bearing performance is achieved. When measuring the internal bearing clearance, pay careful attention to locate the rollers in the appropriate position(s) for the various methods.

MEASURING UNMOUNTED BEARING CLEARANCE

When measuring unmounted internal bearing clearance, stand the bearing upright (vertically) on a flat surface. Rotate the inner ring clockwise and counterclockwise at least one half rotation while keeping both rings and roller sets aligned to each other. Adjust the rollers until one roller on both sides is located at the top (12 o'clock) position. Measure the clearance at the appropriate position(s) with a feeler gauge.



Bearing Outside Diameter Is Smaller Than 200 mm

Measure a single clearance value across both sets of rollers of the bearing (Δ rT, **Figure 5**). Insert the feeler gauge blade to the side of the rollers positioned at the top of the bearing. Select a blade thinner than the minimum value of internal clearance (as listed on **Table 2, page B12**). Slide the blade between the rollers and the outer ring raceway until there is slight resistance. Do not force a blade between the rollers and raceway if the blade pinches. Repeat this process with a thicker blade each time until the blade does not pass between the rollers and the outer ring raceway. Repeat the procedure again at a different outer ring raceway location and different rollers.

Bearing Outside Diameter Is Larger Than 200 mm

For most cases, the clearance measurement method used for unmounted bearings with outside diameter less than 200 mm is adequate. However, the outer ring of large bearings may deform slightly into an elliptical shape due to its own weight. For the purpose of obtaining the true geometrical internal clearance it is recommended to measure multiple clearance values from both rows of the bearing at 3 positions: the top (12 o'clock), the right (3 o'clock), and the left (9 o'clock) (**Figure 6**).

As previously described, use the feeler gauge to measure the clearance values at the top of the bearing (Δ rT) from each row of the bearing. The internal clearance for this position is:

$\Delta rT = 1/2 (\Delta rT1 + \Delta rT2)$

Repeat the clearance measurements for the right and left positions. The respective internal clearances are as follows:

$\Delta rL = 1/2 (\Delta rL1 + \Delta rL2)$

$\Delta rR = 1/2 (\Delta rR1 + \Delta rR2)$

The internal clearance for the bearing is calculated as follows:

 $\Delta r = 1/2 (\Delta rT + \Delta rL + \Delta rR)$



Fig. 5 - Measuring Clearance (0.D < 200 mm)

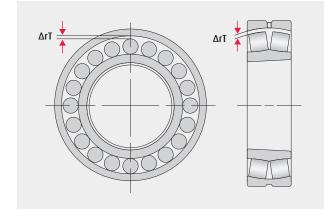


Fig. 6 - Measuring Clearance (0.D > 200 mm)

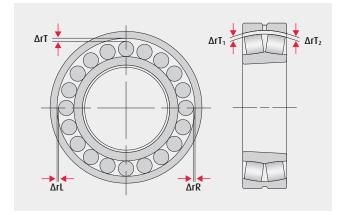
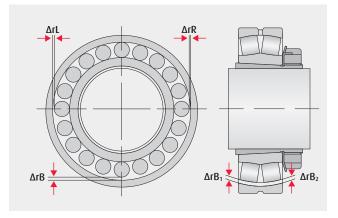


Fig. 7 - Measuring Mounted Clearance (0.D > 200 mm)



MEASURING MOUNTED BEARING CLEARANCE

When measuring mounted internal bearing clearance it is recommended to follow the same methodology employed prior to the bearing mounting for comparative purposes. In this case the mounted bearing is seated and suspended on a shaft in an upright (vertical) orientation. Rotate the inner ring clockwise and counterclockwise at least one half rotation while keeping both rings and roller sets aligned to each other. Adjust the rollers until one roller on both sides is located at the bottom (6 o'clock) position. Measure the clearance at the appropriate position(s) with a feeler gauge.

Bearing Outside Diameter Is Smaller Than 200 mm

Follow the procedure described / employed for measuring unmounted bearings, but in this case measuring clearance from the side of the roller(s) positioned at the bottom of the bearing to measure the clearance ΔrB (6 o'clock).

Bearing Outside Diameter Is Larger Than 200 mm

Follow the procedure described / employed for measuring unmounted bearings, but in this case measuring clearance from the side of the roller(s) positioned at the bottom of the bearing to measure the clearance ΔrB (6 o'clock). If measuring true geometrical internal clearance, measure the clearance at the bottom, ΔrB (6 o'clock), the right, ΔrR (3 o'clock), and the left, ΔrL (9 o'clock) (**Figure 7**).

Follow the calculations provided on **page B9**, substituting clearance values for ΔrT with ΔrB .

Note: In cases where the mounted bearing is resting on a bench or seated in a housing, the clearance measurement should be taken from the 12 o'clock position (**Figure 6**) rather than the bottom position as described above.

PROCEDURE - ADAPTER SLEEVES

Spherical roller bearings with tapered bores must be mounted to a tapered shaft, adapter sleeve, or withdrawal sleeve. When pushing the bearing onto the tapered shaft or sleeve, the inner ring of the bearing expands, resulting in an increase of interference fit to the shaft and a **Reduction in Radial Internal Clearance**. Obtaining proper interference and internal clearance is important when mounting the bearing.

The bearing should be driven up the tapered shaft or sleeve in small increments. The radial internal clearance should be measured after each incremental adjustment to ensure that the bearing isn't driven up too far onto the taper. Repeat the procedure of driving up the bearing in small increments until the desired radial internal clearance reduction is obtained. See **Table 2**.

Note: Always use clearance tables provided by the manufacturer of the bearing installed. Using alternative tables can result in clearances that are too tight or loose, and lead to bearing damage, including inner ring fracture. Always verify the final radial internal clearance with a feeler gauge.

If heat is used to install the bearing - make sure the bearing and mating components (shaft, etc.) have all cooled to the same temperature before measuring

If a lock washer is used to lock the nut - prior to bending the lock washer tab into the slot of the nut, verify once again that the clearance matches specification and has not changed during installation of the lock washer.

If a hydraulic nut is used to install the bearing - verify the radial internal clearance before locking the lock nut.

If an oil injection pump is used to assist in installation -

the oil pressure must be bled to zero before verifying the final measurement with the feeler gauge. Measuring with oil injection pressure still applied can make the measurement appear smaller than the actual clearance of the bearing

CLEARANCE REDUCTION AMOUNT

When radial internal clearance is CN (normal clearance), C3 or C4, target the clearance adjustment at the lower end of the reduction range unless the bearing is subject to high vibration, heavy loads or is manufactured with case hardened inner rings, in which case the upper end of the reduction range is recommended.

When the load condition is known, target the following clearance reduction amounts:

- > For light or normal loads, use the lower half of the reduction range
- > For heavy or shock loads, use the upper half of the reduction range

INTERNAL CLEARANCE ADJUSTMENT

Perform the adjustment by measuring the clearance reduction amount with the feeler gauge.

- For measurement position and measured point, refer to Measuring Bearing Clearance on pages B9 and 10.
- > When mounting a bearing on a tapered shaft, repeat the clearance measurement each time the bearing is driven up by the lock nut, end plate, end cap or hydraulic nut.
- > When using an adapter sleeve, repeat the clearance measurement each time the bearing is driven up by the lock nut or hydraulic nut.
- > When using a withdrawal sleeve, measure clearance each time the withdrawal sleeve is driven up by the lock nut or hydraulic nut.

Record the value of each clearance measurement for use in the clearance adjustment process.



NOMINA BORE DIAMETE		RADIAL II	NTERNAL CI	LEARANCE	(INCH)			REDUCTIO	.L	AXIAL DI	SPLACEMEN	PLACEMENT* (INCH) 1:12 Taper 1:30		MINIMUM PERMISSIBLE RESIDUAL CLEARANCE AFTER MOUNTING (INCH)		
(MM)	~	CI	N	C	3	c	4	CLEARAN	CLEARANCE (INCH)		CLEARANCE (INCH) Taper 1:12					
over	incl.	min	max	min	max	min	max	min	max	min	max	min	max	CN	C3	C4
30	40	0.0014	0.0020	0.0020	0.0026	0.0026	0.0033	0.0010	0.0012	0.0157	0.0177	-	-	0.0004	0.0010	0.0014
40	50	0.0018	0.0024	0.0024	0.0031	0.0031	0.0039	0.0012	0.0014	0.0177	0.0217	-	-	0.0006	0.0012	0.0018
50	65	0.0022	0.0030	0.0030	0.0037	0.0037	0.0047	0.0012	0.0014	0.0177	0.0217	-	-	0.0010	0.0014	0.0024
65	80	0.0028	0.0037	0.0037	0.0047	0.0047	0.0059	0.0016	0.0018	0.0236	0.0276	-	-	0.0012	0.0016	0.0030
80	100	0.0031	0.0043	0.0043	0.0055	0.0055	0.0071	0.0018	0.0022	0.0276	0.0335	0.0689	0.0846	0.0014	0.0020	0.0033
100	120	0.0039	0.0053	0.0053	0.0067	0.0067	0.0087	0.0020	0.0024	0.0295	0.0354	0.0748	0.0886	0.0018	0.0026	0.0043
120	140	0.0047	0.0063	0.0063	0.0079	0.0079	0.0102	0.0024	0.0028	0.0354	0.0433	0.0886	0.1083	0.0022	0.0031	0.0051
140	160	0.0051	0.0071	0.0071	0.0091	0.0091	0.0118	0.0026	0.0031	0.0394	0.0512	0.0984	0.1280	0.0024	0.0039	0.0059
160	180	0.0055	0.0079	0.0079	0.0102	0.0102	0.0134	0.0028	0.0035	0.0433	0.0551	0.1083	0.1378	0.0028	0.0043	0.0067
180	200	0.0063	0.0087	0.0087	0.0114	0.0114	0.0146	0.0031	0.0039	0.0512	0.0630	0.1280	0.1575	0.0028	0.0043	0.0075
200	225	0.0071	0.0098	0.0098	0.0126	0.0126	0.0161	0.0035	0.0043	0.0551	0.0669	0.1378	0.1673	0.0031	0.0051	0.0083
225	250	0.0079	0.0106	0.0106	0.0138	0.0138	0.0177	0.0039	0.0047	0.0630	0.0748	0.1575	0.1870	0.0035	0.0055	0.0091
250	280	0.0087	0.0118	0.0118	0.0154	0.0154	0.0193	0.0043	0.0055	0.0669	0.0866	0.1673	0.2165	0.0039	0.0059	0.0098
280	315	0.0094	0.0130	0.0130	0.0169	0.0169	0.0213	0.0047	0.0059	0.0748	0.0945	0.1870	0.2362	0.0043	0.0063	0.0110
315	355	0.0106	0.0142	0.0142	0.0185	0.0185	0.0232	0.0055	0.0067	0.0866	0.1063	0.2165	0.2657	0.0047	0.0071	0.0118
355	400	0.0118	0.0157	0.0157	0.0205	0.0205	0.0256	0.0059	0.0075	0.0945	0.1181	0.2362	0.2953	0.0051	0.0079	0.0130
400	450	0.0130	0.0173	0.0173	0.0224	0.0224	0.0283	0.0067	0.0083	0.1063	0.1299	0.2657	0.3248	0.0055	0.0087	0.0142
450	500	0.0146	0.0193	0.0193	0.0248	0.0248	0.0311	0.0075	0.0094	0.1181	0.1457	0.2953	0.3642	0.0063	0.0094	0.0154
500	560	0.0161	0.0213	0.0213	0.0268	0.0268	0.0343	0.0083	0.0106	0.1339	0.1693	0.3346	0.4331	0.0067	0.0106	0.0161
560	630	0.0181	0.0236	0.0236	0.0299	0.0299	0.0386	0.0091	0.0118	0.1457	0.1890	0.3642	0.4724	0.0079	0.0122	0.0181
630	710	0.0201	0.0264	0.0264	0.0335	0.0335	0.0429	0.0102	0.0130	0.1654	0.2087	0.4134	0.5118	0.0087	0.0130	0.0205
710	800	0.0224	0.0295	0.0295	0.0378	0.0378	0.0480	0.0110	0.0146	0.1772	0.2323	0.4528	0.5906	0.0094	0.0154	0.0232
800	900	0.0252	0.0331	0.0331	0.0421	0.0421	0.0539	0.0122	0.0161	0.1969	0.2598	0.4921	0.6496	0.0110	0.0169	0.0260
900	1,000	0.0280	0.0366	0.0366	0.0469	0.0469	0.0598	0.0134	0.0181	0.2165	0.2913	0.5512	0.7283	0.0122	0.0185	0.0287
1,000	1,120	0.0303	0.0406	0.0406	0.0512	0.0512	0.0657	0.0146	0.0197	0.2323	0.3150	0.5906	0.7874	0.0142	0.0209	0.0315

Table 2 - Radial Clearance Reduction for Spherical Roller Bearings with Tapered Bore

*Axial displacement values apply only to solid steel shafts or hollow steel shafts where the bore is equal to or less than one-half of the outside diameter. If the material is other than steel, or if thin wall journals are used, please consult NSK.

Taper 1:12 applies to series 213, 222, 223, 230, 231, 232, 233, 238 and 239. Taper 1:30 applies to series 240, 241 and 242.

For normal (CN) clearance, target the middle of the reduction range. For C3 or C4 clearance, target the upper half of the reduction range. For light or normal loads, target the lower half of the reduction range. For heavy or shock loads, target the upper half of the reduction range.

MOUNTING BEARINGS WITH TAPERED BORES AXIAL DRIVE-UP METHOD

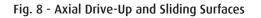
AXIAL DRIVE-UP METHOD

This method can be used for medium and large bearings with a tapered bore being mounted with an adapter or withdrawal sleeve, or directly onto a tapered shaft. The hydraulic nut provides the drive-up force to seat the bearing on the journal. This method is most beneficial as the bearings get large and the required force becomes too great for other manual methods. **Tables 3.1 to 3.9** provide the pressure necessary to move the bearing into the starting position along with a measured axial drive-up distance, typically executed with use of a dial indicator.

Figure 8 illustrates axial drive-up starting and final positions (**Figure 8.1**) as well as relative sliding surfaces for mounting directly onto a tapered shaft (**Figure 8.2**), with an adapter sleeve (**Figure 8.3, 8.4**) or withdrawal sleeve (**Figure 8.5**).

Table 3.1 - Series 213
Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUC		PRESSURE A	ND DRIVE-UP	REMAINING	
PART NO.	RADIAL CLEA (INCH)	KANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE	
	min	max	psi	psi	inch	
21310EAK	0.0012	0.0014	359	652	0.0185	
21311EAK	0.0012	0.0014	262	476	0.0168	
21312EAK	0.0012	0.0014	366	666	0.0185	
21313EAK	0.0012	0.0014	355	645	0.0184	
21314EAK	0.0016	0.0018	456	828	0.0238	
21315EAK	0.0016	0.0018	369	670	0.0222	
21316EAK	0.0016	0.0018	388	705	0.0224	
21317EAK	0.0018	0.0022	349	635	0.0245	
21318EAK	0.0018	0.0022	350	636	0.0246	
21319CAMK	0.0018	0.0022	423	770	0.0258	
21320CAMK	0.0018	0.0022	455	826	0.0255	
21322CAMK	0.0020	0.0024	458	832	0.0284	



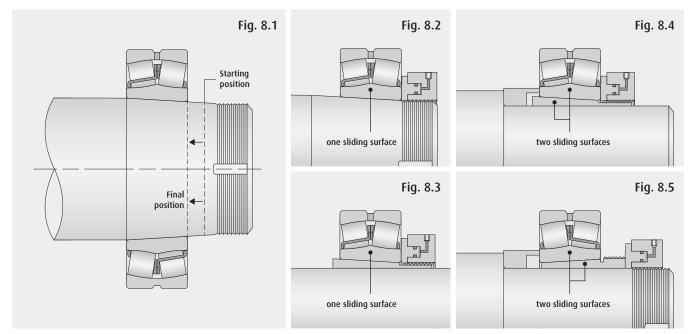




Table 3.2 - Series 222

Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUC		PRESSURE A	REMAINING		
PART NO.	RADIAL CLEA (INCH)	RANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE	
	min	max	psi	psi	inch	
22210EAK	0.0012	0.0014	148	269	0.0153	
22211EAK	0.0012	0.0014	145	263	0.0152	
22212EAK	0.0012	0.0014	166	302	0.0154	
22213EAK	0.0012	0.0014	189	343	0.0157	
22214EAK	0.0016	0.0018	197	357	0.0198	
22215EAK	0.0016	0.0018	162	294	0.0193	
22216EAK	0.0016	0.0018	177	322	0.0195	
22217EAK	0.0018	0.0022	223	406	0.0230	
22218EAK	0.0018	0.0022	244	443	0.0232	
22219EAK	0.0018	0.0022	261	475	0.0233	
22220EAK	0.0018	0.0022	252	459	0.0230	
22222EAK	0.0020	0.0024	273	495	0.0250	
22224EAK	0.0020	0.0024	284	517	0.0251	
22226EAK	0.0024	0.0028	333	606	0.0294	
22228CAMK	0.0024	0.0028	349	634	0.0296	
22230CAMK	0.0026	0.0031	399	726	0.0332	
22232CAMK	0.0026	0.0031	375	682	0.0331	
22234CAMK	0.0028	0.0035	446	811	0.0371	
22236CAMK	0.0028	0.0035	349	635	0.0361	
22238CAMK	0.0031	0.0039	391	711	0.0409	
22240CAMK	0.0031	0.0039	407	740	0.0413	
22244CAMK	0.0035	0.0043	431	783	0.0458	
22248CAMK	0.0039	0.0047	468	851	0.0505	
22252CAMK	0.0043	0.0055	515	937	0.0575	
22256CAMK	0.0043	0.0055	431	784	0.0569	
22260CAMK	0.0047	0.0059	471	856	0.0619	
22264CAMK	0.0055	0.0067	526	956	0.0712	

Table 3.3 - Series 223Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUCTION IN		PRESSURE AND DRIVE-UP		REMAINING
PART NO.	RADIAL CLEA (INCH)	RANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
22310EAK	0.0012	0.0014	382	695	0.0167
22311EAK	0.0012	0.0014	409	744	0.0170
22312EAK	0.0012	0.0014	406	738	0.0168
22313EAK	0.0012	0.0014	371	674	0.0166
22314EAK	0.0016	0.0018	489	889	0.0217
22315EAK	0.0016	0.0018	494	898	0.0215
22316EAK	0.0016	0.0018	488	888	0.0214
22317EAK	0.0018	0.0022	573	1042	0.0252
22318EAK	0.0018	0.0022	555	1009	0.0250
22319EAK	0.0018	0.0022	544	989	0.0248
22320EAK	0.0018	0.0022	610	1110	0.0252
22322EAK	0.0020	0.0024	711	1293	0.0282
22324EAK	0.0020	0.0024	692	1258	0.0279
22326CAMK	0.0024	0.0028	757	1376	0.0321
22328CAMK	0.0024	0.0028	765	1391	0.0319
22330CAMK	0.0026	0.0031	828	1505	0.0357
22332CAMK	0.0026	0.0031	754	1371	0.0356
22334CAMK	0.0028	0.0035	666	1211	0.0376
22336CAMK	0.0028	0.0035	641	1166	0.0376
22338CAMK	0.0031	0.0039	678	1232	0.0423
22340CAMK	0.0031	0.0039	796	1447	0.0443
22344CAMK	0.0035	0.0043	737	1340	0.0481
22348CAMK	0.0039	0.0047	758	1378	0.0529
22352CAMK	0.0043	0.0055	802	1458	0.0600
22356CAMK	0.0043	0.0055	756	1375	0.0600
22360CAMK	0.0047	0.0059	765	1391	0.0646
22364CAMK	0.0055	0.0067	891	1620	0.0749

*Values apply only to solid steel shafts or hollow steel shafts where the shaft bore is equal to or less than one-half of the shaft outside diameter. If the material is other than steel, or if thin wall journals are used, please consult NSK.

MOUNTING BEARINGS WITH TAPERED BORES AXIAL DRIVE-UP METHOD

Table 3.4 - Series 230

Pressure and Axial Drive-Up for Spherical Roller Bearings

PART NO.	TOTAL REDUCTION IN		PRESSURE AND DRIVE-UP		REMAINING
	RADIAL CLEA (INCH)	ARANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
23020CDK	0.0018	0.0022	129	235	0.0216
23022CDK	0.002	0.0024	169	308	0.0239
23024CDK	0.002	0.0024	149	271	0.0237
23026CDK	0.0024	0.0028	201	365	0.0282
23028CDK	0.0024	0.0028	179	326	0.0279
23030CDK	0.0026	0.0031	198	359	0.0312
23032CDK	0.0026	0.0031	179	326	0.0311
23034CDK	0.0028	0.0035	213	387	0.0345
23036CDK	0.0028	0.0035	207	377	0.0343
23038CAMK	0.0031	0.0039	216	393	0.0387
23040CAMK	0.0031	0.0039	249	453	0.0393
23044CAMK	0.0035	0.0043	238	433	0.0431
23048CAMK	0.0039	0.0047	206	375	0.0467
23052CAMK	0.0043	0.0055	238	433	0.0531
23056CAMK	0.0043	0.0055	219	398	0.0532
23060CAMK	0.0047	0.0059	264	481	0.0582
23064CAMK	0.0055	0.0067	256	465	0.0661
23068CAMK	0.0055	0.0067	270	491	0.0664
23072CAMK	0.0059	0.0075	250	454	0.0721
23076CAMK	0.0059	0.0075	230	419	0.0719
23080CAMK	0.0059	0.0075	233	424	0.072
23084CAMK	0.0067	0.0083	238	433	0.0803
23088CAMK	0.0067	0.0083	231	420	0.0801
23092CAMK	0.0075	0.0094	260	473	0.0908
23096CAMK	0.0075	0.0094	225	410	0.0901

Table 3.5 - Series 231 Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUCTION IN		PRESSURE AN	REMAINING	
PART NO.	RADIAL CLEA (INCH)		1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
23120CK	0.0018	0.0022	213	387	0.022
23122CK	0.002	0.0024	261	474	0.0246
23124CK	0.002	0.0024	255	463	0.0244
23126CK	0.0024	0.0028	283	514	0.0286
23128CK	0.0024	0.0028	258	470	0.0283
23130CK	0.0026	0.0031	369	671	0.0323
23132CK	0.0026	0.0031	344	626	0.0323
23134CK	0.0028	0.0035	323	588	0.0351
23136CK	0.0028	0.0035	329	599	0.0352
23138CK	0.0031	0.0039	378	688	0.0399
23140CK	0.0031	0.0039	392	712	0.0401
23144CK	0.0035	0.0043	385	700	0.0442
23148CK	0.0039	0.0047	376	684	0.0482
23152CAMK	0.0043	0.0055	432	785	0.055
23156CAMK	0.0043	0.0055	366	666	0.0545
23160CAMK	0.0047	0.0059	402	730	0.0591
23164CAMK	0.0055	0.0067	466	847	0.068
23168CAMK	0.0055	0.0067	496	901	0.0686
23172CAMK	0.0059	0.0075	456	829	0.0743
23176CAMK	0.0059	0.0075	409	745	0.0738
23180CAMK	0.0059	0.0075	391	711	0.0739
23184CAMK	0.0067	0.0083	467	849	0.083
23188CAMK	0.0067	0.0083	423	769	0.0824
23192CAMK	0.0075	0.0094	491	892	0.0936
23196CAMK	0.0075	0.0094	466	847	0.0934

^aValues apply only to solid steel shafts or hollow steel shafts where the shaft bore is equal to or less than one-half of the shaft outside diameter. If the material is other than steel, or if thin wall journals are used, please consult NSK.



Table 3.6 - Series 232

Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUCTION IN		PRESSURE AND DRIVE-UP		REMAINING
PART NO.	RADIAL CLEA (INCH)	RANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
23218CK	0.0018	0.0022	287	521	0.0227
23219CK	0.0018	0.0022	290	527	0.0227
23220CK	0.0018	0.0022	327	595	0.023
23222CK	0.002	0.0024	378	687	0.0252
23224CK	0.002	0.0024	361	656	0.0249
23226CK	0.0024	0.0028	400	727	0.0292
23228CK	0.0024	0.0028	437	795	0.0294
23230CK	0.0026	0.0031	505	919	0.033
23232CK	0.0026	0.0031	484	880	0.0331
23234CK	0.0028	0.0035	524	953	0.0366
23236CK	0.0028	0.0035	462	839	0.0362
23238CK	0.0031	0.0039	486	883	0.0405
23240CK	0.0031	0.0039	519	944	0.0411
23244CK	0.0035	0.0043	556	1011	0.0455
23248CAMK	0.0039	0.0047	579	1053	0.0498
23252CAMK	0.0043	0.0055	648	1178	0.0569
23256CAMK	0.0043	0.0055	539	981	0.0561
23260CAMK	0.0047	0.0059	577	1050	0.0607
23264CAMK	0.0055	0.0067	667	1213	0.0701
23268CAMK	0.0055	0.0067	672	1222	0.0702
23272CAMK	0.0059	0.0075	659	1199	0.0763
23276CAMK	0.0059	0.0075	636	1155	0.0763
23280CAMK	0.0059	0.0075	616	1119	0.0762
23284CAMK	0.0067	0.0083	689	1252	0.0855
23288CAMK	0.0067	0.0083	655	1190	0.0852
23292CAMK	0.0075	0.0094	782	1423	0.0974
23296CAMK	0.0075	0.0094	722	1313	0.0965

Table 3.7 - Series 239Pressure and Axial Drive-Up for Spherical Roller Bearings

PART NO.	TOTAL REDUCTION IN RADIAL CLEARANCE (INCH)		PRESSURE AND DRIVE-UP		REMAINING
			1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
23926CAMK	0.0024	0.0028	98	177	0.0271
23932CAMK	0.0026	0.0031	98	177	0.0301
23934CAMK	0.0028	0.0035	93	170	0.0331
23936CAMK	0.0028	0.0035	109	197	0.0333
23938CAMK	0.0031	0.0039	104	189	0.0373
23940CAMK	0.0031	0.0039	125	227	0.0377
23944CAMK	0.0035	0.0043	106	192	0.0414
23948CAMK	0.0039	0.0047	94	170	0.0452
23952CAMK	0.0043	0.0055	140	254	0.0521
23956CAMK	0.0043	0.0055	117	212	0.0517
23960CAMK	0.0047	0.0059	149	271	0.0563
23964CAMK	0.0055	0.0067	150	272	0.0645
23968CAMK	0.0055	0.0067	123	224	0.0638
23972CAMK	0.0059	0.0075	121	219	0.0699
23976CAMK	0.0059	0.0075	148	270	0.0705
23980CAMK	0.0059	0.0075	126	229	0.0701
23984CAMK	0.0067	0.0083	124	225	0.078
23988CAMK	0.0067	0.0083	138	251	0.0784
23992CAMK	0.0075	0.0094	141	257	0.0884
23996CAMK	0.0075	0.0094	144	261	0.0885

*Values apply only to solid steel shafts or hollow steel shafts where the shaft bore is equal to or less than one-half of the shaft outside diameter. If the material is other than steel, or if thin wall journals are used, please consult NSK.

MOUNTING BEARINGS WITH TAPERED BORES AXIAL DRIVE-UP METHOD

Table 3.8 - Series 240

Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUCTION IN		PRESSURE AND DRIVE-UP		REMAINING
PART NO.	RADIAL CLEA (INCH)	RANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
24020CK30	0.0018	0.0022	172	313	0.0539
24022CK30	0.002	0.0024	222	403	0.0597
24024CK30	0.002	0.0024	188	342	0.0589
24026CK30	0.0024	0.0028	263	478	0.0703
24028CK30	0.0024	0.0028	233	423	0.0697
24030CK30	0.0026	0.0031	261	474	0.0779
24032CK30	0.0026	0.0031	248	451	0.078
24034CK30	0.0028	0.0035	294	534	0.0864
24036CK30	0.0028	0.0035	309	562	0.0868
24038CK30	0.0031	0.0039	297	540	0.097
24040CK30	0.0031	0.0039	318	579	0.0978
24044CK30	0.0035	0.0043	321	584	0.108
24048CK30	0.0039	0.0047	287	521	0.1177
24052CAMK30	0.0043	0.0055	345	627	0.134
24056CAMK30	0.0043	0.0055	297	540	0.1333
24060CAMK30	0.0047	0.0059	343	624	0.1447
24064CAMK30	0.0055	0.0067	336	611	0.1651
24068CAMK30	0.0055	0.0067	382	694	0.1668
24072CAMK30	0.0059	0.0075	357	649	0.1815
24076CAMK30	0.0059	0.0075	311	565	0.18
24080CAMK30	0.0059	0.0075	322	586	0.1804
24084CAMK30	0.0067	0.0083	329	598	0.2015
24088CAMK30	0.0067	0.0083	333	606	0.2018
24092CAMK30	0.0075	0.0094	369	671	0.2285
24096CAMK30	0.0075	0.0094	319	581	0.2268

Table 3.9 - Series 241 Pressure and Axial Drive-Up for Spherical Roller Bearings

	TOTAL REDUCTION IN		PRESSURE AND DRIVE-UP		REMAINING
PART NO.	RADIAL CLEA (INCH)	RANCE	1 Surface	2 Surfaces	DRIVE-UP DISTANCE
	min	max	psi	psi	inch
24122CK30	0.002	0.0024	300	545	0.0609
24124CK30	0.002	0.0024	357	649	0.0617
24126CK30	0.0024	0.0028	370	674	0.0721
24128CK30	0.0024	0.0028	341	620	0.0712
24130CK30	0.0026	0.0031	457	830	0.0807
24132CK30	0.0026	0.0031	429	781	0.0805
24134CK30	0.0028	0.0035	414	752	0.0882
24136CK30	0.0028	0.0035	422	768	0.0885
24138CK30	0.0031	0.0039	442	804	0.0989
24140CK30	0.0031	0.0039	491	892	0.1003
24144CK30	0.0035	0.0043	502	913	0.1112
24148CK30	0.0039	0.0047	471	855	0.1206
24152CK30	0.0043	0.0055	591	1075	0.1393
24156CAMK30	0.0043	0.0055	485	882	0.1375
24160CAMK30	0.0047	0.0059	531	965	0.1489
24164CAMK30	0.0055	0.0067	628	1143	0.1722
24168CAMK30	0.0055	0.0067	649	1180	0.1722
24172CAMK30	0.0059	0.0075	606	1102	0.187
24176CAMK30	0.0059	0.0075	541	984	0.1857
24180CAMK30	0.0059	0.0075	503	915	0.1854
24184CAMK30	0.0067	0.0083	656	1193	0.2111
24188CAMK30	0.0067	0.0083	588	1069	0.2095
24192CAMK30	0.0075	0.0094	654	1190	0.2361
24196CAMK30	0.0075	0.0094	617	1122	0.2357

"Values apply only to solid steel shafts or hollow steel shafts where the shaft bore is equal to or less than one-half of the shaft outside diameter. If the material is other than steel, or if thin wall journals are used, please consult NSK.

MOUNTING BEARINGS WITH TAPERED BORES ANGULAR DRIVE-UP METHOD



ANGULAR DRIVE-UP METHOD

This method can be used for series 222 and 223 spherical roller bearings and for self-aligning ball bearings and relies on tightening the lock nut to a predetermined angle specific to the bearing part number. After handtightening the lock nut to a position where the adapter sleeve no longer rotates or moves axially on the shaft, a reference point made at the 12 o'clock position on the lock nut face serves as the starting point to complete the bearing drive-up to the specified tightening angle with a spanner wrench and hammer. Table 4 provides the angular turn guidelines for series 222 and 223 spherical roller bearings. For self-aligning ball bearings, see Tables 5 and 6 on pages B41 and 42.

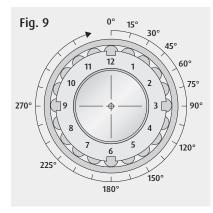


Figure 9 depicts angular turns, such as the data presented in **Table 4**, relative to a 12 o'clock reference point.

Table 4 - Series 222 and 223

Angular Drive-up for Spherical Roller Bearings, Inch and Metric Lock Nut

BORE DIAMETER (MM)	AXIAL DRIV	AXIAL DRIVE UP (IN)		ANGULAR 1 (DEGREES)	URN	METRIC LOCK	ANGULAR T (DEGREES)	ANGULAR TURN (DEGREES)	
	min	max	NUT	min	max	NUT	min	max	
35	0.016	0.018	N07	100	115	КМ7	95	105	
40	0.016	0.018	N08	100	115	КМ8	95	105	
45	0.018	0.022	N09	115	140	КМ9	105	130	
50	0.018	0.022	N10	115	140	КМ10	105	130	
55	0.018	0.022	N11	115	140	KM11	80	100	
60	0.018	0.022	N12	115	140	KM12	80	100	
65	0.018	0.022	N13	115	140	KM13	80	100	
70	0.024	0.028	N14	155	180	KM14	105	125	
75	0.024	0.028	AN15	100	120	KM15	105	125	
80	0.024	0.028	AN16	100	120	KM16	105	125	
85	0.028	0.034	AN17	120	145	KM17	125	155	
90	0.028	0.034	AN18	120	145	KM18	125	155	
95	0.028	0.034	AN19	120	145	KM19	125	155	
100	0.028	0.034	AN20	120	145	КМ20	125	155	
105	0.030	0.035	AN21	125	150	KM21	135	160	
110	0.030	0.035	AN22	125	150	KM22	135	160	
120	0.030	0.035	AN24	125	150	KM24	135	160	
130	0.035	0.043	AN26	150	185	KM26	160	195	
140	0.035	0.043	AN28	150	185	KM28	160	195	
150	0.039	0.051	AN30	165	220	KM30	175	230	
160	0.039	0.051	AN32	110	145	KM32	115	155	
170	0.043	0.055	AN34	120	155	KM34	130	165	
180	0.043	0.055	AN36	120	155	KM36	130	165	
190	0.051	0.063	AN38	145	180	KM38	155	190	
200	0.051	0.063	AN40	145	180	КМ40	155	190	

^aValues apply only to solid steel shafts or hollow steel shafts where the shaft bore is equal to or less than one-half of the shaft outside diameter. If the material is other than steel, or if thin wall journals are used, please consult NSK.

MOUNTING BEARINGS WITH TAPERED BORES HANDLING OF SLEEVES AND LOCK NUTS

PROCEDURE - ADAPTER SLEEVES

- Unpack the adapter while wearing clean thin rubber gloves. Put it upright on the surface plate and remove the lock nut mounted on the adapter.
- Wipe the surface of the shaft with clean oil to remove dirt, then wipe the shaft and the adapter bore with a clean cloth to remove oils from these surfaces. Also wipe clean the tapers of the adapter OD and bearing bore to remove oils.
- 3. Verify that the shaft diameter is within specification.
- 4. Before mounting, apply a light oil to all mating surfaces.
- 5. Mount the adapter sleeve so that its threaded end is toward the shaft end. For shafts with shoulders (Figure 10), if a spacer ring is needed, insert the adapter sleeve into the bore of the spacer ring face, then mount onto the shaft. For straight shafts without shoulders, mount the adapter ring into the desired axial position on the shaft, keeping in mind that the bearing will move up the taper as the lock nut is tightened. To facilitate mounting the adapter sleeve onto the shaft, the slot can be widened slightly by holding it open with a screwdriver or chisel.



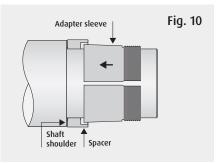


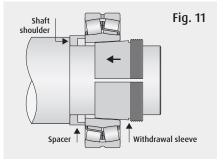
- Measure and record the bearing internal clearance. This is the Measured Initial Clearance.
- With bearing and sleeve tapered surfaces aligned, mount the bearing onto the adapter sleeve. For a shaft with shoulder and spacer ring, the bearing inner ring end face should contact the spacer ring end face.

PROCEDURE - WITHDRAWAL SLEEVES

Begin by executing Steps 1 to 4 of **Procedure – Adapter Sleeves**, then continue with the following steps:

- 5. If a spacer ring is needed, then mount it onto the shaft.
- 6. Measure and record the bearing internal clearance. This is the Measured Initial Clearance.
- Install the bearing onto the shaft with the larger side of the tapered bore oriented toward the shaft end. If a spacer ring is used, the bearing inner ring end face should contact the spacer ring end face (Figure 11).
- 8. After mounting the bearing, mount the withdrawal sleeve on the shaft with the threaded portion of the sleeve oriented toward the shaft end. Slide the withdrawal sleeve into the bearing bore as it is installed. To facilitate mounting the withdrawal sleeve onto the shaft, the slot can be widened slightly by holding it open with a screwdriver or chisel.







METHODS TO SECURE LOCK NUT

The lock nut should be secured from loosening during operation using a lock washer or a lock plate. The final position of a lock plate is set during radial clearance setting. A lock washer is not used during clearance setting, so lock washer thickness must be accounted for in setting its final position. The final position is verified using matching marks, vernier caliper or direct check methods.

Matching marks method (Fig. 12)

Before the lock nut is loosened, matching marks are applied to the lock nut and adapter sleeve/shaft end after completing the clearance setting (**Figure 12.1**). The final lock nut position is determined by a change in angle based on the thickness of the lock washer and the pitch of the lock nut (**Figure 12.2**). If the change in angle is more than 360 degrees, record the number of additional rotations required to remove the lock nut after determining the final position.

The change in angle is calculated as:

θ = (t/p) x 360°

Where:

- **p**: Thread pitch of lock nut, (mm)
- t: Thickness of lock washer, (mm)
- *Θ*: Degrees by which the lock nut angular position must reduced.

Installing the lock washer

After the lock nut has been removed, lubricate the contacting faces of the lock washer and lock nut. Install the lock washer between the lock nut and bearing, aligning the inside tab with the slot of the adapter sleeve or key way in the shaft. Tighten the lock nut to the calculated position or beyond until a tab aligns. Do not loosen. Bend the lock washer tab until it seats in the notch.

Caution: Do not rotate the lock washer with the lock nut as the inside tab may break. Do not use sharp tools to bend the tab.

Vernier calipers method (Figure 13)

Measure the distance between the adapter sleeve end face and the nut end face with vernier calipers. The target value is the measured value less the plate thickness of the lock washer.

L = L0 - t

Where:

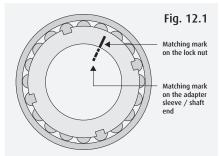
- **LO** : Measured value of distance between the sleeve end face and lock nut outer face (mm)
- t: Thickness of lock washer (mm)
- L: Target value (mm)

Direct check method

The radial clearance should be recorded upon setting. The lock nut is removed, the lock washer is set as recommended, and the lock nut is reinstalled securely. Ensure there is no deviation from the original recorded clearance setting.

Lock plate method (Figure 14)

When a lock plate is used for the nut, adjust the lock nut so that the nearest cutout on the outside of the lock nut mates with the slot of the adapter sleeve. Measure the radial clearance



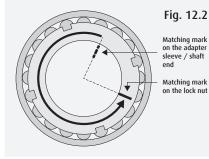
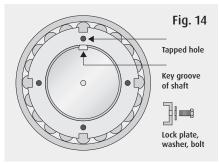


Fig. 13



with a feeler gauge to confirm that the target radial clearance has been achieved. Insert, then fix the lock plate to the nut with the washer and bolt.

MOUNTING BEARINGS WITH TAPERED BORES HANDLING INSTRUCTIONS FOR HYDRAULIC NUTS

Tools required: feeler gauges, portable hydraulic pump, dial indicator

The hydraulic nut is an installation tool designed to assist bearing mounting on a tapered adapter sleeve, withdrawal sleeve, or tapered shaft. After the bearing has been tightened, the hydraulic nut must be replaced with the standard lock washer and lock nut.

PROCEDURE

- Ensure that you have the correct bearing, hydraulic nut, sleeve (if used), and tools.
- 2. Inspect the shaft's condition and dimensions
- 3. Record the following items from tables provided by the manufacturer:
 - the internal clearance specification for the bearing
 - the clearance reduction, starting pressure, and pushup distance for mounting
- Using feeler gauges, measure and verify the unmounted internal clearance of the bearing. Record this measurement.



- Clean the mating parts. Apply a thin film of low viscosity oil on the shaft and sleeve (if used).
- Position the sleeve (if used), bearing, and any other parts (spacer, seals, etc.) loosely on the shaft as close as possible to the final desired installed position.
- Install the hydraulic nut with the plunger toward the bearing. Turn until snug against the bearing. A bar spanner supplied with the hydraulic nut can be used to further tighten by hand. Install the spanner into the shallow hole on the outer diameter of the nut.



- Once the nut is snug, install the dial indicator and connect the hydraulic pump to the nut.
- Increase pressure to the hydraulic nut until the starting pressure is achieved. Zero the dial indicator.
- 10. Increase pressure to the hydraulic nut while measuring the internal clearance at regular intervals.



- 11. Continue to increase pressure until clearance reduction is achieved using the pushup distance as a guide.
- 12. Measure the final clearance and record this value to keep with installation details.
- 13. Release the pressure, measure the internal clearance to verify that it didn't change, and remove the dial indicator. Using the bar spanner, tighten the hydraulic nut to push in the plunger and return oil to the pump.
- 14. Disconnect the hydraulic pump and remove the hydraulic nut.
- 15. Install the lock washer and lock nut (the tapered side of the washer goes against the beveled side of the nut). Using the spanner wrench, tighten the nut against the bearing until snug and bend the nearest tab of the washer into a slot on the OD of the nut. If a locking clamp is used instead of a lock washer (size 44 and larger) locate the nearest locking slot so the clip fits into the notch in the adapter sleeve.





MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS WITH ADAPTER SLEEVE

Method: lock nut Shaft: cylindrical Bearing: tapered bore Sleeve: adapter

PROCEDURE

Begin by executing Steps 1 to 7 of Handling Procedure - Adapter Sleeves on page B19, then continue with the following steps.

 Thread the lock nut onto the adapter sleeve without the lock washer to prevent damage to the lock washer tang due to application of heavy torque during drive-up. Advance the lock nut with the spanner wrench until it touches the bearing inner ring end face. From the position where the lock nut touches the bearing inner ring end face, with the spanner wrench, continue to turn the lock nut, stopping as soon as the turning torque of the spanner wrench increases.

For a straight shaft without shoulder, back off the lock nut a little to adjust the axial position to match the specified bearing span. After axial position adjustment, turn the lock nut again with the spanner wrench and stop as soon as the turning torque increases and/or the sleeve no longer spins on the shaft. This will be the starting point for the bearing clearance adjustment Refer to "Radial Clearance Reduction Method" on Page B11 for step 10

- Find the nominal bore and clearance symbol of the bearing being mounted, then confirm the target **Reduction in Radial Internal Clearance** (specified value) listed in **Table 2** on **page B12**.
 - For normal (CN) clearance, target the middle of the reduction range
 - For C3 or C4 clearance, target the upper half of the reduction range
 - For light or normal loads, target the lower half of the reduction range
 - > For heavy or shock loads, target the upper half of the reduction range

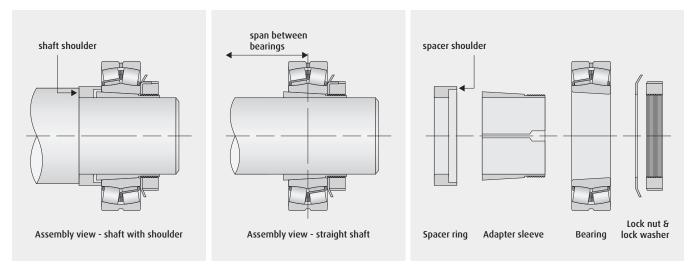


Fig. 15 - Spherical Roller Bearing Mounted with Adapter Sleeve on Cylindrical Shaft - Lock Nut Method



11. Turn the lock nut, measure radial internal clearance again, and repeat this operation until the radial internal clearance varies. Record this new radial clearance value, then calculate the difference between the measured initial value and the new measured value. If the obtained difference is less than the target **Reduction in** Radial Internal Clearance, continue to gradually drive the bearing up the tapered adapter by turning the nut, stopping at regular intervals to re-measure the bearing internal clearance. Repeat this operation until the target value is obtained.

Be careful to avoid driving the bearing up too far onto the tapered sleeve. If the clearance reduction amount exceeds the specified value, it may cause an improper interference and clearance that could result in inner ring fracture, abnormal temperature rise or seizure during bearing operation.





Refer to "Methods to Secure Lock Nut" on Page B20 for step 12

- 12. When the target **Reduction in Radial Internal Clearance** is obtained, secure the lock nut by using either a lock washer or lock plate.
- 13. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.

MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS WITH ADAPTER SLEEVE

Method: hydraulic nut Shaft: cylindrical Bearing: tapered bore Sleeve: adapter

PROCEDURE

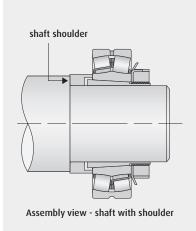
Begin by executing Steps 1 to 7 of Handling Procedure - Adapter Sleeves on page B19, then continue with the following steps.

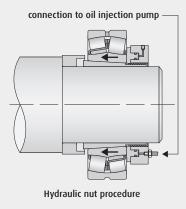
- Thread the hydraulic nut onto the adapter with the plunger toward the bearing. Turn until snug against the bearing. A bar spanner supplied with the hydraulic nut can be used to further tighten by hand. Install the spanner into the shallow hole on the outer diameter of the nut.
- Once the nut is snug, install the dial indicator and connect the hydraulic pump to the nut.
- Increase pressure to the hydraulic nut until the starting pressure is achieved. Zero the dial indicator. This is the starting point for adjustment of the radial internal clearance.

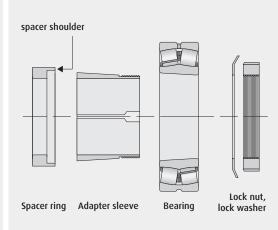
Refer to "Axial Drive-up Method" on Page B13 for step 11

- Confirm the target Reduction in Radial Internal Clearance listed in Tables 3.1 to 3.9 on pages B13 to B17.
- 12. Increase pressure to the hydraulic nut while measuring the internal clearance at regular intervals.
- 13. Continue to increase pressure until clearance reduction is achieved using the drive-up distance as a guide.

Fig. 16 - Spherical Roller Bearing Mounted with Adapter Sleeve on Cylindrical Shaft - Hydraulic Nut Method











- 14. Measure the final clearance and record this value to keep with installation details.
- 15. Release the pressure, measure the internal clearance to verify that it didn't change, and remove the dial indicator. Using the bar spanner, tighten the hydraulic nut to push in the plunger and return oil to the pump.
- 16. Disconnect the hydraulic pump and remove the hydraulic nut.
- 17. Mount the lock nut with the lock washer or lock plate.
- 18. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.





Refer to "Methods to Secure Lock Nut" on Page B20 for step 17

MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS WITH ADAPTER SLEEVE

Method: oil injection Shaft: cylindrical Bearing: tapered bore Sleeve: adapter

Some adapter sleeves have oil holes (oil ducts) to assist in bearing mounting and dismounting. High pressure oil is injected via a hand operated pump into the oil hole of the adapter sleeve during mounting to temporarily expand the bearing inner ring, reducing friction. This reduces the torque necessary to turn the lock nut during drive-up of the bearing onto the adapter. For this approach to be effective, the fit between the adapter sleeve and bearing must be adequate to maintain pressure between the two tapered surfaces.

PROCEDURE

Begin by executing Steps 1 to 7 of Handling Procedure - Adapter Sleeves on page B19, then continue with the following steps.

- Thread the lock nut onto the adapter sleeve without the lock washer to prevent damage to the lock washer tang due to application of heavy torque during drive-up. Advance the lock nut with the spanner wrench until it touches the bearing inner ring end face.
- From the position where the lock nut touches the bearing inner ring end face, with the spanner wrench, continue to turn the lock nut, stopping as soon as the turning torque of the spanner wrench increases.

For a straight shaft without shoulder, back off the lock nut a little to adjust the axial position to match the specified bearing span. After axial position adjustment, turn the lock nut again with the spanner wrench and stop as soon as the turning torque increases and/or the sleeve no longer spins on the shaft. This will be the starting point for the bearing clearance adjustment.

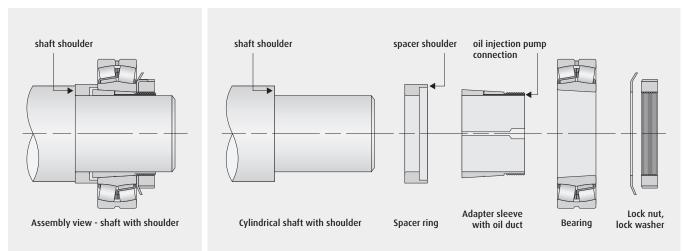


Fig. 17 - Spherical Roller Bearing Mounted with Adapter Sleeve on Cylindrical Shaft - Oil Injection Method



Refer to "Radial Clearance Reduction Method" on Page B11 for step 10

- Find the nominal bore and clearance symbol of the bearing being mounted, then confirm the target Reduction in Radial Internal Clearance (specified value) listed in Table 2 on page B12.
 - > For normal (CN) clearance, target the middle of the reduction range
 - > For C3 or C4 clearance, target the upper half of the reduction range
 - > For light or normal loads, target the lower half of the reduction range
 - > For heavy or shock loads, target the upper half of the reduction range
- 11. Connect the oil injection pump hose to the threaded oil hole (oil duct) of the adapter sleeve. Start the oil injection pump and begin incrementally turning the lock nut with the spanner wrench to drive up the bearing onto the adapter sleeve.

12. After each increment of drive-up, measure radial internal clearance again, and repeat this operation until the radial internal clearance changes. Record this new radial clearance value, then calculate the difference between the measured initial value and the new measured value. If this difference is less than the target **Reduction in Radial Internal** Clearance, continue to gradually drive up the bearing onto the tapered adapter with the spanner wrench (while running the oil injection pump), stopping at regular intervals to re-measure the bearing internal clearance. Repeat this operation until the target value is obtained.

Stop the pump, bleed down the oil injection pressure, and re-measure the bearing internal clearance to confirm the **Reduction in Radial Internal Clearance**. Re-start the pump and drive up the bearing further onto the adapter as necessary to reach the target **Reduction in Radial Internal Clearance** with oil injection pressure at zero.

Be careful to avoid driving the bearing up too far onto the tapered sleeve. If the clearance reduction amount exceeds the specified value, it may cause an improper interference and clearance that could result in inner ring fracture, abnormal temperature rise or seizure during bearing operation. 13. When the target **Reduction in Radial Internal Clearance** is obtained, disconnect the oil injection pump hose from the hydraulic nut and stop turning the lock nut. Mount the lock nut with the lock washer or lock plate.

Refer to "Methods to Secure Lock Nut" on Page B20 for step 13

14. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.

MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS WITH WITHDRAWAL SLEEVE

Method: lock nut Shaft: cylindrical Bearing: tapered bore Sleeve: withdrawal

PROCEDURE

Begin by executing Steps 1 to 8 of Handling Procedure - Withdrawal Sleeves on page B19, then continue with the following steps.

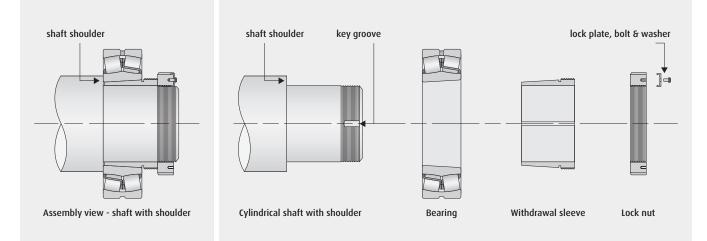
 Thread the lock nut onto the shaft and turn it with the spanner wrench until it contacts the bearing inner ring.

- 10. With the spanner wrench, continue to turn the lock nut, stopping as soon as the turning torque increases and/ or the sleeve no longer spins on the shaft. This is the starting point for adjustment of the radial internal clearance.
- Find the nominal bore and clearance symbol of the bearing being mounted, then confirm the target Reduction in Radial Internal Clearance (specified value) listed in Table 2 on page B12.
 - For normal (CN) clearance, target the middle of the reduction range
 - > For C3 or C4 clearance, target the upper half of the reduction range

Refer to "Radial Clearance Reduction Method" on Page B11 for step 11

- > For light or normal loads, target the lower half of the reduction range
- > For heavy or shock loads, target the upper half of the reduction range

Fig. 18 - Spherical Roller Bearing Mounted with Withdrawal Sleeve on Cylindrical Shaft - Lock Nut Method





12. Turn the lock nut, measure radial internal clearance again, and repeat this operation until the radial internal clearance varies. Record this new radial clearance value, then calculate the difference between the measured initial value and the new measured value. If the obtained difference is less than the target Reduction in Radial Internal Clearance, continue to gradually push the bearing onto the tapered adapter by turning the nut, stopping at regular intervals to re-measure the bearing internal clearance. Repeat this operation until the target value is obtained.

Be careful to avoid driving the bearing up too far onto the tapered sleeve. If the clearance reduction amount exceeds the specified value, it may cause an improper interference and clearance that could result in inner ring fracture, abnormal temperature rise or seizure during bearing operation.





Refer to "Methods to Secure Lock Nut" on Page B20 for step 13

- 13. When the target **Reduction in Radial Internal Clearance** is obtained, secure the lock nut by using either a lock washer or lock plate.
- 14. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.

MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS WITH WITHDRAWAL SLEEVE

Method: hydraulic nut Shaft: cylindrical Bearing: tapered bore Sleeve: withdrawal

PROCEDURE

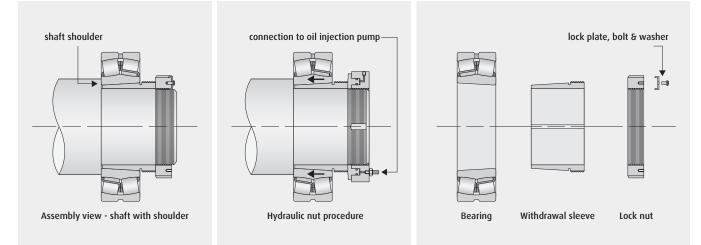
Begin by executing Steps 1 to 8 of Handling Procedure - Withdrawal Sleeves on page B19, then continue with the following steps.

- Thread the hydraulic nut onto the shaft with the plunger toward the bearing. Turn until snug against the withdrawal sleeve. A bar spanner supplied with the hydraulic nut can be used to further tighten by hand. Install the spanner into the shallow hole on the outer diameter of the nut.
- 10. Once the nut is snug, install the dial indicator and connect the hydraulic pump to the nut.
- Increase pressure to the hydraulic nut until the starting pressure is achieved. Zero the dial indicator. This is the starting point for adjustment of the radial internal clearance.

Refer to "Axial Drive-up Method" on Page B13 for step 12

- 12. Confirm the target **Reduction in Radial Internal Clearance** listed in **Tables 3.1 to 3.9** on **pages B13 to B17**.
- 13. Increase pressure to the hydraulic nut while measuring the internal clearance at regular intervals.

Fig. 19 - Spherical Roller Bearing Mounted with Withdrawal Sleeve on Cylindrical Shaft - Hydraulic Nut Method







- 14. Continue to increase pressure until clearance reduction is achieved using the drive-up distance as a guide.
- 15. Measure the final clearance and record this value to keep with installation details.
- 16. Release the pressure, measure the internal clearance to verify that it didn't change, and remove the dial indicator. Using the bar spanner, tighten the hydraulic nut to push in the plunger and return oil to the pump.
- 17. Disconnect the hydraulic pump and remove the hydraulic nut.





Refer to "Methods to Secure Lock Nut" on Page B20 for step 18

- 18. Mount the lock nut with the lock washer or lock plate.
- 19. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.

MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS WITH WITHDRAWAL SLEEVE

Method: oil injection Shaft: cylindrical Bearing: tapered bore Sleeve: withdrawal

Some withdrawal sleeves have oil holes (oil ducts) to assist in bearing mounting and dismounting. High pressure oil is injected via a hand operated pump into the oil hole of the withdrawal sleeve during mounting to temporarily expand the bearing inner ring, reducing friction. This reduces the torque necessary to turn the lock nut during drive-up of the bearing onto the adapter. For this approach to be effective, the fit between the withdrawal sleeve and the shaft and bearing must be adequate to maintain pressure between the surfaces. The withdrawal sleeve must be held onto the shaft by an end plate or end cap with a cutout to allow access to the oil port of the withdrawal sleeve. The end plate or cap is secured to the shaft with bolts that thread into holes cut into the shaft end. A nut cannot be easily used here, since it will block the oil port of the withdrawal sleeve.

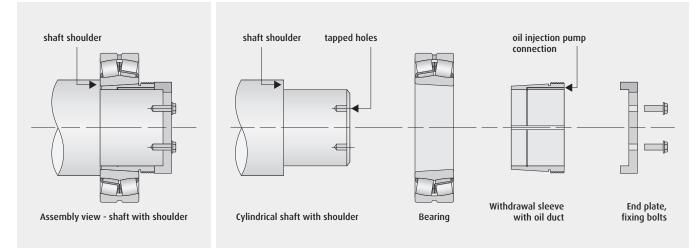
The end plate or cap bolts are used to drive up the bearing onto the withdrawal sleeve, setting the radial internal clearance. It is not unusual for the bolt torque to be high, so use bolts with appropriate strength.

PROCEDURE

Begin by executing Steps 1 to 8 of Handling Procedure - Withdrawal Sleeves on page B19, then continue with the following steps.

- To facilitate connection of the oil injection pump hose, orient the cutout on the end cap to match the oil hole on the removable sleeve. Mount the end cap on the shaft with the fixing bolts. If spring washers are used with the fixing bolts, insert the spring washers at this time.
- 10. Tighten all the bolts finger-tight, then starting with one bolt, tighten until a torque increase is felt. Next, tighten the bolt opposite the first bolt until a torque increase is felt. Continue with the remaining bolts, alternating from one side of the end cap to the other until all of the bolts are tightened to the same torque.

Fig. 20 - Spherical Roller Bearing Mounted with Withdrawal Sleeve on Cylindrical Shaft - Oil Injection Method





Refer to "Radial Clearance Reduction Method" on Page B11 for step 11

- Find the nominal bore and clearance symbol of the bearing being mounted, then confirm the target **Reduction in Radial Internal Clearance** (specified value) listed in **Table 2** on **page B12**.
 - For normal (CN) clearance, target the middle of the reduction range
 - > For C3 or C4 clearance, target the upper half of the reduction range
 - > For light or normal loads, target the lower half of the reduction range
 - For heavy or shock loads, target the upper half of the reduction range

- 12. Evenly tighten the end cap bolts to drive the withdrawal sleeve further into the bearing, then measure radial internal clearance again. Repeat this operation until the radial internal clearance varies. Record this new radial clearance value.
- 13. Connect the oil injection pump hose to the threaded oil hole (oil duct) on the withdrawal sleeve. Start the oil injection pump and begin incrementally driving up the bearing onto the withdrawal sleeve by evenly tightening the end cap bolts.
- 14. After each increment of drive-up, measure radial internal clearance again. Record this new radial clearance value, then calculate the difference between the measured initial value and the new measured value. If this difference is less than the target Reduction in Radial **Internal Clearance** continue to gradually drive the withdrawal sleeve into the bearing by evenly tightening the end plate or cap bolts (while running the oil injection pump), stopping at regular intervals to re-measure the bearing internal clearance. Repeat this operation until the target value is obtained.

Stop the pump, bleed down the oil injection pressure, and re-measure the bearing internal clearance to confirm the **Reduction in Radial Internal Clearance**. Re-start the pump and drive up the bearing further onto the adapter as necessary to reach the target **Reduction in Radial Internal Clearance** with oil injection pressure at zero.

Be careful to avoid driving the bearing up too far onto the withdrawal sleeve. If the clearance reduction amount exceeds the specified value, it may cause an improper interference and clearance that could result in inner ring fracture, abnormal temperature rise or seizure during bearing operation.

- 15. When the specified value is obtained, disconnect the oil injection pump hose from the hydraulic nut and stop tightening the end cap bolts. If the fixing bolts have holes for safety wire drilled in their heads, insert safety wire to secure the bolts against loosening.
- 16. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.

MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS - DIRECT SHAFT MOUNT

Method: lock nut Shaft: tapered Bearing: tapered bore Sleeve: none

PROCEDURE

- 1. Wipe the surface of the shaft with clean oil to remove dirt.
- Verify that the shaft taper is within specification. Use a sine bar and bluing compound to facilitate measurements of the taper's pitch and surface. The contact area should be at least 80%. Refer to Checking of Tapered Shafts on page B51.
- Measure the bearing internal clearance and record the measured clearance value. This is the Measured Initial Clearance.
- Mount the bearing with the taper oriented to match the shaft taper. For shafts with shoulders for use with spacers (see Fig. 21), proceed with bearing adjustment without the spacer installed. The spacer will be installed after radial clearance adjustment of the bearing.
- Thread the lock nut onto the shaft without the lock washer to prevent damage to the lock washer tang due to application of heavy torque during drive-up. Advance the lock nut with the spanner wrench until it touches the bearing inner ring end face.

6. From the position where the lock nut touches the bearing inner ring end face, with the spanner wrench, continue to turn the lock nut, stopping as soon as the turning torque of the spanner wrench increases. This will be the starting point for the bearing clearance adjustment.





- Find the nominal bore and clearance symbol of the bearing being mounted, then confirm the target Reduction in Radial Internal Clearance (specified value) listed in Table 2 on page B12.
 - For normal (CN) clearance, target the middle of the reduction range
 - For C3 or C4 clearance, target the upper half of the reduction range
 - > For light or normal loads, target the lower half of the reduction range
 - > For heavy or shock loads, target the upper half of the reduction range





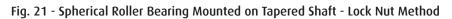
Refer to "Radial Clearance Reduction Method" on Page B11 for step 7

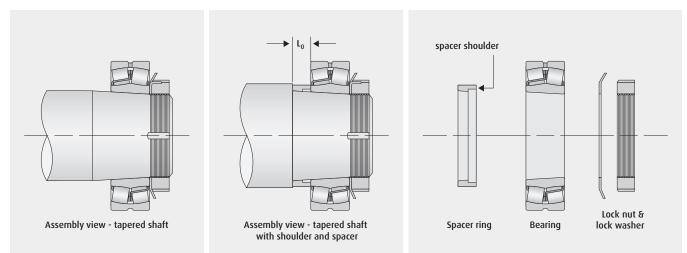
 Turn the lock nut, measure radial internal clearance again, and repeat this operation until the radial internal clearance varies. Record this new radial clearance value, then calculate the difference between the measured initial value and the new measured value. If the obtained difference is less than the target **Reduction in Radial Internal Clearance**, continue to gradually push the bearing onto the tapered shaft by turning the nut, stopping at regular intervals to re-measure the bearing internal clearance. Repeat this operation until the target value is obtained.

Be careful to avoid driving the bearing up too far onto the tapered shaft. If the clearance reduction amount exceeds the specified value, it may cause an improper interference and clearance that could result in inner ring fracture, abnormal temperature rise or seizure during bearing operation.

*If a spacer ring will be used in the final assembly, proceed to **When a Spacer Ring is Used** on **page B37**. Refer to "Methods to Secure Lock Nut" on Page B20 for step 9

- When the target Reduction in Radial Internal Clearance is obtained, secure the lock nut by using either a lock washer or lock plate.
- 10. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.





MOUNTING BEARINGS WITH TAPERED BORES SPHERICAL ROLLER BEARINGS - DIRECT SHAFT MOUNT

Method: lock nut Shaft: tapered Bearing: tapered bore Sleeve: none

WHEN A SPACER RING IS USED

Measure the gap (see "L₀", **Figure 21** on **page B36**) between the end face of the shaft shoulder and the end face of the bearing inner ring at 8 evenly distributed positions 45 degrees apart. Calculate the mathematical mean value of the measured dimensions.

Measure the width of the spacer ring at 8 evenly distributed positions and calculate the mathematical mean value of the spacer ring width.

Compare the mathematical mean value of the gap and the spacer ring width to determine whether the spacer ring width matches the gap width. If the spacer ring is wider than the gap, it must be ground to match the width of the gap. If the spacer is already narrower than the gap width, a new spacer ring must be made to match the width of the gap.





After confirming the correct width of the spacer ring, perform the following steps.

- Back off the lock nut with a spanner wrench, leaving the lock nut still threaded onto the end of the shaft.
- 10. Temporarily remove the bearing using a bearing puller. Mount a 3-jaw puller plate between the shaft shoulder and the bearing. The puller plate must only contact the inner ring of the bearing, not the outer ring. Set up the bearing puller to pull on the puller plate while the threaded shaft pushes against the end of the shaft. Use a safety net as a preventative measure against any parts breaking free while pulling.
- 11. With the bearing loose, completely remove the lock nut and remove the bearing from the shaft.
- 12. Mount the spacer ring using the orientation shown in **Figure 21**.
- Re-install the bearing and lock nut. The bearing is located in the proper position when it is pushed up tight to the correct spacer width.
- 14. Secure the lock nut by using either a lock washer or lock plate.
- 15. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.



Method: hydraulic nut Shaft: tapered Bearing: tapered bore Sleeve: none

PROCEDURE

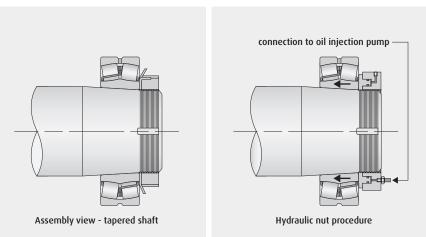
- 1. Wipe the surface of the shaft with clean oil to remove dirt.
- Verify that the shaft taper is within specification. Use a sine bar and bluing compound to facilitate measurements of the taper's pitch and surface. The contact area should be at least 80%. Refer to Checking of Tapered Shafts on page B51.
- Measure the bearing internal clearance and record the measured clearance value. This is the Measured Initial Clearance.
- 4. Mount the bearing with the taper oriented to match the shaft taper.
- 5. Thread the hydraulic nut onto the shaft with the plunger toward the bearing. Turn until snug against the bearing. A bar spanner supplied with the hydraulic nut can be used to further tighten by hand. Install the spanner into the shallow hole on the outer diameter of the nut.
- Once the nut is snug, install the dial indicator and connect the hydraulic pump to the nut.

- Increase pressure to the hydraulic nut until the starting pressure is achieved. Zero the dial indicator. This is the starting point for adjustment of the radial internal clearance.
- Confirm the target Reduction in Radial Internal Clearance listed in Tables 3.1 to 3.9 on pages B13 to B17.
- Increase pressure to the hydraulic nut while measuring the internal clearance at regular intervals.
- 10. Continue to increase pressure until clearance reduction is achieved using the drive-up distance as a guide.
- 11. Measure the final clearance and record this value to keep with installation details.

Refer to "Axial Drive-up Method" on Page B13 for step 8

- 12. Release the pressure, measure the internal clearance to verify that it didn't change, and remove the dial indicator. Using the bar spanner, tighten the hydraulic nut to push in the plunger and return oil to the pump.
- 13. Mount the lock nut with the lock washer or lock plate.
- 14. Check to ensure that the bearing outer ring and shaft can be easily rotated by hand.

Fig. 22 - Spherical Roller Bearing Mounted on Tapered Shaft - Hydraulic Nut Method



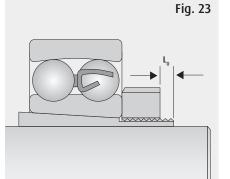
MOUNTING BEARINGS WITH TAPERED BORES SELF-ALIGNING BALL BEARINGS WITH ADAPTER SLEEVE

Method: axial drive-up

PROCEDURE

Begin by executing Steps 1 to 7 of Handling Procedure - Adapter Sleeves on page B19, then continue with the following steps.

- Slide bearing, lock washer and lock nut onto sleeve and tighten nut with a spanner wrench until all slackness is removed.
- Measure distance from end tapered sleeve to the face of lock nut or to the face of the inner ring and note the dimension.
- Refer to Tables 5 and 6 on pages
 B41 42 and tighten the lock nut until the bearing has moved the required distance up the taper of the sleeve indicated by the reduction or increase in the measured distance originally noted.



11. A self-aligning ball bearing with normal clearance when adjusted correctly should rotate freely but should have some resistance to swiveling.



12. Align one tab on the lock washer with a slot in the lock nut and bend it into the slot. If no tabs line up with the slots, slightly tighten the lock nut until one aligns. Never back off the nut to line up the tab with the slot.

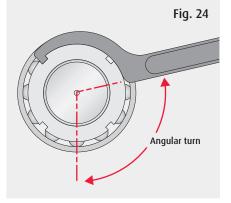


Method: tightening angle

PROCEDURE

Begin by executing Steps 1 to 7 of Handling Procedure - Adapter Sleeves on page B19, then continue with the following steps.

- Slide bearing, lock washer and lock nut onto sleeve and tighten nut with a spanner wrench until all slackness is removed.
- Refer to Tables 5 and 6 on pages
 B41 42 and tighten the lock nut through the required angle, taken from chart.



- 10. A self-aligning ball bearing with normal clearance when adjusted correctly should rotate freely but should have some resistance to swiveling.
- 11. Align one tab on the lock washer with a slot in the lock nut and bend it into the slot. If no tabs line up with the slots, slightly tighten the lock nut until one aligns. Never back off the nut to line up the tab with the slot.

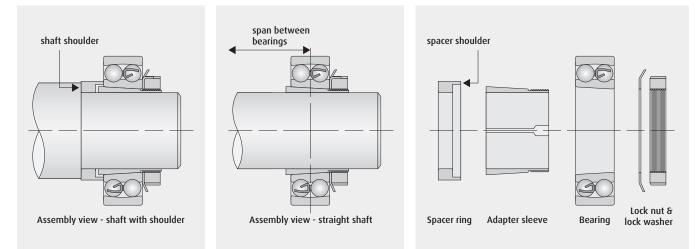


Fig. 25 - Self-aligning Ball Bearing Mounted with Adapter Sleeve on Cylindrical Shaft - Lock Nut Method

MOUNTING BEARINGS WITH TAPERED BORES

SELF-ALIGNING BALL BEARINGS WITH ADAPTER SLEEVE

BORE DIAMETER	INCH LOCK	AXIAL DISPLACEMENT (INCH)			ANGULAR TURN (DEGREES)				
(MM)	(MM) NUT	12K	13K	22К	23К	12K	13K	22К	23К
20	N04	0.006	0.006	0.007	0.006	70	70	75	70
25	N05	0.007	0.007	0.008	0.007	80	85	90	80
30	N06	0.007	0.007	0.008	0.007	45	45	50	45
35	N07	0.009	0.009	0.010	0.009	60	55	60	55
40	N08	0.009	0.009	0.010	0.009	60	55	60	55
45	N09	0.010	0.010	0.011	0.010	65	65	65	60
50	N10	0.010	0.010	0.011	0.010	65	65	65	60
55	N11	0.013	0.013	0.013	0.012	80	80	85	75
60	N12	0.013	0.013	0.013	0.012	80	80	85	75
65	N13	0.013	0.013	0.013	0.012	80	80	85	75
70	N14	0.017	0.017	0.017	0.016	105	105	110	100
75	AN15	0.017	0.017	0.017	0.016	70	70	70	65
80	AN16	0.017	0.017	0.017	0.016	70	70	70	65
85	AN17	0.020	0.019	0.020	0.019	85	80	85	80
90	AN18	0.020	0.019	0.020	0.019	85	80	85	80
95	AN19	0.020	0.019	0.020	0.019	85	80	85	80
100	AN20	0.020	0.019	0.020	0.019	85	80	85	80
110	AN22	0.024	0.023	0.025	-	100	95	105	-

Table 5 - Axial and Angular Drive-up for Self-aligning Ball Bearings - Inch Lock Nut



BORE DIAMETER	INCH LOCK	AXIAL DISPLACEMENT (INCH)				ANGULAR TURN (DEGREES)			
(MM)	NUT	12K	13K	22К	23К	12K	13K	22К	23К
20	KM4	0.160	0.160	0.170	0.160	55	55	60	55
25	KM5	0.180	0.190	0.200	0.180	40	45	45	40
30	KM6	0.180	0.190	0.200	0.180	40	45	45	40
35	KM7	0.240	0.230	0.250	0.220	55	55	60	50
40	KM8	0.240	0.230	0.250	0.220	55	55	60	50
45	KM9	0.260	0.260	0.270	0.250	60	60	60	60
50	KM10	0.260	0.260	0.270	0.250	60	60	60	60
55	KM11	0.330	0.320	0.340	0.310	55	55	60	55
60	KM12	0.330	0.320	0.340	0.310	55	55	60	55
65	KM13	0.330	0.320	0.340	0.310	55	55	60	55
70	KM14	0.420	0.420	0.440	0.400	75	75	75	70
75	KM15	0.420	0.420	0.440	0.400	75	75	75	70
80	KM16	0.420	0.420	0.440	0.400	75	75	75	70
85	KM17	0.510	0.490	0.510	0.480	90	85	90	85
90	KM18	0.510	0.490	0.510	0.480	90	85	90	85
95	KM19	0.510	0.490	0.510	0.480	90	85	90	85
100	KM20	0.510	0.490	0.510	0.480	90	85	90	85
110	KM22	0.610	0.580	0.630	-	105	100	110	-

Table 6 - Axial and Angular Drive-up for Self-aligning Ball Bearings - Metric Lock Nut

MOUNTING PILLOW BLOCKS AND SEALS

Installing SAF series split pillow blocks

PROCEDURE

- Inspect the shaft condition for any burrs. Wipe the shaft with a clean cloth.
- Verify the diameter of the shaft.
 Refer to Table 9 on page C15 for the diameter tolerance of the shaft.
- Add seals to the inboard side of the shaft. This must be done prior to mounting the bearing. Refer to the seal mounting instructions for TER and OLB seals on page B46.

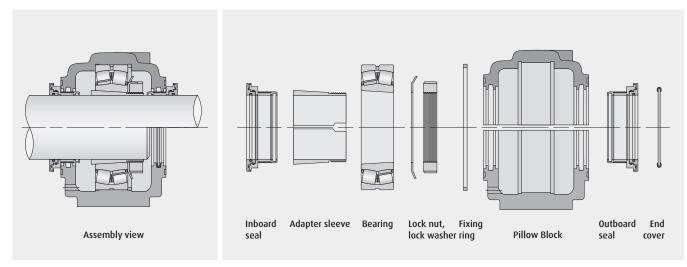


 Mount the bearing, referring to the various mounting instructions for spherical roller bearings and self-aligning ball bearings on pages B23 to B40.



- 5. Attach seal to the outboard side of the shaft.
- Position bottom half of the pillow block unit to its mounted location. Carefully lower the mounted bearing and seals into the unit.

Fig. 26 - SAF Pillow Block Assembly with Spherical Roller Bearing and OLB Seal













- If grease lubrication is to be used, apply grease to the bearing. Work the grease into the bearing and add until the bottom half of the pillow block is about 1/3 to 1/2 full.
- Identify if the bearing will be used as a fixed or expansion (float) set. If the bearing is fixed, leave the fixing ring in the unit. If it is an expansion end, remove and discard the fixing ring and ensure the bearing is centered in the housing seat.
- Attach the upper half of the pillow block unit to the housing. Lightly apply oil to the bearing contact surfaces. (Note: caps and bases of pillow block units are not interchangeable). Tighten bolts to the torque specified in Table 7 on page B45.

MOUNTING PILLOW BLOCKS AND SEALS

Table 7 - Recommended Tightening Torque SAF Pillow Block

SAF PILLOW	RECOMMENDED TIGHTENING TORQUE FOR CAP BOLTS						
BLOCK SIZE	Bolt Size	Qty	Torque (ft-lbf)				
509	3/8-16 UNC x 2	2	26				
510	3/8-16 UNC x 2	2	26				
511	1/2-13 UNC x 2 1/4	2	50				
513	1/2-13 UNC x 2 1/4	2	50				
515	1/2-13 UNC x 2 1/4	2	50				
516	1/2-13 UNC x 2 1/4	4	50				
517	1/2-13 UNC x 3	4	50				
518	1/2-13 UNC x 3	4	50				
520	5/8-11 UNC x 3 1/2	4	100				
522	5/8-11 UNC x 3 1/2	4	100				
524	5/8-11 UNC x 4	4	100				
526	3/4-10 UNC x 4 1/2	4	175				
528	3/4-10 UNC x 4 1/2	4	175				
530	3/4-10 UNC x 5	4	175				
532	3/4-10 UNC x 5	4	175				
534	1-8 UNC x 6 1/2	4	245				
536	1-8 UNC x 6 1/2	4	245				
538	1-8 UNC x 6 1/2	4	245				
540	1-8 UNC x 7	4	245				
544	1-8 UNC x 7 1/2	4	245				

Table 8 - Recommended Initial Grease Fill SAF Pillow Block

SAF PILLOW	RECOMMENDED INITIAL GREASE FILL (OZ)				
BLOCK SIZE	Low Speed	High Speed			
509	2.2	1.8			
510	2.8	2			
511	3.7	2.5			
513	6.5	4			
515	8.3	5			
516	10	6			
517	12	7			
518	16	7.5			
520	23	15			
522	31	20			
524	37	22			
526	40	28			
528	52	32			
530	62	34			
532	75	40			
534	90	55			
536	120	65			
538	150	75			
540	200	85			
544	250	125			

For data pertaining to additional series SAF pillow blocks, contact NSK.

(1) Low speed applications Typically involve conveyors. Generally, bearings exposed to weather benefit from a relatively full grease charge to deter moisture ingress.

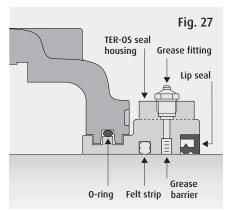
(2) Higher speed applications do not require as much grease, as purging of excess will occur at the seals naturally.

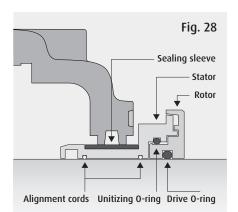
Installing TER seals (Fig. 27)

PROCEDURE

- Soak the felt strips in a lightweight oil for a few minutes. After soaking, insert into the internal seal groove nearest to the bearing. The strips may need to be trimmed to length.
- 2. Hand pack the grease groove with the same grease to be used in the bearing.
- Lightly grease or oil the shaft and bore of the inboard seal to protect the shaft. Carefully slide the inboard seal onto the shaft, but clear of the bearing area.
- 4. Finish mounting the bearing onto the shaft.
- 5. Apply grease by hand to the seal grooves of the housing where the TER-OS seal will fit. This will help begin to form the contamination barrier.
- Lower the assembled bearing, seal and shaft into the housing base. Adjust the seal position along the shaft to fit into the designated seal groove. Lubricate the bearing as specified in Table 8.

- Attach the housing cap and tighten the cap bolts as specified in Table 7. The seal should be a tight fit.
- Add a small amount of grease to the seal lubrication fittings to ensure the internal cavities of the seal are full.
 Slight grease purge from the seal showing fresh grease is preferred.
- Relubricate the seals as often as needed. Fresh grease purge is the best way to prevent contaminant entry.





Installing OLB seals (Fig. 28)

PROCEDURE

- In the case of a damaged bore internal diameter surface, and if the seal design does not include a stator o-ring, apply a thin layer of RTV sealant onto the stator insertion outside diameter surface.
- Line up the contaminant exclusion port with the 6 o'clock position on the cover or housing. Using a hand arbor press or direct even pressure, apply force on the inner half of the rotor face until the bearing protective device stops at the location shoulder.
- Lightly lubricate the shaft with the lubrication supplied. If more lubrication is needed, use a diluted mixture of liquid hand soap and water. Do not use a grease-based lubricant. While holding the cover assembly or seal alone, push on the rotor face and slide the cover assembly into position.
- 4. Secure the cover into place. Push firmly on the rotor to ensure full rotor/stator engagement.
- 5. Turn the shaft to confirm smooth operation.

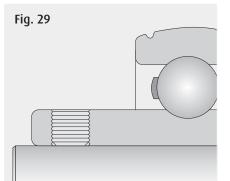
Note: If the rotor and stator become separated, the rotor can be re-engaged with the stator after the cover is secured in place.

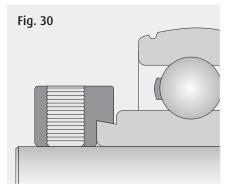
MOUNTING BALL BEARING UNITS

Installing set screw locking arrangements (Fig.29)

PROCEDURE

- Loosen set screws clear of the bearing bore and slide the mounted unit onto the shaft.
- Install the mounting bolts and tighten to secure mounted unit to the equipment.
- Tighten set screws on the bearing inner ring to the recommended torque. (see Table 9)

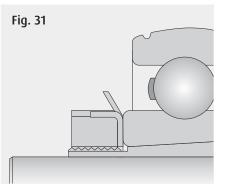




Installing eccentric locking collar arrangements (Fig. 30)

PROCEDURE

- Remove the eccentric locking collar and slide the mounted unit onto the shaft.
- Install the mounting bolts and tighten to secure mounted unit to the equipment.
- Loosen the eccentric locking collar set screw clear of the collar bore and install onto bearing unit.
- 4. Engage the eccentric locking collar in the direction of shaft rotation.
- 5. Tighten eccentric locking collar with a drift pin and a small hammer.
- Tighten eccentric locking collar set screw to the recommended torque. (see Table 9)



Installing tapered adapter sleeve arrangements (Fig. 31)

PROCEDURE

- 1. Clean the shaft, sleeve and bearing bore of any oil or grease.
- 2. Install the mounted unit onto the equipment.
- Install the mounting bolts and tighten to secure mounted unit to the equipment.
- Position the shaft within the unit and tighten up the lockup by hand. If the sleeve assembly turns on the shaft, tap the sleeve into the bearing to obtain a positive grip.
- Use the appropriate spanner wrench to tighten the lock nut to the recommended torque. (see Table 10)
- Check that the bearing rotates freely to ensure that the internal clearance has not been completely removed.
- Secure the nut with the appropriate locking tab. If no tab aligns with the locking slot in the nut, tighten the nut slightly until they align. Do not loosen the nut.





SET SCREW SIZE	SOCKET / ALLEN KEY SIZE		ED MAXIMUM IG TORQUE	SET SCREW MAXIMUM AXIAL LOAD		
5126		newton metres (Nm)	lbf-inches	newtons (N)	lbf	
1/4 UNF	1/8"	6.8	60	2,500	560	
5/16 UNF	5/32"	12.4	110	3,500	785	
3/8 UNF	3/16"	22.6	200	4,500	1,010	
7/16 UNF	7/32"	31.6	280	7,500	1,685	
1/2 UNF	1/4"	45.2	400	9,000	2,025	
5/8 UNF	5/16"	53.9	477	15,000	3,370	
M6 x 0.75	3 mm	5.7	50	2,500	560	
M8 x 1.00	4 mm	12.4	110	3,500	785	
M10 x 1.25	5 mm	27.1	240	5,000	1,235	
M12 x 1.50	6 mm	38.4	340	8,000	1,800	
M16 x 1.50	8 mm	53.9	477	15,000	3,370	

Table 9 - Set Screw Tightening Torques and Maximum Axial Loads





SLEEVE BORE SIZE	E	TIGHTENING TORQUES		
mm	inch	inch	Nm	lbf-inches
20	3/4		30	265
25	15/16	1	40	355
30	1 1/8	1 3/16	50	440
35	1 1/4	1 3/8	60	530
40	1 7/16	1 1/2	65	575
45	1 11/16	1 3/4	75	660
50	1 15/16	2	85	750

It is advisable to the check tightness of the installation after 100 hours of operation.

METHODS OF DISMOUNTING

SELECTION OF DISMOUNTING METHODS

Bearings are typically removed for periodic inspection, lubrication, or for replacement. If the bearing being removed is going to be used again, it is crucial to remove the bearing the correct way using the proper procedure to avoid damaging the bearing. The removal process can be determined from the bearing size and the initial mounting arrangement.

There are four different types of mounting arrangements: cylindrical bore, tapered bore, adapter sleeve, and withdrawal sleeve. There are two basic removal methods, mechanical and thermal. Mechanical removal methods include pullers, presses and hydraulic nuts. Pullers are typically only used on small and medium sized bearings, while hydraulic removal methods are used on larger sized bearings or bearings with heavy press fits.

INTERFERENCE FITS - CYLINDRICAL SHAFTS

Bearings that have an inner diameter of up to 120 mm can be removed using a mechanical puller. In order to remove the bearing, the puller claws are clamped around the inner ring and a steady torque is then applied to the puller until the bearing is removed from the shaft. For bearing bores larger than 120 mm, it is recommended to use a hydraulic press to remove the bearing as the force required to remove the bearing is too great for that of a mechanical puller.

Table 11 - Methods of Bearing Dismounting

BEARING INNER RING SHAPE	SHAFT SHAPE AND FEAT	TURES	MOUNTING PARTS AND	WORKING METHOD	
	Shape	Features	Parts	Features	
cylindrical bore	cylindrical	 shaft with shoulder with or without oil duct 	→ with or without spacer		 bearing puller press oil injection pump + puller
tapered bore	tapered	 shaft with shoulder with or without oil duct 	 with or without spacer 		 bearing puller press oil injection pump + puller
tapered bore	cylindrical	> shaft with shoulder	 adapter sleeve with or without spacer 	 with or without oil duct 	 > dead-blow mallet > bearing puller > press > oil injection pump + puller
tapered bore	cylindrical	> shaft with shoulder	→ withdrawal sleeve	 with or without oil duct 	 nut hydraulic nut oil injection pump + nut



INTERFERENCE FITS - SHAFT AND HOUSING

For small to medium sized bearings with interference fits in the housing, these can be removed by inserting a sleeve in the housing and hammering the sleeve uniformly until the bearing is free from the housing. Larger bearings require hydraulic presses in order to remove.

For bearings with an interference fit on both the shaft and the housing, it is recommended to push the shaft out of the bearing with the bearing fixed into the housing.

DISMOUNTING TAPERED BORE BEARINGS

In order to remove small to medium sized bearings with tapered bores, the puller should engage and pull against the inner ring, as the interference fit is on the shaft. Centering the bearing puller is important for tapered bore bearing removal in order to help eliminate the risk of permanent damage and to allow for an easier bearing removal. The use of a lock nut when removing bearings from tapered bores is recommended to prevent the bearing from flying off the shaft.

DISMOUNTING FROM SLEEVES

For bearings with adapter sleeves, the bearing can be removed by installing a fixture to the shaft that locks the inner ring in place and then loosening the nut several turns. Then, the sleeve is then hammered uniformly using a suitable tool until the bearing and sleeve are removed.

For withdrawal sleeves, the removal nut is tightened. This procedure is often difficult, and so it is also possible to drill and tap bolt holes in the nut and withdraw the sleeve by tightening the bolts. The benefit of removal sleeves is that, if installed properly, they cause no damage to the bearing or shaft when removed.

HYDRAULIC NUTS

Hydraulic nuts can considerably reduce time and effort in bearing removal when compared to their mechanical puller counterparts. This type of removal method is typically used to remove medium and large sized bearings with a bore diameter greater than 120 mm. When using hydraulic nuts, it is important to wear proper Personal Protective Equipment (PPE) such as safety glasses, gloves, and protective footwear.

CLEANING AND REUSE

In order to determine if the removed bearing can be used again, the bearing must first be cleaned. This cleaning removes the grease and any other debris or particulates that may have found their way into the grease. For the initial cleaning, wash the bearing using an industrial safety-solvent, or petroleum-based solvent such as kerosene. Once the bearing has been washed with the solvent, drain the solution and then flush with hot, light oil and drain once more. Then proceed with the visual examination of the bearing to determine if it can be used again.

If the bearing is being sent to NSK's America's Technical Center for analysis, apply a light coating of rust preventative oil on the bearing then package and store the bearing in a dry, cool environment until it is shipped. If the bearing was removed for relubrication with new grease or oil, the new lubricant may be added to the bearing following the hot, light oil wash.

CHECKING SHAFTS AND HOUSINGS

CHECKING OF CYLINDRICAL SHAFTS

Dimensional check of shaft

Measure the shaft size at the place where the bearing will be mounted to confirm that the bearing size is correct. The measurement positions are shown in Figure 32. Use an outside micrometer.

Inspect the shaft outside surface - where the bearing was mounted for scratches, dents, rust or stepped wearing.

- > When there are scratches, dents or rust round the edges or remove with oil stone and/or sandpaper to smoothen the surface.
- > When there is stepped wearing after measuring the shaft, decide whether correction is possible.

Anticorrosive agent - apply after completion of check.

CHECKING OF TAPERED SHAFTS

Check the shaft shape - where the bearing will be mounted to confirm that its shape is correct. The measurement positions are shown in Figure 33. Use a taper gauge (sine-bar system).

Inspect the shaft outside surface - where the bearing was mounted for scratches, dents, rust or stepped wearing.

- > When there are scratches, dents or rust round the edges or remove with oil stone and/or sandpaper to smoothen the surface. If the area with rust to be corrected is wide, inspect the shape of the tapered zone by using a taper gauge. Apply a thin coat of bluing over the entire surface of the taper gauge bore face, insert it slowly after adjusting the taper gauge to the shaft center tapered shaft, and execute a run-in by moving back-and-forth. Pull the taper gauge out slowly when adjusting to the shaft center, observing where blue dye is attached to the surface of tapered shaft. If the blue area is larger than 80%, the shaft may be reused.
- > When there is stepped wearing after measuring the shaft, decide whether correction is possible.

Anticorrosive agent - apply after completion of check.

Fig. 32 - Checking Cylindrical Shafts

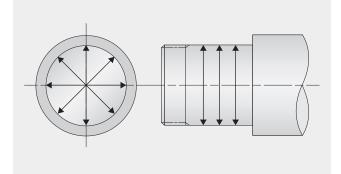
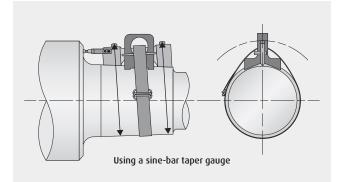


Fig. 33 - Checking Tapered Shafts





CHECKING OF HOUSING - INTEGRATED TYPE

Check the bore size of the housing - where the bearing will be mounted to confirm that the size is correct. The measurement position is shown in Figure 34. Use an inside micrometer.

Inspect the housing bore face - where the bearing was mounted for scratches, dents, rust or stepped wearing.

- > When there are scratches, dents or rust round the edges or remove with oil stone and/or sandpaper to smoothen the surface.
- > When there is stepped wearing from the dimensional check, decide whether correction and reuse are possible. In this case, if the measured value of the housing bore is within its tolerance, remove the stepped worn part with oil stone and/or sandpaper, etc. and smoothen the surface, then, reuse. If the stepped wearing is severe, either plate or apply thermal spraying to reconstitute to the correct housing size before reusing.

Anticorrosive agent - apply after completion of check.

CHECKING OF HOUSING - SPLIT TYPE

Check the bore size of the assembled housing - where the bearing will be mounted to confirm that the dimension is correct. The measurement position is shown in Figure 35. Use an inside micrometer.

Inspect the housing bore face - where the bearing was mounted for scratches, dents, rust or stepped wearing.

- > When there are scratches, dents or rust round the edges or remove with oil stone and/or sandpaper to smoothen the surface.
- > When there is stepped wearing from the dimensional check, decide whether correction is possible. If the measured value of housing bore is within its tolerance, remove the stepped worn portion with oil stone and/or sandpaper, smoothen the surface and reuse.
- > When stepped wear is severe, either plate or apply thermal spraying to reconstitute to the correct housing size and reuse.
- > When there is a step at the joint of the split housing halves, correction or a replacement housing is required.

Anticorrosive agent - apply after completion of check.

Fig. 34 - Checking Housings, Integrated Type

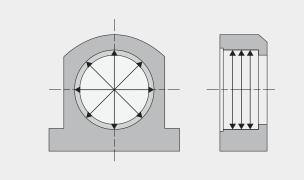
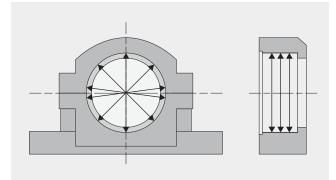


Fig. 35 - Checking Housings, Split Type



CHECKING SLEEVES AND LOCK NUTS

CHECKING ADAPTER AND WITHDRAWAL SLEEVES

After removal of the adapter or withdrawal sleeve, check the appearance as follows:

Inspect the sleeve threads - for crushed thread ridges or rust in thread valleys. If there is any indication of either, do not reuse.

Inspect the sleeve bore and outside surface - for scratches, dents, rust or uneven wearing.

- > When there are scratches, dents or rust round the edges or remove with oil stone and/or sandpaper to smoothen the surface. If dents are severe, do not reuse.
- > When uneven wear is found do not reuse.

Inspect the sleeve slot - for deformation or chips. If there is any indication of either, do not reuse.

Anticorrosive agent - apply after completion of check.

CHECKING LOCK NUTS

After removal of the lock nut, check the appearance as follows:

Inspect the lock nut threads - for crushed thread ridges or rust in thread valleys. If there is any indication of either, do not reuse.

Inspect the lock nut end face - for scratches, dents, rust or uneven wearing.

- When there are scratches, dents or rust round the edges or remove with oil stone and/or sandpaper to smoothen the surface. If dents or rust are severe, do not reuse.
- > When uneven wear is found do not reuse.

Inspect the lock nut slots for deformation. If found, do not reuse.

Anticorrosive agent - apply after completion of check.

CHECKING LOCK WASHER OR LOCK PLATE

After removal of the lock washer or lock plate, check the appearance for chips or severe deformation. If there is any indication of either, do not reuse.

CHECKING DAMAGED BEARINGS



In general, when a bearing is handled correctly it can be used for the duration of its fatigue life. Occasionally it may fail prematurely as a result of bearing damage. Such premature damage is often caused by inadequate consideration given to the fundamentals of mounting, handling, and lubrication, or inadequate compensation for contamination or thermal influences of the shaft and/or housing.

If a bearing is found to be damaged when dismounted, the cause should be thoroughly investigated. It may be difficult to determine the real cause of the trouble merely by the appearance of the damaged bearing, as several of the factors mentioned above may be working together to contribute to the damage.

Periodic maintenance and inspection reports should be reviewed for any indications of phenomena observed during operation. The condition of residual lubricant in the bearing should be carefully examined. The results of shaft, housing and sleeve inspections should be reviewed for possible associated cause of effect.

The potential for preventing reoccurrence increases dramatically with acquiring a complete understanding of the machinery, the operating conditions, the structure surrounding the bearing, and any warning signs before and after the trouble occurred.

Refer to **Section E: Troubleshooting / Bearing Damage** of this catalog for additional information. For assistance with diagnosing bearing damage and failure, and implementing effective solutions, contact NSK.





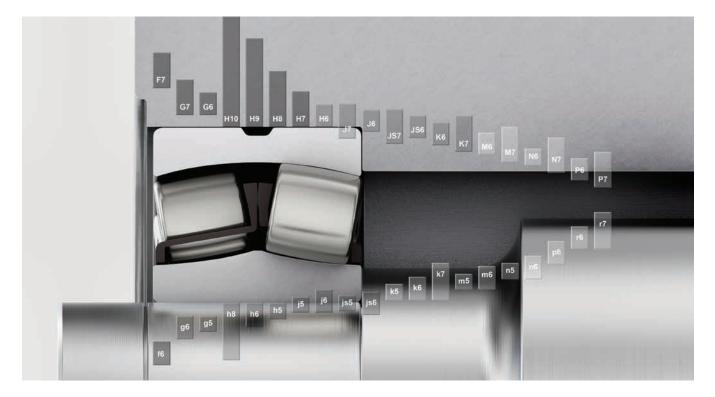
SECTION C:

SHAFT AND HOUSING FITS



SHAFT AND HOUSING FITS

For rolling bearings to achieve their full life expectancy, their inner and outer rings must be properly fitted to the shaft and the housing. Typically for the ring that rotates an interference fit is chosen, whereas the stationary ring will have a clearance or loose fit. The shaft and housing tolerances are selected by considering many factors: the magnitude of load, the temperature differences among the bearing, shaft and housing, the level of surface finishes, the shaft thickness, and the mounting / dismounting methods.



The image above is a liberal depiction of shaft and housing fits ranging from loose to tight. Recommended shaft and housing fits by bearing type and application, as well as calculated fit values, can be found throughout this section.



IMPORTANCE OF PROPER FITS

When properly mounting a rolling element bearing, there must be adequate interference to prevent harmful damage to the mating surfaces. Creep or fretting damage can occur without sufficient interference fits. This damage can cause debris from the mating surfaces to enter the interior of the bearing, causing denting, vibration, and shortened bearing life.

In order to mitigate the risk of creep it is important to have sufficient interference between components to firmly secure the rotating bearing ring to its mating component - inner ring to shaft, outer ring to housing. Snap rings and lock nuts are used to secure the bearing axially, but they will have little effect in preventing creep. Fits without interference can be used in certain operating conditions or for ease of mounting or dismounting. Anti-fretting paste is suggested for loose fits.

LOAD CONDITIONS AND FITS

LOAD CONDITIONS

Bearing loads are typically classified by the magnitude of the load and the direction of the load. With respect to magnitude, loads are classified as light, medium, or heavy. With respect to direction, they are classified as rotating, stationary, or indeterminate. The direction of the load does not apply to the bearing itself; rather it is intended to describe the means by which the load is acting on each of the bearing rings.

Whether an interference fit or a loose fit should be adopted depends entirely upon whether the load applied to the inner and outer rings is rotating or stationary. A "rotating load" is one where the loading direction on a bearing ring changes continuously regardless of whether the bearing ring itself rotates or remains stationary. On the other hand, a "stationary load" is one where the loading direction on a bearing ring is the same regardless of whether the bearing ring itself rotates or remains stationary. An " indeterminate load" is one that is impacted by unbalanced weight, vibration or shock, etc. that impacts the direction of the load in ways that cannot be easily predicted.

As an example, when the load direction on a bearing remains constant and the inner ring rotates and the outer ring stays fixed, a rotating load is applied to the inner ring and a stationary load to the outer ring. In the case that the majority of the bearing load is an unbalanced load due to rotation, even if the inner ring rotates and the outer ring stays fixed, a stationary load is applied to the inner ring and a rotating load to the outer ring (see Table 1).

Depending on the actual conditions, the situation is not usually as simple as described above. The loads may vary in complex ways with the load direction being a combination of fixed and rotating loads caused by mass, by imbalance, by vibration, and by power transmission. If the load direction on a bearing is highly irregular or a rotating load and stationary load are applied alternatively, such a load is called an indeterminate load. Table 1 - Rotating and Stationary Load of Inner Rings

Rotating load	Bearing load direction is constant, the inner ring rotates and the outer ring remains fixed
on inner ring	Inner ring remains fixed, the outer ring rotates, and the load direction rotates with the same speed as the outer ring (unbalanced load, etc.)
Stationary load	Outer ring remains fixed, the inner ring rotates, and the load direction rotates with the same speed as the inner ring (unbalanced load, etc.).
on inner ring	Bearing load direction is constant, the outer ring rotates, and the inner ring remains fixed.

The fit of a bearing ring on which a rotating load is applied should generally be an interference fit. If a bearing ring, on which a rotating load is applied, is mounted with a loose fit, the bearing ring may slip on the shaft or in the housing and, if the load is heavy, the fitting surface may be damaged or fretting corrosion may occur. The tightness of the fit should be sufficient to prevent the interference from becoming zero as a result of the applied load and a temperature difference between the inner ring and shaft or between the outer ring and housing during operation.

For large bearings, to avoid the difficulty of mounting and dismounting, sometimes a loose fit is adopted for the bearing ring on which a rotating load is applied. In such a case, the shaft material must be sufficiently hard, its surface must be well finished, and a lubricant needs to be applied to minimize damage due to slipping.

There is generally no problem with slipping between the shaft or housing for a bearing ring on which a stationary load is applied; therefore, a loose fit or transition fit can be used. The looseness of the fit depends on the accuracy required in use, temperature variations and the reduction in the load distribution range caused by bearing-ring deformation.



Table 2 - Load Conditions and Fits

OPERATING CONDITIONS	LOAD CONDITION	RECOMMENDED FITS			
UPERATING CONDITIONS	LOAD CONDITION	Inner Ring	Outer Ring		
Inner ring : rotating Outer ring : stationary Load : stationary	Rotating inner ring load Stationary outer ring load	Tight fit	Loose fit		
Inner ring : stationary Outer ring : rotating Load : rotating	Rotating inner ring load Stationary outer ring load	Tight fit	Loose fit		
Inner ring : stationary Outer ring : rotating Load : stationary	Stationary inner ring load Rotating outer ring load	Loose fit	Tight fit		
Inner ring : rotating Outer ring : stationary Load : rotating	Stationary inner ring load Rotating outer ring load	Loose fit	Tight fit		

FIT CALCULATION

It is easier to mount a bearing with a loose fit than with an interference fit. However, if there is clearance between the fitting surfaces or too little interference, depending on the loading condition, creep may occur and damage the fitting surfaces; therefore, a sufficient interference must be chosen to prevent such damage.

The most common loading condition is to have a fixed load and fixed direction with the inner ring (i.e. shaft) rotating and the outer ring stationary. This condition is referred to as a rotating load on the inner ring or a stationary load on the outer ring. In other words, a circumferential load is applied to the inner ring and a spot load on the outer ring. For indeterminate loads caused by unbalanced weight, vibration, etc., interference fits are usually recommended for both inner and outer bearing rings. Standard shaft and housing fit tolerances are typically sufficient. However, if axial movement of the outer ring is desired, a looser than standard fit may be appropriate.

The selection of proper fits according to load conditions are presented in **Table 2**. For recommended shaft and housing fits by bearing type in accordance to load conditions and operating conditions, see **Tables 3 to 7**.

RECOMMENDED SHAFT FITS

Table 3 - Shaft Tolerances for Radial Bearings

			SHA	.FT DIAMETER (N	мм)			
LOAD CONDITIC	DNS	EXAMPLES	Ball bearings	Cylindrical roller tapered roller bearings	Spherical roller bearings	TOLERANCE OF SHAFT	REMARKS	
Radial bearing	s with cylindrical bores							
Rotating outer ring	Easy axial displacement of inner ring on shaft desirable	Wheels on stationary axles		.ll shaft diameter	-c	g6	Use g5 and h5 where accuracy is required. In case of large	
load	Easy axial displacement of inner ring on shaft unnecessary	Tension pulleys rope sheaves		h6	bearings, f6 can be used to allow easy axial movement			
			≤ 18	-	-	js5		
	Light loads or variable Loads (≤ 0.06 Cr (1))	Electrical home appliances, pumps, blowers, transport vehicles,	18-100	≤ 40	-	js6 (j6)	-	
		precision machinery, machine tools	100-200	40-140	-	k6		
			-	140-200	-	m6		
	g General bearing appl medium and large m (0.06 to 0.13 Cr (1)) gears, woodworking		≤ 18	-	-	js5/6 (j5/6)		
			18-100	≤ 40	≤ 40	k5/6		
Rotating inner ring		General bearing applications	100-140	40-100	40-65	m5/6	k6 and m6 can be used for	
load or		medium and large motors, turbines,	140-200	100-140	65-100	m6	single-row tapered roller bearings and single-row angular contact ball bearings instead of k5 and m5	
direction of load		gears, woodworking machine	200-280	140-200	100-140	n6		
indeterminate			-	200-400	140-280	р6		
			-	-	280-500	r6		
			-	-	> 500	r7		
			-	50-140	50-100	n6		
	Heavy loads or shock loads (> 0.13 Cr (1))	Railway axleboxes, industrial vehicles, traction motors,	-	140-200	100-140	p6	More than CN bearing internal clearance is necessary	
	(× 0.15 CI (1))	construction, equipment, crushers	-	> 200	140-200	r6	clearance is necessary	
			-	-	200-500	r7		
Axial Loads On	ly		A	ll Shaft Diameter	rs	js6 (J6)	-	
Radial bearing	s with tapered bores and sleeves							
		General bearing applications, railway axleboxes				h9/IT5	IT5 and IT7 mean that the deviation of the shaft from its true geometric from, e.g.	
All types of loa	ading	Transmission shafts, woodworking spindles	A	ll shaft diameter	ſS	h10/IT7	should be within the tolerances of IT5 h10/IT7 and IT7 respectively	
Thrust bearing	s with shafts							
Central axial lo	bad only	Main shafts of lathes	A	ll shaft diameter	5	h6 or js6 (j6)		
Combined	Stationary inner ring load	Cone crushers	All shaft diameters			js6 (j6)		
radial and axial loads (Spherical				≤200			_	
thrust roller bearings)	Rotating inner ring load or direction of load indeterminate	Paper pulp refiners, plastic extruders		200 ~ 400		m6		
				> 400		n6		

Notes : This table is applicable only to solid steel shafts. (1) Cr represents the basic load rating of the bearing.



NOMINAL BORE DIAMETER (INCH) SHAFT DIAMETER TOLERANCE (INCH) **BORE DIAMETER** TOLERANCE (INCH) RESULTING FIT (0.0001") **OPERATING CONDITIONS** REMARKS incl 5 T / 15 T +0.0010 3 +0.0005 0.0000 +0.0015 3 12 +0.0010 0.0000 +0.0025 +0.0015 5 T / 25 T For bearings with d≤6", clearance is usually larger than CN. Normal loads 12 24 +0.0020 0.0000 +0.0050 +0.0030 10 T / 50 T 15 T / 75 T 24 36 +0.0030 0.0000 +0.0075 +0.0045 **Rotating Inner** Ring Loads +0.0025 +0.0015 10 T / 25 T +0.0005 0.0000 3 In general, bearings with a clearance larger than CN are Heavy Loads Shock Loads High Speeds 3 12 +0.0010 0.0000 "--" means that the average interference is about 0.0005 d. 12 24 +0.0020 0.0000 24 36 +0.0030 0.0000 +0.0150 +0.0120 90 T / 150 T 5 L / 5 T 3 +0.00050.0000 +0.00050.0000 The inner ring cannot be displaced axially. When heavy or shock loads exist, the values for rotating inner ring loads - heavy or shock loads - apply. 3 12 +0.0010 0 0000 +0.0010 0.0000 10 L / 10 T 12 24 +0.0020 0.0000 +0.0020 0.0000 20 L / 20 T 24 36 +0.0030 0.0000 +0.0030 0.0000 30 L / 30 T Stationary Inner Ring Loads Normal Loads Without Shocks 3 +0.0005 0.0000 0.0000 -0.0005 10 L / 0 +0.0010 3 17 0 0000 0 0000 -0.0010 20 L / 0 The inner ring can be displaced axially. 12 24 +0.0020 0.0000 0.0000 -0.0020 40 L / 0 24 +0.0030 0.0000 0.0000 -0.0030 60 L / 0 36

Table 4 - Shaft Tolerances for Inch Size Tapered Roller Bearings

Table 5 - Shaft Tolerances for Bearings Mounted on Sleeves

NOMINAL SHAFT DIAMETER (MM)			DIAMETER AND FORM TOLERANCES (INCH)							
		ł	19	IT5/2	h10		IT7/2			
over	incl.	high		max	high	low	max			
10	18	0.0000	-0.0017	0.0002	0.0000	-0.0028	0.0004			
18	30	0.0000	-0.0020	0.0002	0.0000	-0.0033	0.0004			
30	50	0.0000	-0.0024	0.0002	0.0000	-0.0039	0.0005			
50	80	0.0000	-0.0029	0.0003	0.0000	-0.0047	0.0006			
80	120	0.0000	-0.0034	0.0003	0.0000	-0.0055	0.0007			
120	180	0.0000	-0.0039	0.0004	0.0000	-0.0063	0.0008			
180	250	0.0000	-0.0045	0.0004	0.0000	-0.0073	0.0009			
250	315	0.0000	-0.0051	0.0005	0.0000	-0.0083	0.0010			
315	400	0.0000	-0.0055	0.0005	0.0000	-0.0091	0.0011			
400	500	0.0000	-0.0061	0.0005	0.0000	-0.0098	0.0012			
500	630	0.0000	-0.0069	0.0006	0.0000	-0.0110	0.0014			
630	800	0.0000	-0.0079	0.0007	0.0000	-0.0126	0.0016			
800	1000	0.0000	-0.0091	0.0008	0.0000	-0.0142	0.0018			
1000	1250	0.0000	-0.0102	0.0009	0.0000	-0.0165	0.0021			

RECOMMENDED HOUSING FITS

Table 6 - Housing Tolerances for Radial Bearings

LOAD CONDI	TIONS		EXAMPLES	TOLERANCES FOR HOUSING BORES	AXIAL DISPLACEMENT OF OUTER RING	REMARKS			
Radial bearir	ngs with housings								
		Heavy loads on bearing in thin-walled housing of heavy shock loads	Automotive wheel hubs (Roller bearings) Crane traveling wheels	Ρ7					
Solid	Rotating outer ring load	Normal or heavy loads	Automotive wheel hubs (Ball bearings) Vibrating screens	N7	Impossible	_			
housings		Light or variable loads	Conveyor rollers rope sheaves Tension pulleys	M7					
		Heavy shock loads	Traction motors						
	Direction of load indeterminate	Normal or heavy loads	Pumps crankshaft	К7	Impossible	Axial displacement of the outer ring is not required			
		Normal or light loads	Main bearings Medium and large motors	JS7 (J7)	Possible	Axial displacement of outer ring is required			
Solid or split		Loads of all kinds	General bearing applications, Railway axleboxes	H7					
housings		Normal or light loads	Plummer blocks	H8	Easily possible				
	Rotating inner ring load	High temperature rise of inner ring through shaft	Paper dryers	G7		_			
		Accurate running required under normal or light loads	Grinding spindle rear ball bearings	JS6 (J6)	Possible				
			High speed centrifugal compressor free bearings		POSSIDIE				
Solid	Direction of load		Grinding spindle front ball bearings	- K6	Impossible	For heavy loads, interference fit tighter than K is used.			
housing	indeterminate		High speed centrifugal compressor fixed bearings			When high accuracy is required, very strict tolerances should be used			
	Rotating inner	Accurate running and high rigidity required under variable loads	Cylindrical roller bearings for machine tool main spindle	M6 or N6	Fixed	for fitting			
	ring load	Minimum noise is required	Electrical home appliances	H6	Easily possible	_			
Thrust bearir	ngs with housings								
				Clearance > 0.25 mi	m	For general applications			
			Thrust ball bearings	H8		When precision is required			
Axial load or	nly		Spherical thrust roller bearings	Outer ring has radia	l clearance	When radial loads are sustained by other bearings			
			Steep angle tapered roller bearings	H7 or JS7 (J7)		-			
Combined	Stationary outer	ring loads		К7		Normal loads			
radial and axial loads	Rotating outer r indeterminate	ing loads or direction of load	Spherical thrust roller bearings	M7		Relatively heavy radial loads			

Notes: (1) This table is applicable to cast iron and steel housings. For housings made of light alloys, the interference should be tighter than those in this table. (2) Refer to NSK catalogs for special fittings such as drawn cup needle.



Table 7 - Housing Tolerances for Inch Size Tapered Roller Bearings

OPERATING CONDITION	OPERATING CONDITIONS		NOMINAL OUTER DIAMETER (INCH)		OUTSIDE DIAMETER TOLERANCE (INCH)		IG BORE CE (INCH)	RESULTING FIT (0.0001″)	REMARKS	
		over	incl	max	min	max	min			
		-	3	+0.0010	0.0000	+0.0030	+0.0020	30 L / 10 L		
		3	6	+0.0010	0.0000	+0.0030	+0.0020	30 L / 10 L		
	Used either on free-end or fixed-end	6	12	+0.0010	0.0000	+0.0030	+0.0020	30 L / 10 L		
	free end of fixed end	12	24	+0.0020	0.0000	+0.0060	+0.0040	60 L / 20 L	REMARKS The outer ring can be easily displaced axially The outer ring can be displaced axially Generally, the outer ring is fixed axially The outer ring is fixed axially	
		24	36	+0.0030	0.0000	+0.0090	+0.0060	90 L / 30 L		
		-	3	+0.0010	0.0000	+0.0010	0.0000	10 L / 10 T	The outer ring can be easily displaced axially The outer ring can be displaced axially Generally, the outer ring is fixed axially	
	The surface de s	3	6	+0.0010	0.0000	+0.0010	0.0000	10 L / 10 T		
Stationary Outer Ring Loads	The outer ring position can be	6	12	+0.0010	0.0000	+0.0020	0.0000	20 L / 10 T		
	adjusted axially	12	24	+0.0020	0.0000	+0.0030	0.0010	30 L / 10 T		
		24	36	+0.0030	0.0000	+0.0050	+0.0020	50 L / 10 T		
		-	3	+0.0010	0.0000	-0.0005	-0.0015	5 T / 25 T		
	The outer size	3	6	+0.0010	0.0000	-0.0010	-0.0020	10 T / 30 T		
	The outer ring position cannot be	6	12	+0.0010	0.0000	-0.0010	-0.0020	10 T / 30 T	 displaced axially The outer ring can be displaced axially Generally, the outer ring is fixed axially 	
	adjusted axially	12	24	+0.0020	0.0000	-0.0010	-0.0030	10 T / 50 T		
		24	36	+0.0030	0.0000	-0.0010	-0.0040	10 T / 70 T		
		-	3	+0.0010	0.0000	-0.0005	-0.0015	5 T / 25 T		
	Normal Loads	3	6	+0.0010	0.0000	-0.0010	-0.0020	10 T / 30 T		
Rotating Outer Ring Loads	The outer ring	6	12	+0.0010	0.0000	-0.0010	-0.0020	10 T / 30 T	The outer ring is fixed axially	
	position cannot be adjusted axially	12	24	+0.0020	0.0000	-0.0010	-0.0030	10 T / 50 T		
		24	36	+0.0030	0.0000	-0.0010	-0.0040	10 T / 70 T		

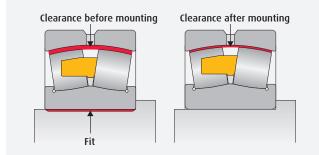
FITS AND CLEARANCE

FITTING AND RESIDUAL CLEARANCE

The internal clearance in rolling bearings in operation greatly influences bearing performance including fatigue life, vibration, noise, heat-generation, etc. Consequently, the selection of the proper internal clearance is one of the most important tasks when choosing a bearing after the type and size have been determined.

When the inner ring or the outer ring is tight-fitted on a shaft or in a housing, a decrease in the radial internal clearance is caused by the expansion or contraction of the bearing rings. The decrease varies according to the bearing type and size and design of the shaft and housing. The amount of this decrease is approximately 70 to 90% of the interference. The internal clearance after subtracting this decrease from the theoretical internal clearance ($\Delta 0$) is called the residual clearance (Δf).

Fig. 1 - Fitting and Clearance Reduction



TEMPERATURE EFFECTS ON INTERNAL CLEARANCE

Under normal operation, the radial internal clearance of a bearing will decrease because of the temperature differences between the inner and outer rings. Typically, the temperatures of the inner ring and the rolling elements are higher than that of the outer ring by 5 to 10°C. When the shaft is heated or when the housing is cooled, the difference between the inner and outer rings is even larger. The amount of decrease due to thermal expansion can be calculated from the following equations:

δt = α∆tDe

Where:

- δt Internal clearance decrease (mm) due to temperature
- α Coefficient of linear expansion of bearing steel (12.5 x 10-6) (1/°C)
- Δt Temperature difference between inner & outer rings (°C)
- De Outer ring raceway diameter (mm)

For ball bearings:

 $De \approx 1 / 5 (4D + d)$

For roller bearings:

 $De \approx 1 / 4 (3D + d)$

Where:

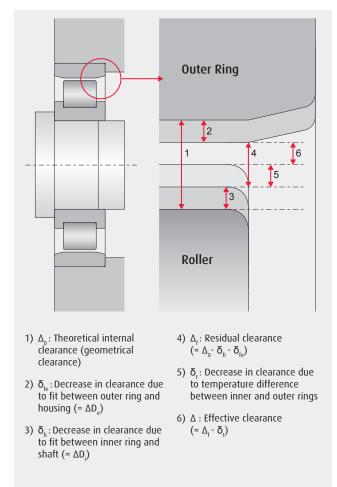
- D Bearing outside diameter (mm)
- d Bearing bore diameter (mm)

EFFECTIVE CLEARANCE

The effective, or operating, clearance Δ is obtained by subtracting δ t from the internal clearance after mounting Δ f. Theoretically, the longest life of a bearing can be expected when the effective clearance is slightly negative. However, it is difficult to achieve this condition and excessive negative clearance will shorten bearing life. Therefore, a clearance of zero or a slightly positive value is preferable.



Fig. 2 - Changes in Radial Clearance of Bearings



Angular contact ball bearings or tapered roller bearings normally require the user to set the internal clearance at mounting. The user should check the proper orientation of these bearings by checking the original bearings or the service manual for the machine. A check should also be made for the recommended set clearance. This can be obtained from the service manual, the machine manufacturer, or in consultation with the bearing manufacturer.

MAGNITUDE OF LOAD AND INTERFERENCE

Under load, a slight amount of deflection or deformation of the bearing rings will occur. This reduces the interference fit. For this reason, heavier loaded bearings require a heavier initial interference fit. The required interference can be calculated using the following equations:

 $\Delta d_{\rm F} = 0.08 \sqrt{\frac{d}{B} F_{\rm r}} \times 10^{-3}$ for light to normal loads

 $\Delta d_e \ge 0.02 \quad \frac{F_r}{B} \times 10^{-3}$

when Fe > .20 Cor

Where:

ΔdFInterference decrease of inner ring (mm)ΔdeEffective interference (mm)dBearing bore diameter (mm)BInner ring width (mm)FRRadial load applied to bearing (N)

Fe Equivalent load (N)

INTERFERENCE VARIATION DUE TO TEMPERATURE

Interference can decrease when bearing temperature increases during operation. If the temperature difference between the interior of the bearing and the surrounding parts of the housing is $\Delta T(^{\circ}C)$, then the temperature difference between the fitted surfaces of the shaft and the inner ring is estimated to be about (0.1 to 0.15)T. Decrease of inner ring interference due to this difference may be calculated from the following equation:

 $\Delta dT = (0.10 \sim 0.15) \Delta T \cdot a \cdot d = 0.0015 \Delta T \cdot dx 10-3$

Where:

- ΔdT Decrease of interference of inner ring due to temperature increase (mm)
- ΔT Temperature difference between bearing and surrounding parts
- d Bore diameter

SHAFTS AND HOUSINGS

FINISH OF SHAFT AND HOUSING

Since the roughness of fitted surfaces is reduced during fitting, the effective interference becomes less than the apparent interference. The amount of this interference decrease varies depending on the roughness of the surfaces and may be estimated using the following equations:

For ground shafts:

 $\Delta d = d / (d+2) \Delta da$

For machined shafts:

 $\Delta d = d / (d+3) \Delta da$

Where:

Δd	Effective interference (mm)
∆da	Apparent interference (mm)
d	Bearing bore diameter (mm)

According to these equations, the effective interference of bearings with a bore diameter of 30 to 150 mm is about 95% of the apparent interference.

ACCURACY OF SHAFTS & HOUSINGS

If the accuracy of a shaft or housing does not meet specification, the performance of the bearings will be impacted. For example, inaccuracy in the squareness of the shaft shoulder may cause misalignment of bearing inner and outer rings, which may reduce bearing fatigue life by adding an edge load to the normal load. Cage fracture and seizure can occur for this same reason. Housings should be rigid in order to provide firm bearing support, as well as advantages with noise and load distribution.

For normal operating conditions, a turned finish or smooth bored finish is sufficient for the fitting surface; however, a ground finish is necessary for applications where vibration and noise must be low or where heavy loads are applied.

Where two or more bearings are mounted in a single solid housing, the fitting surfaces of the housing bore should be designed so both bearing seats may be finished together with one operation such as in-line boring. For split housings, care must be taken in the fabrication of the housing so the outer ring will not become deformed during installation. The accuracy and surface finish of shafts and housings are listed in **Table 8** for normal operating conditions. For IT tolerance grade values, please refer to **Table 14** on **page C51**.

ITEM	CLASS OF BEARINGS		SHAFT	HOUSING BORE
Tolerance for Out-of-Roundness	Normal	Class 6	IT3 / 2 to IT4 / 2	IT4 / 2 to IT5 / 2
Interance for out-of-koundness	Class 5	Class 4	IT2 / 2 to IT3 / 2	IT2 / 2 to IT3 / 2
The second se	Normal	Class 6	IT3 / 2 to IT4 / 2	IT4 / 2 to IT5 / 2
Tolerance for Cylindricality	Class 5	Class 4	IT2 / 2 to IT3 / 2	IT2 / 2 to IT3 / 2
The second second second	Normal	Class 6	IT3	IT3 to IT4
Tolerance for Shoulder Runout	Class 5	Class 4	IT3	IT3
Developer of Fiblic Conference	Small Bearings	s: 0D ≤180 mm	32 µin	63 µin
Roughness of Fitting Surfaces R _a	Large Bearings	s: OD >180 mm	63 µin	125 µin

Table 8 - Accuracy and Roughness of Shaft and Housing

Note: This table is for general recommendation using radius measuring method, the basic tolerance (IT) class should be selected in accordance with the bearing precision class. In cases where outer ring is mounted in the housing bore with interference, the accuracy of the shaft and housing should be higher since this affects the bearing raceway directly.



For a practical measurement of the out-of-roundness of shafts and housings:

- > Using an appropriate micrometer, measure the diameter in a single plane in four or more locations as equally spaced as possible angularly and record all dimensions
- > The out-of-roundness value is the difference between the maximum and minimum values obtained, Max (-) Min

The values derived from **Table 8** should be doubled since the diameter method has been used. The process can be repeated at different radial planes across the bearing seating location (see **Figure 3**).

An example of methodology to record and evaluate findings can be found in **Table 9**.

Fig. 3 - Checking Cylindrical Shafts

For a practical measurement of the cylindricity of shafts and housings:

- Using an appropriate micrometer, measure the diameter at the same angular position in three or more axial planes equally spaced and covering the seating position of the bearing, recording all dimensions
- The cylindricality value is the difference between the maximum and minimum values obtained, Max (-) Min

The values derived from **Table 8** should be doubled since the diameter method has been used. The process can be repeated at different angular positions across the bearing seating location (see **Figure 4**).

Fig. 4 - Checking Housings

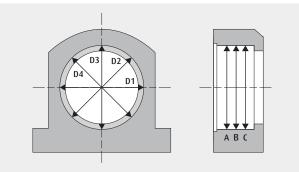


Table 9 - Recording and Evaluating Out-of-Roundness and Cylindricality

ANGULAR LOCATION	PLANE A	PLANE B	PLANE C	CYLINDRICALITY
0°	D1 _A	D1 _B	D1 _C	Max (-) Min at 0°
45°	D2 _A	D2 _B	D2 _C	Max (-) Min at 45°
90°	D3 _A	D3 _B	D3 _C	Max (-) Min at 90°
135°	D4 _A	D4 _B	D4 _C	Max (-) Min at 135°
OUT-OF-ROUNDNESS	Max (-) Min Plane A	Max (-) Min Plane B	Max (-) Min Plane C	

Note: None of the individual values should exceed the tolerances in Table 8. In the case of split housings, additional angular positions of measurement are recommended.

SHAFTS AND HOUSINGS

FITS FOR HOLLOW SHAFTS

Hollow shafts can be compressed under the stress imparted by interference fits. This deflection in the shaft material may result in a loss of interference, exposing the interface to bearing creep when under load. Following is an approach for correcting shaft fits to make up for the deflection that may occur when using a hollow shaft.

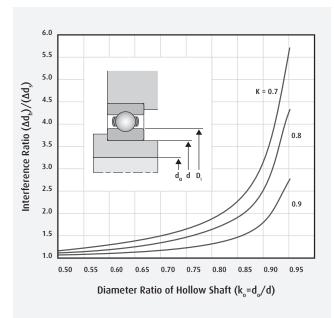
$$\frac{\Delta d_{h}}{\Delta d_{s}} = \frac{M + 2\left[\frac{k_{o}^{2}}{E_{s}(1-k_{o}^{2})} + \frac{1}{E_{i}(1-k^{2})}\right]}{M + \frac{2}{E_{i}(1-k^{2})}}$$

Where:

∆dh Interference of fit, hollow shaft Interference of fit, solid shaft ∆ds Shaft diameter, inner ring bore d Bore diameter, hollow shaft do Raceway diameter, inner ring Di Young's Modulus, inner ring (MPa) Ei Young's Modulus, shaft (MPa) Es Poisson's Number, inner ring mi (inverse of Poisson's Ratio) ms Poisson's Number, shaft (inverse of Poisson's Ratio) k = d/Di Diameter ratio, bearing inner ring Diameter ratio, hollow shaft ko = do/d

$$M = \left[\frac{m_s - 1}{m_s E_s} - \frac{m_i - 1}{m_i E_i} \right]$$

Fig. 5 - Shaft Fit Compensation for Hollow Shafts



If Di is not known for a particular bearing, it can be approximated by the following:

For ball bearings:

 $Di \approx d + 0.2(D - d)$

For roller bearings:

 $Di \approx d + 0.25(D - d)$



TOLERANCES FOR SHAFT DIAMETERS

Table 10 - Tolerances for Shaft Diameters

DIAMETER CLASS. (MM)		B D DEVIATION		f7	g5	g6	h5	h6
over	incl	∆ dmp						
3	6	0	- 0.0004	- 0.0004	- 0.0002	- 0.0002	0	0
5	0	- 0.0003	- 0.0007	- 0.0009	- 0.0004	- 0.0005	- 0.0002	- 0.0003
6	10	0	- 0.0005	- 0.0005	- 0.0002	- 0.0002	0	0
		- 0.0003	- 0.0009	- 0.0011	- 0.0004	- 0.0006	- 0.0002	- 0.0004
10	18	0	- 0.0006	- 0.0006	- 0.0002	- 0.0002	0	0
		- 0.0003	- 0.0011	- 0.0013	- 0.0006	- 0.0007	- 0.0003	- 0.0004
18	30	- 0.0004	- 0.0013	- 0.0008	- 0.0005	- 0.0003	- 0.0004	- 0.0005
		0.0004	- 0.0010	- 0.0010	- 0.0004	- 0.0004	0.0004	0.0005
30	50	- 0.0005	- 0.0016	- 0.0020	- 0.0008	- 0.0010	- 0.0004	- 0.0006
		0	- 0.0012	- 0.0012	- 0.0004	- 0.0004	0	0
50	65	- 0.0006	- 0.0019	- 0.0024	- 0.0009	- 0.0011	- 0.0005	- 0.0007
45	80	0	- 0.0012	- 0.0012	- 0.0004	- 0.0004	0	0
65	80	- 0.0006	- 0.0019	- 0.0024	- 0.0009	- 0.0011	- 0.0005	- 0.0007
80	100	0	- 0.0014	- 0.0014	- 0.0005	- 0.0005	0	0
50	100	- 0.0008	- 0.0023	- 0.0028	- 0.0011	- 0.0013	- 0.0006	- 0.0009
100	120	0	- 0.0014	- 0.0014	- 0.0005	- 0.0005	0	0
		- 0.0008	- 0.0023	- 0.0028	- 0.0011	- 0.0013	- 0.0006	- 0.0009
120	140	0	- 0.0017	- 0.0017	- 0.0006	- 0.0006	0	0
		- 0.0010	- 0.0027 - 0.0017	- 0.0033	- 0.0013	- 0.0015 - 0.0006	- 0.0007	- 0.0010
140	160	- 0.0010	- 0.0017	- 0.0033	- 0.0008	- 0.0008	- 0.0007	- 0.0010
		0.0010	- 0.0017	- 0.0017	- 0.0006	- 0.0006	0.0007	0.0010
160	180	- 0.0010	- 0.0027	- 0.0033	- 0.0013	- 0.0015	- 0.0007	- 0.0010
		0.0010	- 0.0020	- 0.0020	- 0.0006	- 0.0006	0.0007	0
180	200	- 0.0012	- 0.0031	- 0.0038	- 0.0014	- 0.0017	- 0.0008	- 0.0011
200	225	0	- 0.0020	- 0.0020	- 0.0006	- 0.0006	0	0
200		- 0.0012	- 0.0031	- 0.0038	- 0.0014	- 0.0017	- 0.0008	- 0.0011
225	250	0	- 0.0020	- 0.0020	- 0.0006	- 0.0006	0	0
225	230	- 0.0012	- 0.0031	- 0.0038	- 0.0014	- 0.0017	- 0.0008	- 0.0011
250	280	0	- 0.0022	- 0.0022	- 0.0007	- 0.0007	0	0
		- 0.0014	- 0.0035	- 0.0043	- 0.0016	- 0.0019	- 0.0009	- 0.0013
280	315	0	- 0.0022	- 0.0022	- 0.0007	- 0.0007	0	0
		- 0.0014	- 0.0035	- 0.0043	- 0.0016	- 0.0019	- 0.0009	- 0.0013
315	355	0 - 0.0016	- 0.0024 - 0.0039	- 0.0024 - 0.0047	- 0.0007 - 0.0017	- 0.0007 - 0.0021	0 - 0.0010	0 - 0.0014
		0.0018	- 0.0039	- 0.0024	- 0.0007	- 0.0007	0.0010	0.0014
355	400	- 0.0016	- 0.0024	- 0.0024	- 0.0007	- 0.0021	- 0.0010	- 0.0014
		0.0010	- 0.0027	- 0.0027	- 0.0008	- 0.0008	0.0010	0
400	450	- 0.0018	- 0.0043	- 0.0052	- 0.0019	- 0.0024	- 0.0011	- 0.0016
450	500	0	- 0.0027	- 0.0027	- 0.0008	- 0.0008	0	0
450	500	- 0.0018	- 0.0043	- 0.0052	- 0.0019	- 0.0024	- 0.0011	- 0.0016
500	560	0	- 0.0030	- 0.0030	- 0.0009	- 0.0009	0	0
500	500	- 0.0020	- 0.0047	- 0.0057	- 0.0020	- 0.0026	- 0.0011	- 0.0017
560	630	0	- 0.0030	- 0.0030	- 0.0009	- 0.0009	0	0
		- 0.0020	- 0.0047	- 0.0057	- 0.0020	- 0.0026	- 0.0011	- 0.0017
630	710	0	- 0.0031	- 0.0031	- 0.0009	- 0.0009	0	0
		- 0.0030	- 0.0047	- 0.0063	- 0.0022	- 0.0029	- 0.0013	- 0.0020
710	800	0 - 0.0030	- 0.0031 - 0.0051	- 0.0031 - 0.0063	- 0.0009 - 0.0022	- 0.0009 - 0.0029	0 - 0.0013	0 - 0.0020
		0	- 0.0034	- 0.0063	- 0.0022	- 0.0029	- 0.0013	- 0.0020
800	900	- 0.0039	- 0.0056	- 0.0069	- 0.0010	- 0.0032	- 0.0014	- 0.0022
		0.0035	- 0.0034	- 0.0034	- 0.0010	- 0.0010	0.0014	0.0022
900	1000	- 0.0039	- 0.0056	- 0.0069	- 0.0024	- 0.0032	- 0.0014	- 0.0022
100-		0	- 0.0039	- 0.0039	- 0.0011	- 0.0011	0	0
1000	1120	- 0.0049	- 0.0065	- 0.0080	- 0.0028	- 0.0037	- 0.0017	- 0.0026
1120	1250	0	- 0.0039	- 0.0039	- 0.0011	- 0.0011	0	0
1120	1250	- 0.0049	- 0.0065	- 0.0080	- 0.0028	- 0.0037	- 0.0017	- 0.0026



DIAMETER CLASS. (MM)		j7	j6	j5	h10	h9	h8	h7
incl	over							
	3	+ 0.0003	+ 0.0002	+ 0.0001	0	0	0	0
6	5	- 0.0002	- 0.0001	- 0.0001	- 0.0019	- 0.0012	- 0.0007	- 0.0005
10	6	+ 0.0004	+ 0.0003	+ 0.0002	0	0	0	0
	-	- 0.0002	- 0.0001	- 0.0001	- 0.0023	- 0.0014	- 0.0009	- 0.0006
18	10	+ 0.0005 - 0.0002	+ 0.0003 - 0.0001	+ 0.0002 - 0.0001	0 - 0.0028	0 - 0.0017	0 - 0.0011	0 - 0.0007
		+ 0.0005	+ 0.0004	+ 0.0002	0.0028	0.0017	0.0011	0.0007
30	18	- 0.0003	- 0.0002	- 0.0002	- 0.0033	- 0.0020	- 0.0013	- 0.0008
50	20	+ 0.0006	+ 0.0004	+ 0.0002	0	0	0	0
50	30	- 0.0004	- 0.0002	- 0.0002	- 0.0039	- 0.0024	- 0.0015	- 0.0010
65	50	+ 0.0007	+ 0.0005	+ 0.0002	0	0	0	0
05	50	- 0.0005	- 0.0003	- 0.0003	- 0.0047	- 0.0029	- 0.0018	- 0.0012
80	65	+ 0.0007	+ 0.0005	+ 0.0002	0	0	0	0
		- 0.0005	- 0.0003	- 0.0003	- 0.0047	- 0.0029	- 0.0018	- 0.0012
100	80	+ 0.0008	+ 0.0005	+ 0.0002	0	0	0	0
		- 0.0006	- 0.0004	- 0.0004	- 0.0055	- 0.0034	- 0.0021	- 0.0014
120	100	+ 0.0008 - 0.0006	+ 0.0005 - 0.0004	+ 0.0002 - 0.0004	0 - 0.0055	0 - 0.0034	0 - 0.0021	0 - 0.0014
		+ 0.0009	+ 0.0004	+ 0.0003	0.0033	0.0034	0.0021	0.0014
140	120	- 0.0007	- 0.0004	- 0.0004	- 0.0063	- 0.0039	- 0.0025	- 0.0016
		+ 0.0009	+ 0.0006	+ 0.0003	0	0	0	0
160	140	- 0.0007	- 0.0004	- 0.0004	- 0.0063	- 0.0039	- 0.0025	- 0.0016
400	470	+ 0.0009	+ 0.0006	+ 0.0003	0	0	0	0
180	160	- 0.0007	- 0.0004	- 0.0004	- 0.0063	- 0.0039	- 0.0025	- 0.0016
200	180	+ 0.0010	+ 0.0006	+ 0.0003	0	0	0	0
200	100	- 0.0008	- 0.0005	- 0.0005	- 0.0073	- 0.0045	- 0.0028	- 0.0018
225	200	+ 0.0010	+ 0.0006	+ 0.0003	0	0	0	0
		- 0.0008	- 0.0005	- 0.0005	- 0.0073	- 0.0045	- 0.0028	- 0.0018
250	225	+ 0.0010	+ 0.0006	+ 0.0003	0	0 - 0.0045	0	0 - 0.0018
		- 0.0008 + 0.0010	- 0.0005 + 0.0006	- 0.0005 + 0.0003	- 0.0073	- 0.0045	- 0.0028	- 0.0018
280	250	- 0.0010	- 0.0006	- 0.0005	- 0.0083	- 0.0051	- 0.0032	- 0.0020
		+ 0.0010	+ 0.0006	+ 0.0003	0.0000	0.0051	0.0052	0.0020
315	280	- 0.0010	- 0.0006	- 0.0006	- 0.0083	- 0.0051	- 0.0032	- 0.0020
		+ 0.0011	+ 0.0007	+ 0.0003	0	0	0	0
355	315	- 0.0011	- 0.0007	- 0.0007	- 0.0091	- 0.0055	- 0.0035	- 0.0022
400	355	+ 0.0011	+ 0.0007	+ 0.0003	0	0	0	0
400	222	- 0.0011	- 0.0007	- 0.0007	- 0.0091	- 0.0055	- 0.0035	- 0.0022
450	400	+ 0.0012	+ 0.0008	+ 0.0003	0	0	0	0
450	700	- 0.0013	- 0.0008	- 0.0008	- 0.0098	- 0.0061	- 0.0038	- 0.0025
500	450	+ 0.0012	+ 0.0008	+ 0.0003	0	0	0	0
		- 0.0013	- 0.0008	- 0.0008	- 0.0098	- 0.0061	- 0.0038	- 0.0025
560	500	-	+ 0.0009 - 0.0009	-	0 - 0.0110	0 0060	0 - 0.0043	0 - 0.0028
		-	+ 0.0009	-	- 0.0110	- 0.0069	- 0.0043	- 0.0028
630	560	-	- 0.0009	-	- 0.0110	- 0.0069	- 0.0043	- 0.0028
		-	+ 0.0010	-	0.0110	0.0009	0.0045	0.0020
710	630	-	- 0.0010	-	- 0.0126	- 0.0079	- 0.0049	- 0.0031
000	710	-	+ 0.0010	-	0	0	0	0
800	710	-	- 0.0010	-	- 0.0126	- 0.0079	- 0.0049	- 0.0031
900	800	-	+ 0.0011	-	0	0	0	0
200	000	-	- 0.0011	-	-0.0142	- 0.0091	- 0.0055	- 0.0035
100	900	-	+ 0.0011	-	0	0	0	0
		-	- 0.0011	-	-0.0142	- 0.0091	- 0.0055	- 0.0035
112	1000	-	+ 0.0013	-	0	0 0103	0	0
		-	- 0.0013	-	- 0.0165	- 0.0102	- 0.0065	- 0.0041
125	1120	-	+ 0.0013 - 0.0013	-	0 - 0.0165	0 - 0.0102	0 - 0.0065	0 - 0.0041

TOLERANCES FOR SHAFT DIAMETERS

Table 10 - Tolerances for Shaft Diameters

DIAMETER CLASS. (MM)		SINGLE PLANE MEAN B.D. DEVIATION (NORMAL)	js4	js5	js6	k4	k5	k6	k7
over	incl	∆ dmp							
3	6	0	+ 0.0001	+ 0.0001	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0004	+ 0.0005
		- 0.0003	- 0.0001	- 0.0001	- 0.0002	0	0	0	0
6	10	0 - 0.0003	+ 0.0001 - 0.0001	+ 0.0001 - 0.0001	+ 0.0002 - 0.0002	+ 0.0002	+ 0.0003	+ 0.0004	+ 0.0006
		0.0005	+ 0.0001	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0004	+ 0.0005	+ 0.0007
10	18	- 0.0003	- 0.0001	- 0.0002	- 0.0002	0	0	0	0
10	20	0	+ 0.0001	+ 0.0002	+ 0.0003	+ 0.0003	+ 0.0004	+ 0.0006	+ 0.0009
18	30	- 0.0004	- 0.0001	- 0.0002	- 0.0003	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
30	50	0	+ 0.0001	+ 0.0002	+ 0.0003	+ 0.0004	+ 0.0005	+ 0.0007	+ 0.0011
50	50	- 0.0005	- 0.0001	- 0.0002	- 0.0003	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
50	65	0	+ 0.0002	+ 0.0003	+ 0.0004	+ 0.0004	+ 0.0006	+ 0.0008	+ 0.0013
		- 0.0006	- 0.0002 + 0.0002	- 0.0003 + 0.0003	- 0.0004 + 0.0004	+ 0.0001 + 0.0004	+ 0.0001 + 0.0006	+ 0.0001 + 0.0008	+ 0.0001 + 0.0013
65	80	- 0.0006	- 0.0002	- 0.0003	- 0.0004	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
		0	+ 0.0002	+ 0.0003	+ 0.0004	+ 0.0005	+ 0.0007	+ 0.0010	+ 0.0015
80	100	- 0.0008	- 0.0002	- 0.0003	- 0.0004	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
100	120	0	+ 0.0002	+ 0.0003	+ 0.0004	+ 0.0005	+ 0.0007	+ 0.0010	+ 0.0015
100	120	- 0.0008	- 0.0002	- 0.0003	- 0.0004	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
120	140	0	+ 0.0002	+ 0.0004	+ 0.0005	+ 0.0006	+ 0.0008	+ 0.0011	+ 0.0017
120	140	- 0.0010	- 0.0002	- 0.0004	- 0.0005	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
140	160	0	+ 0.0002	+ 0.0004	+ 0.0005	+ 0.0006	+ 0.0008	+ 0.0011	+ 0.0017
		- 0.0010	- 0.0002	- 0.0004	- 0.0005	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
160	180	0 - 0.0010	+ 0.0002 - 0.0002	+ 0.0004 - 0.0004	+ 0.0005 - 0.0005	+ 0.0006 + 0.0001	+ 0.0008 + 0.0001	+ 0.0011 + 0.0001	+ 0.0017 + 0.0001
		- 0.0010	+ 0.0002	+ 0.0004	+ 0.0005	+ 0.0001	+ 0.0001	+ 0.0001	+ 0.0001
180	200	- 0.0012	- 0.0003	- 0.0004	- 0.0006	+ 0.0007	+ 0.0002	+ 0.0002	+ 0.0002
		0.0012	+ 0.0003	+ 0.0004	+ 0.0006	+ 0.0002	+ 0.0002	+ 0.0013	+ 0.0020
200	225	- 0.0012	- 0.0003	- 0.0004	- 0.0006	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
225	250	0	+ 0.0003	+ 0.0004	+ 0.0006	+ 0.0007	+ 0.0009	+ 0.0013	+ 0.0020
225	250	- 0.0012	- 0.0003	- 0.0004	- 0.0006	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
250	280	0	+ 0.0003	+ 0.0005	+ 0.0006	+ 0.0008	+ 0.0011	+ 0.0014	+ 0.0022
250	200	- 0.0014	- 0.0003	- 0.0005	- 0.0006	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
280	315	0	+ 0.0003	+ 0.0005	+ 0.0006	+ 0.0008	+ 0.0011	+ 0.0014	+ 0.0022
		- 0.0014	- 0.0003	- 0.0005	- 0.0006	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
315	355	- 0.0016	+ 0.0004 - 0.0004	+ 0.0005 - 0.0005	+ 0.0007 - 0.0007	+ 0.0009 + 0.0002	+ 0.0011 + 0.0002	+ 0.0016 + 0.0002	+ 0.0024 + 0.0002
		0.0010	+ 0.0004	+ 0.0005	+ 0.0007	+ 0.0002	+ 0.0011	+ 0.0002	+ 0.0024
355	400	- 0.0016	- 0.0004	- 0.0005	- 0.0007	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
		0	+ 0.0004	+ 0.0005	+ 0.0008	+ 0.0010	+ 0.0013	+ 0.0018	+ 0.0027
400	450	- 0.0018	- 0.0004	- 0.0005	- 0.0008	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
450	500	0	+ 0.0004	+ 0.0005	+ 0.0008	+ 0.0010	+ 0.0013	+ 0.0018	+ 0.0027
450	500	- 0.0018	- 0.0004	- 0.0005	- 0.0008	+ 0.0002	+ 0.0002	+ 0.0002	+ 0.0002
500	560	0	-	+ 0.0006	+ 0.0009	-	+ 0.0011	+ 0.0017	+ 0.0028
		- 0.0020	-	- 0.0006	- 0.0009	-	0	0	0
560	630	0 - 0.0020	-	+ 0.0006 - 0.0006	+ 0.0009 - 0.0009	-	+ 0.0011	+ 0.0017	+ 0.0028
		0.0020	-	+ 0.0006	+ 0.0010	-	+ 0.0013	+ 0.0020	+ 0.0031
630	710	- 0.0030	-	- 0.0006	- 0.0010	-	0	0	0
710	000	0	-	+ 0.0006	+ 0.0010	-	+ 0.0013	+ 0.0020	+ 0.0031
710	800	- 0.0030	-	- 0.0006	- 0.0010	-	0	0	0
800	900	0	-	+ 0.0007	+ 0.0011	-	+ 0.0014	+ 0.0022	+ 0.0035
000	200	- 0.0039	-	- 0.0007	- 0.0011	-	0	0	0
900	1000	0	-	+ 0.0007	+ 0.0011	-	+ 0.0014	+ 0.0022	+ 0.0035
		- 0.0039	-	- 0.0007	- 0.0011	-	0	0	0
1000	1120	0	-	+ 0.0008	+ 0.0013	-	+ 0.0017	+ 0.0026	+ 0.0041
		- 0.0049	-	- 0.0008 + 0.0008	- 0.0013 + 0.0013	-	0 + 0.0017	+ 0.0026	+ 0.0041
1120	1250	- 0.0049	-	+ 0.0008	- 0.0013	-	+ 0.0017	+ 0.0026	+ 0.0041



m5	m6	n5	n6	р6	p7	r6	r7		METER 5. (MM)
								over	incl
+ 0.0004	+ 0.0005	+ 0.0005	+ 0.0006	+ 0.0008	+ 0.0009	+ 0.0009	+ 0.0011	2	
+ 0.0002	+ 0.0002	+ 0.0003	+ 0.0003	+ 0.0005	+ 0.0005	+ 0.0006	+ 0.0006	3	6
+ 0.0005	+ 0.0006	+ 0.0006	+ 0.0007	+ 0.0009	+ 0.0012	+ 0.0011	+ 0.0013	6	10
+ 0.0002	+ 0.0002	+ 0.0004	+ 0.0004	+ 0.0006	+ 0.0006	+ 0.0007	+ 0.0007	•	
+ 0.0006	+ 0.0007	+ 0.0008	+ 0.0009	+ 0.0011	+ 0.0014	+ 0.0013	+ 0.0016	10	18
+ 0.0003	+ 0.0003	+ 0.0005	+ 0.0005	+ 0.0007	+ 0.0007	+ 0.0009	+ 0.0009		
+ 0.0007 + 0.0003	+ 0.0008 + 0.0003	+ 0.0009 + 0.0006	+ 0.0011 + 0.0006	+ 0.0014 + 0.0009	+ 0.0017 + 0.0009	+ 0.0016 + 0.0011	+ 0.0019 + 0.0011	18	30
+ 0.0003	+ 0.0003	+ 0.0000	+ 0.0003	+ 0.0009	+ 0.0009	+ 0.0020	+ 0.0023		
+ 0.0004	+ 0.0004	+ 0.0007	+ 0.0007	+ 0.0017	+ 0.0020	+ 0.0013	+ 0.0013	30	50
+ 0.0009	+ 0.0012	+ 0.0013	+ 0.0015	+ 0.0020	+ 0.0024	+ 0.0024	+ 0.0028		
+ 0.0004	+ 0.0004	+ 0.0008	+ 0.0008	+ 0.0013	+ 0.0013	+ 0.0016	+ 0.0016	50	65
+ 0.0009	+ 0.0012	+ 0.0013	+ 0.0015	+ 0.0020	+ 0.0024	+ 0.0024	+ 0.0029		
+ 0.0004	+ 0.0004	+ 0.0008	+ 0.0008	+ 0.0013	+ 0.0013	+ 0.0017	+ 0.0017	65	80
+ 0.0011	+ 0.0014	+ 0.0015	+ 0.0018	+ 0.0023	+ 0.0028	+ 0.0029	+ 0.0034		400
+ 0.0005	+ 0.0005	+ 0.0009	+ 0.0009	+ 0.0015	+ 0.0015	+ 0.0020	+ 0.0020	80	100
+ 0.0011	+ 0.0014	+ 0.0015	+ 0.0018	+ 0.0023	+ 0.0028	+ 0.0030	+ 0.0035	100	120
+ 0.0005	+ 0.0005	+ 0.0009	+ 0.0009	+ 0.0015	+ 0.0015	+ 0.0021	+ 0.0021	100	120
+ 0.0013	+ 0.0016	+ 0.0018	+ 0.0020	+ 0.0027	+ 0.0033	+ 0.0035	+ 0.0041	120	140
+ 0.0006	+ 0.0006	+ 0.0011	+ 0.0011	+ 0.0017	+ 0.0017	+ 0.0025	+ 0.0025	120	140
+ 0.0013	+ 0.0016	+ 0.0018	+ 0.0020	+ 0.0027	+ 0.0033	+ 0.0035	+ 0.0041	140	160
+ 0.0006	+ 0.0006	+ 0.0011	+ 0.0011	+ 0.0017	+ 0.0017	+ 0.0026	+ 0.0026	140	100
+ 0.0013	+ 0.0016	+ 0.0018	+ 0.0020	+ 0.0027	+ 0.0033	+ 0.0037	+ 0.0043	160	180
+ 0.0006	+ 0.0006	+ 0.0011	+ 0.0011	+ 0.0017	+ 0.0017	+ 0.0027	+ 0.0027		
+ 0.0015	+ 0.0018	+ 0.0020	+ 0.0024	+ 0.0031	+ 0.0038	+ 0.0042	+ 0.0048	180	200
+ 0.0007	+ 0.0007	+ 0.0012	+ 0.0012	+ 0.0020	+ 0.0020	+ 0.0030	+ 0.0030		
+ 0.0015	+ 0.0018	+ 0.0020	+ 0.0024	+ 0.0031	+ 0.0038	+ 0.0043	+ 0.0050	200	225
+ 0.0007 + 0.0015	+ 0.0007 + 0.0018	+ 0.0012 + 0.0020	+ 0.0012 + 0.0024	+ 0.0020 + 0.0031	+ 0.0020 + 0.0038	+ 0.0031 + 0.0044	+ 0.0031 + 0.0051		
+ 0.0015 + 0.0007	+ 0.0018	+ 0.0020	+ 0.0024	+ 0.0020	+ 0.0038	+ 0.0044	+ 0.0031	225	250
+ 0.0007	+ 0.0020	+ 0.0012	+ 0.0012	+ 0.0020	+ 0.0020	+ 0.0050	+ 0.0055		
+ 0.0008	+ 0.0008	+ 0.0013	+ 0.0013	+ 0.0022	+ 0.0022	+ 0.0037	+ 0.0037	250	280
+ 0.0017	+ 0.0020	+ 0.0022	+ 0.0026	+ 0.0035	+ 0.0043	+ 0.0051	+ 0.0059		
+ 0.0008	+ 0.0008	+ 0.0013	+ 0.0013	+ 0.0022	+ 0.0022	+ 0.0039	+ 0.0039	280	315
+ 0.0018	+ 0.0022	+ 0.0024	+ 0.0029	+ 0.0039	+ 0.0047	+ 0.0057	+ 0.0065		
+ 0.0008	+ 0.0008	+ 0.0015	+ 0.0015	+ 0.0024	+ 0.0024	+ 0.0043	+ 0.0043	315	355
+ 0.0018	+ 0.0022	+ 0.0024	+ 0.0029	+ 0.0039	+ 0.0047	+ 0.0059	+ 0.0067	255	400
+ 0.0008	+ 0.0008	+ 0.0015	+ 0.0015	+ 0.0024	+ 0.0024	+ 0.0045	+ 0.0045	355	400
+ 0.0020	+ 0.0025	+ 0.0026	+ 0.0031	+ 0.0043	+ 0.0052	+ 0.0065	+ 0.0074	400	450
+ 0.0009	+ 0.0009	+ 0.0016	+ 0.0016	+ 0.0027	+ 0.0027	+ 0.0050	+ 0.0050	400	450
+ 0.0020	+ 0.0025	+ 0.0026	+ 0.0031	+ 0.0043	+ 0.0052	+ 0.0068	+ 0.0077	450	500
+ 0.0009	+ 0.0009	+ 0.0016	+ 0.0016	+ 0.0027	+ 0.0027	+ 0.0052	+ 0.0052	450	500
+ 0.0022	+ 0.0028	+ 0.0029	+ 0.0035	+ 0.0048	+ 0.0058	+ 0.0076	+ 0.0087	500	560
+ 0.0010	+ 0.0010	+ 0.0017	+ 0.0017	+ 0.0031	+ 0.0031	+ 0.0059	+ 0.0059		
+ 0.0022	+ 0.0028	+ 0.0029	+ 0.0035	+ 0.0048	+ 0.0058	+ 0.0078	+ 0.0089	560	630
+ 0.0010	+ 0.0010	+ 0.0017	+ 0.0017	+ 0.0031	+ 0.0031	+ 0.0061	+ 0.0061		
+ 0.0024 + 0.0012	+ 0.0031 + 0.0012	+ 0.0032 + 0.0020	+ 0.0039 + 0.0020	+ 0.0054 + 0.0035	+ 0.0066 + 0.0035	+ 0.0089 + 0.0069	+ 0.0100 + 0.0069	630	710
+ 0.0012 + 0.0024	+ 0.0012	+ 0.0020	+ 0.0020	+ 0.0035	+ 0.0035	+ 0.0069	+ 0.0069		
+ 0.0024 + 0.0012	+ 0.0031	+ 0.0032	+ 0.0039	+ 0.0054	+ 0.0086	+ 0.0093	+ 0.0104	710	800
+ 0.0012	+ 0.0035	+ 0.0020	+ 0.0020	+ 0.0061	+ 0.0075	+ 0.0105	+ 0.0073		
+ 0.0023	+ 0.0013	+ 0.0022	+ 0.0022	+ 0.0039	+ 0.0039	+ 0.0083	+ 0.0083	800	900
+ 0.0013	+ 0.0035	+ 0.0022	+ 0.0044	+ 0.0061	+ 0.0075	+ 0.0109	+ 0.0122		
+ 0.0013	+ 0.0013	+ 0.0022	+ 0.0022	+ 0.0039	+ 0.0039	+ 0.0087	+ 0.0087	900	100
+ 0.0032	+ 0.0042	+ 0.0043	+ 0.0052	+ 0.0073	+ 0.0089	+ 0.0124	+ 0.0140		
+ 0.0016	+ 0.0016	+ 0.0026	+ 0.0026	+ 0.0047	+ 0.0047	+ 0.0098	+ 0.0098	1000	1120
+ 0.0032	+ 0.0042	+ 0.0043	+ 0.0052	+ 0.0073	+ 0.0089	+ 0.0128	+ 0.0144	4420	477
+ 0.0016	+ 0.0016	+ 0.0026	+ 0.0026	+ 0.0047	+ 0.0047	+ 0.0102	+ 0.0102	1120	1250

TOLERANCES FOR HOUSING DIAMETERS

Table 11 - Tolerances for Housing Bore Diameters

	METER 5. (MM)	SINGLE PLANE MEAN B.D. DEVIATION (NORMAL)	F7	G6	G7	H6	H7	Н8
Over	incl	Δ dmp						
		0	+ 0.0013	+ 0.0007	+ 0.0009	+ 0.0004	+ 0.0007	+ 0.0011
10	18	- 0.0003	+ 0.0006	+ 0.0002	+ 0.0002	0	0	0
10	20	0	+ 0.0016	+ 0.0008	+ 0.0011	+ 0.0005	+ 0.0008	+ 0.0013
18	30	- 0.0004	+ 0.0008	+ 0.0003	+ 0.0003	0	0	0
20	50	0	+ 0.0020	+ 0.0010	+ 0.0013	+ 0.0006	+ 0.0010	+ 0.0015
30	50	- 0.0004	+ 0.0010	+ 0.0004	+ 0.0004	0	0	0
50	00	0	+ 0.0024	+ 0.0011	+ 0.0016	+ 0.0007	+ 0.0012	+ 0.0018
50	80	- 0.0005	+ 0.0012	+ 0.0004	+ 0.0004	0	0	0
80	120	0	+ 0.0028	+ 0.0013	+ 0.0019	+ 0.0009	+ 0.0014	+ 0.0021
80	120	- 0.0006	+ 0.0014	+ 0.0005	+ 0.0005	0	0	0
120	150	0	+ 0.0033	+ 0.0015	+ 0.0021	+ 0.0010	+ 0.0016	+ 0.0025
120	150	- 0.0007	+ 0.0017	+ 0.0006	+ 0.0006	0	0	0
150	180	0	+ 0.0033	+ 0.0015	+ 0.0021	+ 0.0010	+ 0.0016	+ 0.0025
150	100	- 0.0010	+ 0.0017	+ 0.0006	+ 0.0006	0	0	0
180	250	0	+ 0.0038	+ 0.0017	+ 0.0024	+ 0.0011	+ 0.0018	+ 0.0028
100	250	- 0.0012	+ 0.0020	+ 0.0006	+ 0.0006	0	0	0
250	315	0	+ 0.0043	+ 0.0019	+ 0.0027	+ 0.0013	+ 0.0020	+ 0.0032
250	515	- 0.0014	+ 0.0022	+ 0.0007	+ 0.0007	0	0	0
315	400	0	+ 0.0047	+ 0.0021	+ 0.0030	+ 0.0014	+ 0.0022	+ 0.0035
515	400	- 0.0016	+ 0.0024	+ 0.0007	+ 0.0007	0	0	0
400	500	0	+ 0.0052	+ 0.0024	+ 0.0033	+ 0.0016	+ 0.0025	+ 0.0038
400	500	- 0.0018	+ 0.0027	+ 0.0008	+ 0.0008	0	0	0
500	630	0	+ 0.0057	+ 0.0026	+ 0.0036	+ 0.0017	+ 0.0028	+ 0.0043
500	050	- 0.0020	+ 0.0030	+ 0.0009	+ 0.0009	0	0	0
630	800	0	+ 0.0063	+ 0.0029	+ 0.0041	+ 0.0020	+ 0.0031	+ 0.0049
050		- 0.0030	+ 0.0031	+ 0.0009	+ 0.0009	0	0	0
800	1000	0	+ 0.0069	+ 0.0032	+ 0.0046	+ 0.0022	+ 0.0035	+ 0.0055
000	1000	- 0.0039	+ 0.0034	+ 0.0010	+ 0.0010	0	0	0
1000	1250	0	+ 0.0080	+ 0.0037	+ 0.0052	+ 0.0026	+ 0.0041	+ 0.0065
1000	1250	- 0.0049	+ 0.0039	+ 0.0011	+ 0.0011	0	0	0
2150	1600	0	+ 0.0093	+ 0.0043	+ 0.0061	+ 0.0031	+ 0.0049	+ 0.0077
2150	1500	- 0.0063	+ 0.0043	+ 0.0012	+ 0.0012	0	0	0
1600	2000	0	+ 0.0106	+ 0.0049	+ 0.0072	+ 0.0036	+ 0.0059	+ 0.0091
1000	2000	- 0.0079	+ 0.0047	+ 0.0013	+ 0.0013	0	0	0
2000	2500	0	+ 0.0120	+ 0.0057	+ 0.0082	+ 0.0043	+ 0.0069	+ 0.0110
2000	2300	- 0.0098	+ 0.0051	+ 0.0013	+ 0.0013	0	0	0



DIAMET CLASS. (<i>I</i>	JS7	JS6	JS5	J7	J6	H10	Н9
Over							
	+ 0.0004	+ 0.0002	+ 0.0002	+ 0.0004	+ 0.0002	+ 0.0028	+ 0.0017
10	- 0.0004	- 0.0002	- 0.0002	- 0.0003	- 0.0002	0	0
	+ 0.0004	+ 0.0003	+ 0.0002	+ 0.0005	+ 0.0003	+ 0.0033	+ 0.0020
18	- 0.0004	- 0.0003	- 0.0002	- 0.0004	- 0.0002	0	0
	+ 0.0005	+ 0.0003	+ 0.0002	+ 0.0006	+ 0.0004	+ 0.0039	+ 0.0024
30	- 0.0005	- 0.0003	- 0.0002	- 0.0004	- 0.0002	0	0
	+ 0.0006	+ 0.0004	+ 0.0003	+ 0.0007	+ 0.0005	+ 0.0047	+ 0.0029
50	- 0.0006	- 0.0004	- 0.0003	- 0.0005	- 0.0002	0	0
	+ 0.0007	+ 0.0004	+ 0.0003	+ 0.0009	+ 0.0006	+ 0.0055	+ 0.0034
80	- 0.0007	- 0.0004	- 0.0003	- 0.0005	- 0.0002	0	0
	+ 0.0008	+ 0.0005	+ 0.0004	+ 0.0010	+ 0.0007	+ 0.0063	+ 0.0039
120	- 0.0008	- 0.0005	- 0.0004	- 0.0006	- 0.0003	0	0
	+ 0.0008	+ 0.0005	+ 0.0004	+ 0.0010	+ 0.0007	+ 0.0063	+ 0.0039
150	- 0.0008	- 0.0005	- 0.0004	- 0.0006	- 0.0003	0	0
	+ 0.0009	+ 0.0006	+ 0.0004	+ 0.0012	+ 0.0009	+ 0.0073	+ 0.0045
180	- 0.0009	- 0.0006	- 0.0004	- 0.0006	- 0.0003	0	0
	+ 0.0010	+ 0.0006	+ 0.0005	+ 0.0014	+ 0.0010	+ 0.0083	+ 0.0051
250	- 0.0010	- 0.0006	- 0.0005	- 0.0006	- 0.0003	0	0
	+ 0.0011	+ 0.0007	+ 0.0005	+ 0.0015	+ 0.0011	+ 0.0091	+ 0.0055
315	- 0.0011	- 0.0007	- 0.0005	- 0.0007	- 0.0003	0	0
	+ 0.0012	+ 0.0008	+ 0.0005	+ 0.0017	+ 0.0013	+ 0.0098	+ 0.0061
400	- 0.0012	- 0.0008	- 0.0005	- 0.0008	- 0.0003	0	0
	+ 0.0014	+ 0.0009	+ 0.0006	-	-	+ 0.0110	+ 0.0069
500	- 0.0014	- 0.0009	- 0.0006	-	-	0	0
	+ 0.0016	+ 0.0010	+ 0.0006	_	-	+ 0.0126	+ 0.0079
630	- 0.0016	- 0.0010	- 0.0006	_	-	0	0
	+ 0.0018	+ 0.0011	+ 0.0007	_	-	+ 0.0142	+ 0.0091
800	- 0.0018	- 0.0011	- 0.0007			0.0142	0.0000
	+ 0.0021	+ 0.0013	+ 0.0008	-	-	+ 0.0165	+ 0.0102
1000							
	- 0.0021	- 0.0013	- 0.0008	-	-	0	0
2150	+ 0.0025	+ 0.0015	+ 0.0010	-	-	+ 0.0197	+ 0.0122
	- 0.0025	- 0.0015	- 0.0010	-	-	0	0
1600	+ 0.0030	+ 0.0018	+ 0.0012		-	+ 0.0236	+ 0.0146
	- 0.0030	- 0.0018	- 0.0012	-	-	0	0
2000	+ 0.0034	+ 0.0022	+ 0.0014	-	-	+ 0.0276	+ 0.0173
	- 0.0034	- 0.0022	- 0.0014	-	-	0	0

TOLERANCES FOR HOUSING DIAMETERS

Table 11 - Tolerances for Housing Bore Diameters

	METER 5. (MM)	SINGLE PLANE MEAN B.D. DEVIATION (NORMAL)	К5	K6	К7	M5	M6
Over	incl	Δ dmp					
10	10	0	+ 0.0001	+ 0.0001	+ 0.0002	- 0.0002	- 0.0002
10	18	- 0.0003	- 0.0002	- 0.0004	- 0.0005	- 0.0005	- 0.0006
10	20	0	0	+ 0.0001	+ 0.0002	- 0.0002	- 0.0002
18	30	- 0.0004	- 0.0003	- 0.0004	- 0.0006	- 0.0006	- 0.0007
20	50	0	+ 0.0001	+ 0.0001	+ 0.0003	- 0.0002	- 0.0002
30	50	- 0.0004	- 0.0004	- 0.0005	- 0.0007	- 0.0006	- 0.0008
50	80	0	+ 0.0001	+ 0.0002	+ 0.0004	- 0.0002	- 0.0002
50	80	- 0.0005	- 0.0004	- 0.0006	- 0.0008	- 0.0007	- 0.0009
00	120	0	+ 0.0001	+ 0.0002	+ 0.0004	- 0.0003	- 0.0002
80	120	- 0.0006	- 0.0005	- 0.0007	- 0.0010	- 0.0009	- 0.0011
120	150	0	+ 0.0001	+ 0.0002	+ 0.0005	- 0.0004	- 0.0003
120	150	- 0.0007	- 0.0006	- 0.0008	- 0.0011	- 0.0011	- 0.0013
150	100	0	+ 0.0001	+ 0.0002	+ 0.0005	- 0.0004	- 0.0003
150	180	- 0.0010	- 0.0006	- 0.0008	- 0.0011	- 0.0011	- 0.0013
180	250	0	+ 0.0001	+ 0.0002	+ 0.0005	- 0.0004	- 0.0003
160	250	- 0.0012	- 0.0007	- 0.0009	- 0.0013	- 0.0012	- 0.0015
250	215	0	+ 0.0001	+ 0.0002	+ 0.0006	- 0.0005	- 0.0004
250	315	- 0.0014	- 0.0008	- 0.0011	- 0.0014	- 0.0014	- 0.0016
215	400	0	+ 0.0001	+ 0.0003	+ 0.0007	- 0.0006	- 0.0004
315	400	- 0.0016	- 0.0009	- 0.0011	- 0.0016	- 0.0015	- 0.0018
400	500	0	+ 0.0001	+ 0.0003	+ 0.0007	- 0.0006	- 0.0004
400	500	- 0.0018	- 0.0010	- 0.0013	- 0.0018	- 0.0017	- 0.0020
500	(20	0	-	0	0	-	- 0.0010
500	630	- 0.0020	-	- 0.0017	- 0.0028	-	- 0.0028
630	800	0	-	0	0	-	- 0.0012
030	800	- 0.0030	-	- 0.0020	- 0.0031	-	- 0.0031
200	1000	0	-	0	0	-	- 0.0013
800	1000	- 0.0039	-	- 0.0022	- 0.0035	-	-0.0035
1000	1250	0	-	0	0	-	- 0.0016
1000	1250	- 0.0049	-	- 0.0026	- 0.0041	-	- 0.0042
2150	1600	0	-	0	0	-	- 0.0019
2150	1600	- 0.0063	-	- 0.0031	- 0.0049	-	- 0.0050
1600	2000	0	-	0	0	-	- 0.0023
1600	2000	- 0.0079	-	- 0.0036	- 0.0059	-	- 0.0059
2000	2500	0	-	0	0	-	- 0.0027
2000	2500	- 0.0098	-	- 0.0043	- 0.0069	-	- 0.0070



М7	N6	N7	Р6	Ρ7		METER . (MM)
					Over	incl
0	- 0.0004	- 0.0002	- 0.0006	- 0.0004		
- 0.0007	- 0.0008	- 0.0009	- 0.0010	- 0.0011	10	18
0	- 0.0004	- 0.0003	- 0.0007	- 0.0006	10	20
- 0.0008	- 0.0009	- 0.0011	- 0.0012	- 0.0014	18	30
0	- 0.0005	- 0.0003	- 0.0008	- 0.0007	20	50
- 0.0010	- 0.0011	- 0.0013	- 0.0015	- 0.0017	30	50
0	- 0.0006	- 0.0004	- 0.0010	- 0.0008	50	80
- 0.0012	- 0.0013	- 0.0015	- 0.0018	- 0.0020	50	80
0	- 0.0006	- 0.0004	- 0.0012	- 0.0009	80	120
- 0.0014	- 0.0015	- 0.0018	- 0.0020	- 0.0023	80	120
0	- 0.0008	- 0.0005	- 0.0014	- 0.0011	120	150
- 0.0016	- 0.0018	- 0.0020	- 0.0024	- 0.0027	120	150
0	- 0.0008	- 0.0005	- 0.0014	- 0.0011	150	180
- 0.0016	- 0.0018	- 0.0020	- 0.0024	- 0.0027	150	180
0	- 0.0009	- 0.0006	- 0.0016	- 0.0013	180	250
- 0.0018	- 0.0020	- 0.0024	- 0.0028	- 0.0031	160	250
0	- 0.0010	- 0.0006	- 0.0019	- 0.0014	250	315
- 0.0020	- 0.0022	- 0.0026	- 0.0031	-0.0035	250	515
0	- 0.0010	- 0.0006	- 0.0020	- 0.0016	215	400
- 0.0022	- 0.0024	- 0.0029	- 0.0034	- 0.0039	315	400
0	- 0.0011	- 0.0007	- 0.0022	- 0.0018	400	500
- 0.0025	- 0.0026	- 0.0031	- 0.0037	- 0.0043	400	500
- 0.0010	- 0.0017	- 0.0017	- 0.0031	- 0.0031	500	630
- 0.0038	-0.0035	- 0.0045	- 0.0048	- 0.0058	500	630
- 0.0012	- 0.0020	- 0.0020	- 0.0035	-0.0035	630	000
- 0.0043	- 0.0039	- 0.0051	- 0.0054	- 0.0066	630	800
- 0.0013	- 0.0022	- 0.0022	- 0.0039	- 0.0039	800	1000
- 0.0049	- 0.0044	- 0.0057	- 0.0061	- 0.0075	800	1000
- 0.0016	- 0.0026	- 0.0026	- 0.0047	- 0.0047	1000	1250
- 0.0057	- 0.0052	- 0.0067	- 0.0073	- 0.0089	1000	1250
- 0.0019	- 0.0031	- 0.0031	- 0.0055	- 0.0055	2150	1600
- 0.0068	- 0.0061	- 0.0080	- 0.0086	- 0.0104	2150	1000
- 0.0023	- 0.0036	- 0.0036	- 0.0067	- 0.0067	1(00	2000
- 0.0082	- 0.0072	- 0.0095	- 0.0103	- 0.0126	1600	2000
- 0.0027	- 0.0043	- 0.0043	- 0.0077	- 0.0077	2000	2500
- 0.0096	- 0.0087	- 0.0112	- 0.0120	- 0.0146	2000	2500

Table 12 - Shaft Diameters and Resulting Fits

BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	f	6	RESULTING	f	7	RESULTING	g	5	RESULTING	g	6	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
4	0.1575	0.1572	0.1571	0.1568		0.1571	0.1566		0.1573	0.1571		0.1573	0.1570	
5	0.1969	0.1965	0.1965	0.1961	7L/1L	0.1965	0.1960	9L/1L	0.1967	0.1965	4 L / 2 T	0.1967	0.1964	5 L / 2 T
6	0.2362	0.2359	0.2358	0.2355	/	0.2358	0.2354		0.2361	0.2359	,	0.2361	0.2357	- /
7	0.2756	0.2753	0.2751	0.2747		0.2751	0.2745		0.2754	0.2752		0.2754	0.2750	
8	0.3150	0.3146	0.3144	0.3141		0.3144	0.3139		0.3148	0.3145		0.3148	0.3144	
9	0.3543	0.3540	0.3538	0.3535	9 L / 2 L	0.3538	0.3532	11 L / 2 L	0.3541	0.3539	4 L / 1 T	0.3541	0.3538	6L/1T
10	0.3937	0.3934	0.3932	0.3928		0.3932	0.3926		0.3935	0.3933		0.3935	0.3931	
12	0.4724	0.4721	0.4718	0.4714		0.4718	0.4711		0.4722	0.4719		0.4722	0.4718	
15	0.5906	0.5902	0.5899	0.5895	11 L / 3 L	0.5899	0.5892	13 L / 3 L	0.5903	0.5900	6L/1T	0.5903	0.5899	7 L / 1 T
17	0.6693	0.6690	0.6687	0.6682	,	0.6687	0.6680	,	0.6691	0.6687	· · · ·	0.6691	0.6686	· · ·
20	0.7874	0.7870	0.7866	0.7861		0.7866	0.7858		0.7871	0.7868		0.7871	0.7866	
25	0.9843	0.9839	0.9835	0.9830	13 L / 4 L	0.9835	0.9826	16 L / 4 L	0.9840	0.9836	6L/1T	0.9840	0.9835	8L/1T
30	1.1811	1.1807	1.1803	1.1798	,	1.1803	1.1795	,	1.1808	1.1805	· · ·	1.1808	1.1803	· · ·
35	1.3780	1.3775	1.3770	1.3763		1.3770	1.3760		1.3776	1.3772		1.3776	1.3770	
40	1.5748	1.5743	1.5738	1.5732		1.5738	1.5728		1.5744	1.5740		1.5744	1.5738	
45	1.7717	1.7712	1.7707	1.7700	16 L / 5 L	1.7707	1.7697	20 L / 5 L	1.7713	1.7709	8 L / 1 T	1.7713	1.7707	10 L / 1 T
50	1.9685	1.9680	1.9675	1.9669		1.9675	1.9665		1.9681	1.9677		1.9681	1.9675	
55	2.1654	2.1648	2.1642	2.1634		2.1642	2.1630		2.1650	2.1644		2.1650	2.1642	
60	2.3622	2.3616	2.3610	2.3603	19 L / 6 L	2.3610	2.3598		2.3618	2.3613		2.3618	2.3611	
65	2.5591	2.5585	2.5579	2.5571		2.5579	2.5567		2.5587	2.5581		2.5587	2.5579	
70	2.7559	2.7553	2.7547	2.7540		2.7547	2.7535	24 L / 6 L	2.7555	2.7550	9 L / 2 T	2.7555	2.7548	11 L / 2 T
75	2.9528	2.9522	2.9516	2.9508		2.9516	2.9504		2.9524	2.9519		2.9524	2.9516	
80	3.1496	3.1490	3.1484	3.1477		3.1484	3.1472		3.1492	3.1487		3.1492	3.1485	
85	3.3465	3.3457	3.3450	3.3442		3.3450	3.3437		3.3460	3.3454		3.3460	3.3451	
90	3.5433	3.5425	3.5419	3.5410		3.5419	3.5405		3.5428	3.5422		3.5428	3.5420	
95	3.7402	3.7394	3.7387	3.7379		3.7387	3.7374		3.7397	3.7391		3.7397	3.7388	
100	3.9370	3.9362	3.9356	3.9347	23 L / 6 L	3.9356	3.9342	28 L / 6 L	3.9365	3.9359	11 L / 3 T	3.9365	3.9357	13 L / 3 T
105	4.1339	4.1331	4.1324	4.1316	,	4.1324	4.1311		4.1334	4.1328		4.1334	4.1325	
110	4.3307	4.3299	4.3293	4.3284		4.3293	4.3279		4.3302	4.3296		4.3302	4.3294	
120	4.7244	4.7236	4.7230	4.7221		4.7230	4.7216		4.7239	4.7233		4.7239	4.7231	
130	5.1181	5.1171	5.1164	5.1154		5.1164	5.1148		5.1176	5.1169		5.1176	5.1166	
140	5.5118	5.5108	5.5101	5.5091		5.5101	5.5085		5.5113	5.5106		5.5113	5.5103	
150	5.9055	5.9045	5.9038	5.9028		5.9038	5.9022		5.9050	5.9043		5.9050	5.9040	
160	6.2992	6.2982	6.2975	6.2965	27 L / 7 L	6.2975	6.2959	33 L / 7 L	6.2987	6.2980	13 L / 4 T	6.2987	6.2977	15 L / 4 T
170	6.6929	6.6919	6.6912	6.6902		6.6912	6.6896		6.6924	6.6917		6.6924	6.6914	
180	7.0866	7.0856	7.0849	7.0839		7.0849	7.0833		7.0861	7.0854		7.0861	7.0851	
190	7.4803	7.4791	7.4783	7.4772		7.4783	7.4765		7.4797	7.4789		7.4797	7.4786	
200	7.8740	7.8728	7.8720	7.8709		7.8720	7.8702		7.8734	7.8726		7.8734	7.8723	
220	8.6614	8.6602	8.6594	8.6583	31 L / 8 L	8.6594	8.6576	38 L / 8 L	8.6608	8.6600	14 L / 6 T	8.6608	8.6597	17 L / 6 T
240	9.4488	9.4476	9.4469	9.4457		9.4469	9.4450		9.4482	9.4474		9.4482	9.4471	
260	10.2362	10.2348	10.2340	10.2328		10.2340	10.2320		10.2356	10.2346		10.2356	10.2343	
280	11.0236	11.0222	11.0214	11.0202	35 L / 8 L	11.0214	11.0194	43 L / 8 L	11.0230	11.0220	16 L / 7 T	11.0230	11.0217	19 L / 7 T
300	11.8110	11.8096	11.8088	11.8076	,	11.8088	11.8068	,	11.8104	11.8094	,	11.8104	11.8091	



BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	f	6	RESULTING	f	7	RESULTING	g	5	RESULTING	g	6	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.5960	12.5946		12.5960	12.5937		12.5977	12.5967		12.5977	12.5963	
340	13.3858	13.3843	13.3834	13.3820		13.3834	13.3811		13.3851	13.3841		13.3851	13.3837	
360	14.1732	14.1717	14.1708	14.1694	39 L / 9 L	14.1708	14.1685	47 L / 9 L	14.1725	14.1715	17 L / 9 T	14.1725	14.1711	21 L / 9 T
380	14.9606	14.9591	14.9582	14.9568		14.9582	14.9559		14.9599	14.9589		14.9599	14.9585	
400	15.7480	15.7465	15.7456	15.7442		15.7456	15.7433		15.7473	15.7463		15.7473	15.7459	
420	16.5354	16.5337	16.5328	16.5312		16.5328	16.5303		16.5346	16.5336		16.5346	16.5331	
440	17.3228	17.3211	17.3202	17.3186		17.3202	17.3177		17.3220	17.3210		17.3220	17.3205	
460	18.1102	18.1085	18.1076	18.1060	43 L / 9 L	18.1076	18.1051	52 L / 9 L	18.1094	18.1084	19 L / 10 T	18.1094	18.1079	24 L / 10 T
480	18.8976	18.8959	18.8950	18.8934		18.8950	18.8925		18.8969	18.8958		18.8969	18.8953	
500	19.6850	19.6833	19.6824	19.6808		19.6824	19.6799		19.6843	19.6832		19.6843	19.6827	
530	20.8661	20.8642	20.8631	20.8614	471 (401	20.8631	20.8604		20.8653	20.8642		20.8653	20.8635	
560	22.0472	22.0453	22.0443	22.0425		22.0443	22.0415	57 L / 10 L	22.0464	22.0453	20 L / 11 T	22.0464	22.0446	26 L / 11 T
600	23.6220	23.6201	23.6191	23.6173	47 L / 10 L	23.6191	23.6163	57 L / 10 L	23.6212	23.6201	201/111	23.6212	23.6194	20 L / 11 I
630	24.8031	24.8012	24.8002	24.7984		24.8002	24.7974		24.8023	24.8012		24.8023	24.8006	
670	26.3780	26.3750	26.3748	26.3728		26.3748	26.3717		26.3770	26.3757		26.3770	26.3750	
710	27.9528	27.9498	27.9496	27.9476	51 L / 2 L	27.9496	27.9465	63 L / 2 L	27.9518	27.9506	22 L / 20 T	27.9518	27.9498	29 L / 20 T
750	29.5276	29.5246	29.5244	29.5224	SIL/ZL	29.5244	29.5213	03 L / Z L	29.5266	29.5254	ZZ L / ZU I	29.5266	29.5246	29 L / 20 I
800	31.4961	31.4931	31.4929	31.4909		31.4929	31.4898		31.4951	31.4939		31.4951	31.4931	
850	33.4646	33.4606	33.4612	33.4590		33.4612	33.4576		33.4635	33.4621		33.4635	33.4613	
900	35.4331	35.4291	35.4297	35.4275	56 L / 6 T	35.4297	35.4261	69 L / 6 T	35.4320	35.4306	24 L / 29 T	35.4320	35.4298	32 L / 29 T
950	37.4016	37.3976	37.3982	37.3960	30 L / 0 I	37.3982	37.3946	09L/01	37.4006	37.3991	24 L / 29 I	37.4006	37.3983	JZ L / Z9 I
1000	39.3701	39.3661	39.3667	39.3645		39.3667	39.3631		39.3691	39.3676		39.3691	39.3669	
1060	41.7323	41.7274	41.7284	41.7258		41.7284	41.7243		41.7312	41.7295		41.7312	41.7286	
1120	44.0945	44.0896	44.0906	44.0880	(F.L. / 11.T	44.0906	44.0865	001 / 11 7	44.0934	44.0917	201 / 20 7	44.0934	44.0908	271 / 20 7
1180	46.4567	46.4518	46.4528	46.4502	65 L / 11 T	46.4528	46.4487	80 L / 11 T	46.4556	46.4539	28 L / 38 T	46.4556	46.4530	37 L / 38 T
1250	49.2126	49.2077	49.2087	49.2061		49.2087	49.2046		49.2115	49.2098		49.2115	49.2089	

Table 12 - Shaft Diameters and Resulting Fits

BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	h	5	RESULTING	h	16	RESULTING	h	7	RESULTING	h	8	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
4	0.1575	0.1572	0.1575	0.1573		0.1575	0.1572		0.1575	0.1570		0.1575	0.1568	
5	0.1969	0.1965	0.1969	0.1967	2 L / 3 T	0.1969	0.1965	3 L / 3 T	0.1969	0.1964	5 L / 3 T	0.1969	0.1961	7 L / 3 T
6	0.2362	0.2359	0.2362	0.2360	,	0.2362	0.2359	, í	0.2362	0.2357	, ,	0.2362	0.2355	,
7	0.2756	0.2753	0.2756	0.2754		0.2756	0.2752		0.2756	0.2750		0.2756	0.2747	
8	0.3150	0.3146	0.3150	0.3147		0.3150	0.3146		0.3150	0.3144		0.3150	0.3141	
9	0.3543	0.3540	0.3543	0.3541	2 L / 3 T	0.3543	0.3540	4 L / 3 T	0.3543	0.3537	6 L / 3 T	0.3543	0.3535	9 L / 3 T
10	0.3937	0.3934	0.3937	0.3935		0.3937	0.3933		0.3937	0.3931		0.3937	0.3928	
12	0.4724	0.4721	0.4724	0.4721		0.4724	0.4720		0.4724	0.4717		0.4724	0.4714	
15	0.5906	0.5902	0.5906	0.5902	3 L / 3 T	0.5906	0.5901	4 L / 3 T	0.5906	0.5898	7 L / 3 T	0.5906	0.5895	11 L / 3 T
17	0.6693	0.6690	0.6693	0.6690		0.6693	0.6689		0.6693	0.6686		0.6693	0.6682	
20	0.7874	0.7870	0.7874	0.7870		0.7874	0.7869		0.7874	0.7866		0.7874	0.7861	
25	0.9843	0.9839	0.9843	0.9839	4 L / 4 T	0.9843	0.9837	5 L / 4 T	0.9843	0.9834	8 L / 4 T	0.9843	0.9830	13 L / 4 T
30	1.1811	1.1807	1.1811	1.1807		1.1811	1.1806		1.1811	1.1803		1.1811	1.1798	
35	1.3780	1.3775	1.3780	1.3775		1.3780	1.3773		1.3780	1.3770		1.3780	1.3764	
40	1.5748	1.5743	1.5748	1.5744		1.5748	1.5742		1.5748	1.5738		1.5748	1.5733	
45	1.7717	1.7712	1.7717	1.7712	4 L / 5 T	1.7717	1.7710	6 L / 5 T	1.7717	1.7707	10 L / 5 T	1.7717	1.7701	15 L / 5 T
50	1.9685	1.9680	1.9685	1.9681		1.9685	1.9679		1.9685	1.9675		1.9685	1.9670	
55	2.1654	2.1648	2.1654	2.1648		2.1654	2.1646		2.1654	2.1642		2.1654	2.1635	
60	2.3622	2.3616	2.3622	2.3617	5 L / 6 T	2.3622	2.3615		2.3622	2.3610		2.3622	2.3604	
65	2.5591	2.5585	2.5591	2.5585		2.5591	2.5583		2.5591	2.5579		2.5591	2.5572	
70	2.7559	2.7553	2.7559	2.7554		2.7559	2.7552	7 L / 6 T	2.7559	2.7547	12 L / 6 T	2.7559	2.7541	18 L / 6 T
75	2.9528	2.9522	2.9528	2.9522		2.9528	2.9520		2.9528	2.9516		2.9528	2.9509	
80	3.1496	3.1490	3.1496	3.1491		3.1496	3.1489		3.1496	3.1484		3.1496	3.1478	
85	3.3465	3.3457	3.3465	3.3459		3.3465	3.3456		3.3465	3.3451		3.3465	3.3443	
90	3.5433	3.5425	3.5433	3.5427		3.5433	3.5424		3.5433	3.5419		3.5433	3.5412	
95	3.7402	3.7394	3.7402	3.7396		3.7402	3.7393		3.7402	3.7388		3.7402	3.7380	
100	3.9370	3.9362	3.9370	3.9364	6L/8T	3.9370	3.9361	9L/8T	3.9370	3.9356	14 L / 8 T	3.9370	3.9349	21 L / 8 T
105	4.1339	4.1331	4.1339	4.1333		4.1339	4.1330		4.1339	4.1325		4.1339	4.1317	
110	4.3307	4.3299	4.3307	4.3301		4.3307	4.3298		4.3307	4.3293		4.3307	4.3286	
120	4.7244	4.7236	4.7244	4.7238		4.7244	4.7235		4.7244	4.7230		4.7244	4.7223	
130	5.1181	5.1171	5.1181	5.1174		5.1181	5.1171		5.1181	5.1165		5.1181	5.1156	
140	5.5118	5.5108	5.5118	5.5111		5.5118	5.5108		5.5118	5.5102		5.5118	5.5093	
150	5.9055	5.9045	5.9055	5.9048	7.1	5.9055	5.9045	101.1	5.9055	5.9039		5.9055	5.9030	251
160	6.2992	6.2982	6.2992	6.2985	7 L / 10 T	6.2992	6.2982	10 L / 10 T	6.2992	6.2976	16 L / 10 T	6.2992	6.2967	25 L / 10 T
170	6.6929	6.6919	6.6929	6.6922		6.6929	6.6919		6.6929	6.6913		6.6929	6.6904	
180	7.0866	7.0856	7.0866	7.0859		7.0866	7.0856		7.0866	7.0850		7.0866	7.0841	
190	7.4803	7.4791	7.4803	7.4795		7.4803	7.4792		7.4803	7.4785		7.4803	7.4775	
200	7.8740	7.8728	7.8740	7.8732	8 L / 12 T	7.8740	7.8729		7.8740	7.8722		7.8740	7.8712	
220	8.6614	8.6602	8.6614	8.6606		8.6614	8.6603	11 L / 12 T	8.6614	8.6596	18 L / 12 T	8.6614	8.6586	28 L / 12 T
240	9.4488	9.4476	9.4488	9.4480		9.4488	9.4477		9.4488	9.4470		9.4488	9.4460	
260	10.2362	10.2348	10.2362	10.2353		10.2362	10.2350		10.2362	10.2342		10.2362	10.2330	
280	11.0236	11.0222	11.0236	11.0227	9 L / 14 T	11.0236	11.0224	13 L / 14 T	11.0236	11.0216	20 L / 14 T	11.0236	11.0204	32 L / 14 T
300	11.8110	11.8096	11.8110	11.8101		11.8110	11.8098		11.8110	11.8090		11.8110	11.8078	



BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	h	5	RESULTING	h	6	RESULTING	h	7	RESULTING	h	8	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.5984	12.5974		12.5984	12.5970		12.5984	12.5962		12.5984	12.5949	
340	13.3858	13.3843	13.3858	13.3848		13.3858	13.3844		13.3858	13.3836		13.3858	13.3823	
360	14.1732	14.1717	14.1732	14.1722	10 L / 16 T	14.1732	14.1718	14 L / 16 T	14.1732	14.1710	22 L / 16 T	14.1732	14.1697	35 L / 16 T
380	14.9606	14.9591	14.9606	14.9596		14.9606	14.9592		14.9606	14.9584		14.9606	14.9571	
400	15.7480	15.7465	15.7480	15.7470		15.7480	15.7466		15.7480	15.7458		15.7480	15.7445	
420	16.5354	16.5337	16.5354	16.5344		16.5354	16.5339		16.5354	16.5330		16.5354	16.5316	
440	17.3228	17.3211	17.3228	17.3218		17.3228	17.3213		17.3228	17.3204		17.3228	17.3190	
460	18.1102	18.1085	18.1102	18.1092	11 L / 18 T	18.1102	18.1087	16 L / 18 T	18.1102	18.1078	25 L / 18 T	18.1102	18.1064	38 L / 18 T
480	18.8976	18.8959	18.8976	18.8966		18.8976	18.8961		18.8976	18.8952		18.8976	18.8938	
500	19.6850	19.6833	19.6850	19.6840		19.6850	19.6835		19.6850	19.6826		19.6850	19.6812	
530	20.8661	20.8642	20.8661	20.8650	11 L / 20 T	20.8661	20.8644		20.8661	20.8634		20.8661	20.8618	
560	22.0472	22.0453	22.0472	22.0461		22.0472	22.0455	17 L / 20 T	22.0472	22.0445	28 L / 20 T	22.0472	22.0429	43 L / 20 T
600	23.6220	23.6201	23.6220	23.6209	11 L / 20 I	23.6220	23.6203	17 L / 20 I	23.6220	23.6193	20 L / 20 I	23.6220	23.6177	43 L / 20 I
630	24.8031	24.8012	24.8031	24.8020		24.8031	24.8014		24.8031	24.8004		24.8031	24.7988	
670	26.3780	26.3750	26.3780	26.3767		26.3780	26.3760		26.3780	26.3748		26.3780	26.3730	
710	27.9528	27.9498	27.9528	27.9515	13 L / 30 T	27.9528	27.9508	20 L / 30 T	27.9528	27.9496	31 L / 30 T	27.9528	27.9478	49 L / 30 T
750	29.5276	29.5246	29.5276	29.5263	IJ L / JU I	29.5276	29.5256	201/301	29.5276	29.5244	51L/ 501	29.5276	29.5226	47 L / JU I
800	31.4961	31.4931	31.4961	31.4948		31.4961	31.4941		31.4961	31.4929		31.4961	31.4911	
850	33.4646	33.4606	33.4646	33.4631		33.4646	33.4624		33.4646	33.4610		33.4646	33.4591	
900	35.4331	35.4291	35.4331	35.4317	14 L / 39 T	35.4331	35.4309	22 L / 39 T	35.4331	35.4295	35 L / 39 T	35.4331	35.4276	55 L / 39 T
950	37.4016	37.3976	37.4016	37.4002	14 L / 37 I	37.4016	37.3994	22 L / 37 I	37.4016	37.3980	22 L / 24 L	37.4016	37.3961	22 L / 24 L
1000	39.3701	39.3661	39.3701	39.3687		39.3701	39.3679		39.3701	39.3665		39.3701	39.3646	
1060	41.7323	41.7274	41.7323	41.7306		41.7323	41.7297		41.7323	41.7281		41.7323	41.7258	
1120	44.0945	44.0896	44.0945	44.0928	17 L / 40 T	44.0945	44.0919	261 / 40 T	44.0945	44.0904	41 L / 40 T	44.0945	44.0880	(F L / 40 T
1180	46.4567	46.4518	46.4567	46.4550	17 L / 49 T	46.4567	46.4541	26 L / 49 T	46.4567	46.4526	41 L / 49 T	46.4567	46.4502	65 L / 49 T
1250	49.2126	49.2077	49.2126	49.2109		49.2126	49.2100		49.2126	49.2085		49.2126	49.2061	

Table 12 - Shaft Diameters and Resulting Fits

BEARII	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	h	9	RESULTING	h.	10	RESULTING	j	5	RESULTING	j	6	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
4	0.1575	0.1572	0.1575	0.1563		0.1575	0.1556		0.1576	0.1574		0.1577	0.1574	
5	0.1969	0.1965	0.1969	0.1957	12 L / 3 T	0.1969	0.1950	19 L / 3 T	0.1970	0.1968	1 L / 4 T	0.1971	0.1968	1L/6T
6	0.2362	0.2359	0.2362	0.2350		0.2362	0.2343		0.2363	0.2361		0.2365	0.2361	
7	0.2756	0.2753	0.2756	0.2742		0.2756	0.2733		0.2757	0.2755		0.2759	0.2755	
8	0.3150	0.3146	0.3150	0.3135		0.3150	0.3127		0.3151	0.3149		0.3152	0.3149	
9	0.3543	0.3540	0.3543	0.3529	14 L / 3 T	0.3543	0.3520	23 L / 3 T	0.3545	0.3543	1 L / 5 T	0.3546	0.3543	1 L / 6 T
10	0.3937	0.3934	0.3937	0.3923		0.3937	0.3914		0.3939	0.3936		0.3940	0.3936	
12	0.4724	0.4721	0.4724	0.4707		0.4724	0.4697		0.4726	0.4723		0.4728	0.4723	
15	0.5906	0.5902	0.5906	0.5889	17 L / 3 T	0.5906	0.5878	28 L / 3 T	0.5907	0.5904	1 L / 5 T	0.5909	0.5904	1 L / 6 T
17	0.6693	0.6690	0.6693	0.6676		0.6693	0.6665		0.6695	0.6692		0.6696	0.6692	
20	0.7874	0.7870	0.7874	0.7854		0.7874	0.7841		0.7876	0.7872		0.7878	0.7872	
25	0.9843	0.9839	0.9843	0.9822	20 L / 4 T	0.9843	0.9809	33 L / 4 T	0.9844	0.9841	2 L / 6 T	0.9846	0.9841	2 L / 7 T
30	1.1811	1.1807	1.1811	1.1791		1.1811	1.1778		1.1813	1.1809		1.1815	1.1809	
35	1.3780	1.3775	1.3780	1.3755		1.3780	1.3740		1.3782	1.3778		1.3784	1.3778	
40	1.5748	1.5743	1.5748	1.5724		1.5748	1.5709		1.5750	1.5746		1.5752	1.5746	
45	1.7717	1.7712	1.7717	1.7692	24 L / 5 T	1.7717	1.7677	39 L / 5 T	1.7719	1.7715	2 L / 7 T	1.7721	1.7715	2 L / 9 T
50	1.9685	1.9680	1.9685	1.9661		1.9685	1.9646		1.9687	1.9683		1.9689	1.9683	
55	2.1654	2.1648	2.1654	2.1624		2.1654	2.1606		2.1656	2.1651		2.1658	2.1651	
60	2.3622	2.3616	2.3622	2.3593	29 L / 6 T	2.3622	2.3575		2.3624	2.3619		2.3627	2.3619	
65	2.5591	2.5585	2.5591	2.5561		2.5591	2.5543		2.5593	2.5588		2.5595	2.5588	
70	2.7559	2.7553	2.7559	2.7530		2.7559	2.7512	47 L / 6 T	2.7561	2.7556	3 L / 8 T	2.7564	2.7556	3 L / 11 T
75	2.9528	2.9522	2.9528	2.9498		2.9528	2.9480		2.9530	2.9525		2.9532	2.9525	
80	3.1496	3.1490	3.1496	3.1467		3.1496	3.1449		3.1498	3.1493		3.1501	3.1493	
85	3.3465	3.3457	3.3465	3.3430		3.3465	3.3409		3.3467	3.3461		3.3470	3.3461	
90	3.5433	3.5425	3.5433	3.5399		3.5433	3.5378		3.5435	3.5430		3.5438	3.5430	
95	3.7402	3.7394	3.7402	3.7367		3.7402	3.7346		3.7404	3.7398		3.7407	3.7398	
100	3.9370	3.9362	3.9370	3.9336	34 L / 8 T	3.9370	3.9315	55 L / 8 T	3.9372	3.9367	4 L / 10 T	3.9375	3.9367	4 L / 13 T
105	4.1339	4.1331	4.1339	4.1304		4.1339	4.1283		4.1341	4.1335		4.1344	4.1335	
110	4.3307	4.3299	4.3307	4.3273		4.3307	4.3252		4.3309	4.3304		4.3312	4.3304	
120	4.7244	4.7236	4.7244	4.7210		4.7244	4.7189		4.7246	4.7241		4.7249	4.7241	
130	5.1181	5.1171	5.1181	5.1142		5.1181	5.1118		5.1184	5.1177		5.1187	5.1177	
140	5.5118	5.5108	5.5118	5.5079		5.5118	5.5055		5.5121	5.5114		5.5124	5.5114	
150	5.9055	5.9045	5.9055	5.9016	201 (12.	5.9055	5.8992		5.9058	5.9051		5.9061	5.9051	
160	6.2992	6.2982	6.2992	6.2953	39 L / 10 T	6.2992	6.2929	63 L / 10 T	6.2995	6.2988	4 L / 13 T	6.2998	6.2988	4 L / 15 T
170	6.6929	6.6919	6.6929	6.6890		6.6929	6.6866		6.6932	6.6925		6.6935	6.6925	
180	7.0866	7.0856	7.0866	7.0827		7.0866	7.0803		7.0869	7.0862		7.0872	7.0862	
190	7.4803	7.4791	7.4803	7.4758		7.4803	7.4730		7.4806	7.4798		7.4809	7.4798	
200	7.8740	7.8728	7.8740	7.8695	45 L / 12 T	7.8740	7.8667		7.8743	7.8735		7.8746	7.8735	
220	8.6614	8.6602	8.6614	8.6569		8.6614	8.6541	73 L / 12 T	8.6617	8.6609	5 L / 15 T	8.6620	8.6609	5 L / 18 T
240	9.4488	9.4476	9.4488	9.4443		9.4488	9.4415		9.4491	9.4483		9.4494	9.4483	
260	10.2362	10.2348	10.2362	10.2311		10.2362	10.2280		10.2365	10.2356		10.2369	10.2356	
280	11.0236	11.0222	11.0236	11.0185	51 L / 14 T	11.0236	11.0154	83 L / 14 T	11.0239	11.0230	6 L / 17 T	11.0243	11.0230	6 L / 20 T
300	11.8110	11.8096	11.8110	11.8059		11.8110	11.8028		11.8113	11.8104		11.8117	11.8104	



BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	h	9	RESULTING	h	10	RESULTING	j	5	RESULTING	j	6	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.5984	12.5929		12.5984	12.5894		12.5987	12.5977		12.5991	12.5977	
340	13.3858	13.3843	13.3858	13.3803		13.3858	13.3768		13.3861	13.3851		13.3865	13.3851	
360	14.1732	14.1717	14.1732	14.1677	55 L / 16 T	14.1732	14.1642	91 L / 16 T	14.1735	14.1725	7 L / 19 T	14.1739	14.1725	7 L / 23 T
380	14.9606	14.9591	14.9606	14.9551		14.9606	14.9516		14.9609	14.9599		14.9613	14.9599	
400	15.7480	15.7465	15.7480	15.7425		15.7480	15.7390		15.7483	15.7473		15.7487	15.7473	
420	16.5354	16.5337	16.5354	16.5293		16.5354	16.5256		16.5357	16.5346		16.5362	16.5346	
440	17.3228	17.3211	17.3228	17.3167		17.3228	17.3130		17.3231	17.3220		17.3236	17.3220	
460	18.1102	18.1085	18.1102	18.1041	61 L / 18 T	18.1102	18.1004	98 L / 18 T	18.1105	18.1094	8 L / 20 T	18.1110	18.1094	8 L / 26 T
480	18.8976	18.8959	18.8976	18.8915		18.8976	18.8878		18.8979	18.8969		18.8984	18.8969	
500	19.6850	19.6833	19.6850	19.6789		19.6850	19.6752		19.6853	19.6843		19.6858	19.6843	
530	20.8661	20.8642	20.8661	20.8593		20.8661	20.8551					20.8670	20.8653	
560	22.0472	22.0453	22.0472	22.0404	69 L / 20 T	22.0472	22.0362	110 L / 20 T				22.0481	22.0464	9 L / 28 T
600	23.6220	23.6201	23.6220	23.6152	07L/201	23.6220	23.6110	110 L / 20 I				23.6229	23.6212	7 L / ZO I
630	24.8031	24.8012	24.8031	24.7963		24.8031	24.7921					24.8040	24.8023	
670	26.3780	26.3750	26.3780	26.3701		26.3780	26.3654					26.3789	26.3770	
710	27.9528	27.9498	27.9528	27.9449	79 L / 30 T	27.9528	27.9402	126 L / 30 T				27.9537	27.9518	10 L / 39 T
750	29.5276	29.5246	29.5276	29.5197	/7L/ 301	29.5276	29.5150	120 L / 30 I				29.5285	29.5266	10 L / 37 I
800	31.4961	31.4931	31.4961	31.4882		31.4961	31.4835					31.4970	31.4951	
850	33.4646	33.4606	33.4646	33.4555		33.4646	33.4504					33.4657	33.4635	
900	35.4331	35.4291	35.4331	35.4240	91 L / 39 T	35.4331	35.4189	142 L / 39 T				35.4342	35.4320	11 L / 50 T
950	37.4016	37.3976	37.4016	37.3925	JIL/ 391	37.4016	37.3874	142 L / 37 I				37.4027	37.4005	111/301
1000	39.3701	39.3661	39.3701	39.3610		39.3701	39.3559					39.3712	39.3690	
1060	41.7323	41.7274	41.7323	41.7220		41.7323	41.7157					41.7336	41.7310	
1120	44.0945	44.0896	44.0945	44.0843	102 L / 49 T	44.0945	44.0780	1/EL / 40 T				44.0958	44.0932	12 L / / 2 T
1180	46.4567	46.4518	46.4567	46.4465	102 L / 49 I	46.4567	46.4402	165 L / 49 T				46.4580	46.4554	13 L / 62 T
1250	49.2126	49.2077	49.2126	49.2024		49.2126	49.1961					49.2139	49.2113	

Table 12 - Shaft Diameters and Resulting Fits

BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	j	7	RESULTING	js	;4	RESULTING	js	5	RESULTING	js	6	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
4	0.1575	0.1572	0.1578	0.1573		0.1576	0.1574		0.1576	0.1574		0.1576	0.1573	
5	0.1969	0.1965	0.1972	0.1967	2 L / 6 T	0.1969	0.1968	1 L / 4 T	0.1969	0.1968	1 L / 4 T	0.1970	0.1967	2 L / 5 T
6	0.2362	0.2359	0.2365	0.2361		0.2363	0.2361	, ,	0.2363	0.2361	,	0.2364	0.2361	
7	0.2756	0.2753	0.2760	0.2754		0.2757	0.2755		0.2757	0.2755		0.2758	0.2754	
8	0.3150	0.3146	0.3154	0.3148		0.3150	0.3149		0.3151	0.3148		0.3151	0.3148	
9	0.3543	0.3540	0.3547	0.3541	2 L / 7 T	0.3544	0.3543	1 L / 4 T	0.3544	0.3542	1 L / 4 T	0.3545	0.3542	2 L / 5 T
10	0.3937	0.3934	0.3941	0.3935		0.3938	0.3936		0.3938	0.3936		0.3939	0.3935	
12	0.4724	0.4721	0.4729	0.4722		0.4725	0.4723		0.4726	0.4723		0.4727	0.4722	
15	0.5906	0.5902	0.5910	0.5903	2 L / 8 T	0.5906	0.5905	1L/4T	0.5907	0.5904	2 L / 5 T	0.5908	0.5903	2 L / 5 T
17	0.6693	0.6690	0.6698	0.6691		0.6694	0.6692		0.6694	0.6691		0.6695	0.6691	
20	0.7874	0.7870	0.7879	0.7871		0.7875	0.7873		0.7876	0.7872		0.7877	0.7871	
25	0.9843	0.9839	0.9848	0.9839	3 L / 9 T	0.9844	0.9841	1L/5T	0.9844	0.9841	2 L / 6 T	0.9845	0.9840	3L/6T
30	1.1811	1.1807	1.1816	1.1808		1.1812	1.1810		1.1813	1.1809		1.1814	1.1808	
35	1.3780	1.3775	1.3785	1.3776		1.3781	1.3778		1.3782	1.3777		1.3783	1.3776	
40	1.5748	1.5743	1.5754	1.5744		1.5749	1.5747		1.5750	1.5746		1.5751	1.5745	
45	1.7717	1.7712	1.7722	1.7713	4 L / 11 T	1.7718	1.7715	1 L / 6 T	1.7719	1.7714	2 L / 7 T	1.7720	1.7713	3 L / 8 T
50	1.9685	1.9680	1.9691	1.9681		1.9686	1.9684		1.9687	1.9683		1.9688	1.9682	
55	2.1654	2.1648	2.1661	2.1649		2.1655	2.1652		2.1656	2.1651		2.1657	2.1650	
60	2.3622	2.3616	2.3629	2.3617	5 L / 13 T -	2.3624	2.3620		2.3625	2.3619		2.3626	2.3618	
65	2.5591	2.5585	2.5598	2.5586		2.5592	2.5589		2.5593	2.5588		2.5594	2.5587	
70	2.7559	2.7553	2.7566	2.7554		2.7561	2.7557	2 L / 7 T	2.7562	2.7556	3 L / 8 T	2.7563	2.7555	4 L / 10 T
75	2.9528	2.9522	2.9535	2.9523		2.9529	2.9526		2.9530	2.9525		2.9531	2.9524	
80	3.1496	3.1490	3.1503	3.1491		3.1498	3.1494		3.1499	3.1494		3.1500	3.1492	
85	3.3465	3.3457	3.3472	3.3459		3.3467	3.3463		3.3468	3.3462		3.3469	3.3460	
90	3.5433	3.5425	3.5441	3.5427		3.5435	3.5431		3.5436	3.5430		3.5437	3.5429	
95	3.7402	3.7394	3.7409	3.7396		3.7404	3.7400		3.7405	3.7399		3.7406	3.7397	
100	3.9370	3.9362	3.9378	3.9364	6 L / 16 T	3.9372	3.9368	2 L / 10 T	3.9373	3.9367	3 L / 11 T	3.9374	3.9366	4 L / 12 T
105	4.1339	4.1331	4.1346	4.1333		4.1341	4.1337		4.1342	4.1336		4.1343	4.1334	
110	4.3307	4.3299	4.3315	4.3301		4.3309	4.3305		4.3310	4.3304		4.3311	4.3303	
120	4.7244	4.7236	4.7252	4.7238		4.7246	4.7242		4.7247	4.7241		4.7248	4.7240	
130	5.1181	5.1171	5.1190	5.1174		5.1183	5.1179		5.1185	5.1178		5.1186	5.1176	
140	5.5118	5.5108	5.5127	5.5111		5.5120	5.5116		5.5122	5.5115		5.5123	5.5113	
150	5.9055	5.9045	5.9064	5.9048	7 L / 19 T	5.9057	5.9053	2 L / 12 T	5.9059	5.9052	4 L / 13 T	5.9060	5.9050	5 L / 15 T
160	6.2992	6.2982	6.3001	6.2985	/ L / 191	6.2994	6.2990	2 L / 12 I	6.2996	6.2989	41/101	6.2997	6.2987	51/151
170	6.6929	6.6919	6.6938	6.6922		6.6931	6.6927		6.6933	6.6926		6.6934	6.6924	
180	7.0866	7.0856	7.0875	7.0859		7.0869	7.0864		7.0870	7.0863		7.0871	7.0861	
190	7.4803	7.4791	7.4813	7.4795		7.4806	7.4800		7.4807	7.4799		7.4809	7.4797	
200	7.8740	7.8728	7.8750	7.8732	8 L / 22 T	7.8743	7.8737	3 L / 15 T	7.8744	7.8736	4 L / 16 T	7.8746	7.8734	6 L / 18 T
220	8.6614	8.6602	8.6624	8.6606		8.6617	8.6611	51/151	8.6618	8.6610	41/101	8.6620	8.6608	01/101
240	9.4488	9.4476	9.4498	9.4480		9.4491	9.4485		9.4492	9.4484		9.4494	9.4482	
260	10.2362	10.2348	10.2372	10.2352		10.2365	10.2359		10.2367	10.2358		10.2369	10.2356	
280	11.0236	11.0222	11.0246	11.0226	10 L / 24 T	11.0239	11.0233	3 L / 17 T	11.0241	11.0232	5 L / 18 T	11.0243	11.0230	6 L / 20 T
300	11.8110	11.8096	11.8120	11.8100		11.8113	11.8107		11.8115	11.8106		11.8117	11.8104	



BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	in		j7		RESULTING	js4		RESULTING	js5		RESULTING	js6		RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.5996	12.5973		12.5988	12.5981		12.5989	12.5979		12.5991	12.5977	
340	13.3858	13.3843	13.3870	13.3847		13.3862	13.3855		13.3863	13.3853		13.3865	13.3851	
360	14.1732	14.1717	14.1744	14.1721	11 L / 27 T	14.1736	14.1729	4 L / 19 T	14.1737	14.1727	5 L / 21 T	14.1739	14.1725	7 L / 23 T
380	14.9606	14.9591	14.9618	14.9595		14.9610	14.9603		14.9611	14.9601		14.9613	14.9599	
400	15.7480	15.7465	15.7492	15.7469		15.7484	15.7477		15.7485	15.7475		15.7487	15.7473	
420	16.5354	16.5337	16.5367	16.5342		16.5358	16.5350		16.5360	16.5349		16.5362	16.5346	
440	17.3228	17.3211	17.3241	17.3216		17.3232	17.3224		17.3234	17.3223	5 L / 23 T	17.3236	17.3220	8 L / 26 T
460	18.1102	18.1085	18.1115	18.1090	13 L / 30 T	18.1106	18.1098	4 L / 22 T	18.1108	18.1097		18.1110	18.1094	
480	18.8976	18.8959	18.8989	18.8964		18.8980	18.8972		18.8982	18.8971		18.8984	18.8969	
500	19.6850	19.6833	19.6863	19.6838		19.6854	19.6846		19.6856	19.6845		19.6858	19.6843	
530	20.8661	20.8642							20.8667	20.8656		20.8670	20.8653	
560	22.0472	22.0453							22.0478	22.0467	6 L / 25 T	22.0481	22.0464	9 L / 28 T
600	23.6220	23.6201							23.6226	23.6215	0 L / Z5 I	23.6229	23.6212	7 L / 20 I
630	24.8031	24.8012							24.8037	24.8026		24.8040	24.8023	
670	26.3780	26.3750							26.3786	26.3773		26.3789	26.3770	10 L / 39 T
710	27.9528	27.9498							27.9534	27.9521	6 L / 36 T	27.9537	27.9518	
750	29.5276	29.5246							29.5282	29.5269	01/301	29.5285	29.5266	10 L / 37 I
800	31.4961	31.4931							31.4967	31.4954		31.4970	31.4951	
850	33.4646	33.4606							33.4653	33.4639		33.4657	33.4635	
900	35.4331	35.4291							35.4338	35.4324	71 / 44 1	35.4342	35.4320	11 L / 50 T
950	37.4016	37.3976							37.4023	37.4009	7 L / 46 T	37.4027	37.4005	11L/ 501
1000	39.3701	39.3661							39.3708	39.3694		39.3712	39.3690	
1060	41.7323	41.7274							41.7331	41.7315		41.7336	41.7310	
1120	44.0945	44.0896							44.0953	44.0937	01/577	44.0958	44.0932	12 L / / 2 T
1180	46.4567	46.4518							46.4575	46.4559	8 L / 57 T	46.4580	46.4554	13 L / 62 T
1250	49.2126	49.2077							49.2134	49.2118		49.2139	49.2113	

Table 12 - Shaft Diameters and Resulting Fits

BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	in k4		RESULTING	k5		RESULTING	k6		RESULTING	k7		RESULTING	
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
4	0.1575	0.1572	0.1577	0.1575		0.1577	0.1575		0.1578	0.1575		0.1580	0.1575	
5	0.1969	0.1965	0.1970	0.1969	0 T / 5 T	0.1971	0.1969	0T/6T	0.1970	0.1969	0 T / 7 T	0.1974	0.1969	0T/8T
6	0.2362	0.2359	0.2364	0.2363	01/01	0.2365	0.2363	0.701	0.2366	0.2363	0.777	0.2367	0.2363	01/01
7	0.2756	0.2753	0.2758	0.2756		0.2759	0.2756		0.2760	0.2756		0.2762	0.2756	
8	0.3150	0.3146	0.3152	0.3150		0.3152	0.3150		0.3154	0.3150		0.3156	0.3150	
9	0.3543	0.3540	0.3545	0.3544	0 T / 5 T	0.3546	0.3544	0 T / 6 T	0.3547	0.3544	0 T / 7 T	0.3550	0.3544	0 T / 9 T
10	0.3937	0.3934	0.3939	0.3937		0.3940	0.3937		0.3941	0.3937		0.3943	0.3937	
12	0.4724	0.4721	0.4727	0.4725		0.4728	0.4725		0.4729	0.4725		0.4732	0.4725	
15	0.5906	0.5902	0.5908	0.5906	0 T / 6 T	0.5909	0.5906	0 T / 7 T	0.5910	0.5906	0 T / 8 T	0.5913	0.5906	0 T / 11 T
17	0.6693	0.6690	0.6695	0.6693		0.6696	0.6693		0.6698	0.6693		0.6700	0.6693	
20	0.7874	0.7870	0.7877	0.7875		0.7878	0.7875		0.7880	0.7875		0.7883	0.7875	1 T / 13 T
25	0.9843	0.9839	0.9846	0.9843	1 T / 7 T	0.9847	0.9843	0 T / 8 T	0.9848	0.9843	1 T / 10 T	0.9852	0.9843	
30	1.1811	1.1807	1.1814	1.1812		1.1815	1.1812		1.1817	1.1812		1.1820	1.1812	
35	1.3780	1.3775	1.3783	1.3780	11/81	1.3785	1.3780	1 T / 10 T	1.3787	1.3780	1 T / 12 T	1.3790	1.3780	1 T / 15 T
40	1.5748	1.5743	1.5752	1.5749		1.5753	1.5749		1.5755	1.5749		1.5759	1.5749	
45	1.7717	1.7712	1.7720	1.7717		1.7722	1.7717		1.7724	1.7717		1.7727	1.7717	
50	1.9685	1.9680	1.9689	1.9686		1.9690	1.9686		1.9692	1.9686		1.9696	1.9686	
55	2.1654	2.1648	2.1657	2.1654	1 T / 10 T	2.1659	2.1654	1 T / 12 T	2.1662	2.1654		2.1666	2.1654	
60	2.3622	2.3616	2.3626	2.3623		2.3628	2.3623		2.3630	2.3623		2.3635	2.3623	
65	2.5591	2.5585	2.5594	2.5591		2.5596	2.5591		2.5599	2.5591	1 T / 14 T	2.5603	2.5591	1 T / 19 T
70	2.7559	2.7553	2.7563	2.7560		2.7565	2.7560		2.7567	2.7560	11/141	2.7572	2.7560	,
75	2.9528	2.9522	2.9531	2.9528		2.9533	2.9528		2.9536	2.9528		2.9540	2.9528	
80	3.1496	3.1490	3.1500	3.1497		3.1502	3.1497		3.1504	3.1497		3.1509	3.1497	
85	3.3465	3.3457	3.3470	3.3466		3.3472	3.3466		3.3474	3.3466	1 T / 18 T	3.3480	3.3466	1 T / 23 T
90	3.5433	3.5425	3.5438	3.5434		3.5440	3.5434		3.5443	3.5434		3.5448	3.5434	
95	3.7402	3.7394	3.7407	3.7403		3.7409	3.7403		3.7411	3.7403		3.7417	3.7403	
100	3.9370	3.9362	3.9375	3.9371	1 T / 13 T	3.9377	3.9371	1 T / 15 T	3.9380	3.9371		3.9385	3.9371	
105	4.1339	4.1331	4.1344	4.1340		4.1346	4.1340		4.1348	4.1340		4.1354	4.1340	
110	4.3307	4.3299	4.3312	4.3308		4.3314	4.3308		4.3317	4.3308		4.3322	4.3308	
120	4.7244	4.7236	4.7249	4.7245		4.7251	4.7245		4.7254	4.7245		4.7259	4.7245	
130	5.1181	5.1171	5.1187	5.1182		5.1189	5.1182		5.1192	5.1182		5.1198	5.1182	
140	5.5118	5.5108	5.5124	5.5119		5.5126	5.5119		5.5129	5.5119		5.5135	5.5119	
150	5.9055	5.9045	5.9061	5.9056	1 T / 16 T	5.9063	5.9056	1 T / 18 T	5.9066	5.9056	1 T / 21 T	5.9072	5.9056	1 T / 27 T
160	6.2992	6.2982	6.2998	6.2993		6.3000	6.2993		6.3003	6.2993		6.3009	6.2993	
170	6.6929	6.6919	6.6935	6.6930		6.6937	6.6930		6.6940	6.6930		6.6946	6.6930	
180	7.0866	7.0856	7.0872	7.0867		7.0874	7.0867		7.0877	7.0867		7.0883	7.0867	
190	7.4803	7.4791	7.4810	7.4805		7.4813	7.4805		7.4816	7.4805		7.4823	7.4805	
200	7.8740	7.8728	7.8747	7.8742	2 T / 19 T	7.8750	7.8742	2 T / 21 T	7.8753	7.8742	2 T / 25 T	7.8760	7.8742	2 T / 31 T
220	8.6614	8.6602	8.6621	8.6616		8.6624	8.6616		8.6627	8.6616	,	8.6634	8.6616	,
240	9.4488	9.4476	9.4495	9.4490		9.4498	9.4490		9.4501	9.4490		9.4508	9.4490	
260	10.2362	10.2348	10.2370	10.2364		10.2373	10.2364		10.2376	10.2364		10.2384	10.2364	
280	11.0236	11.0222	11.0244	11.0238	2 T / 22 T	11.0247	11.0238	2 T / 24 T	11.0250	11.0238	2 T / 28 T	11.0258	11.0238	2 T / 36 T
300	11.8110	11.8096	11.8118	11.8112		11.8121	11.8112		11.8124	11.8112		11.8132	11.8112	



BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	in		k4		RESULTING	k5		RESULTING	k6		RESULTING	k7		RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.5993	12.5986		12.5996	12.5986		12.6000	12.5986		12.6008	12.5986	
340	13.3858	13.3843	13.3867	13.3860		13.3870	13.3860		13.3874	13.3860		13.3882	13.3860	
360	14.1732	14.1717	14.1741	14.1734	2 T / 24 T	14.1744	14.1734	2 T / 27 T	14.1748	14.1734	2 T / 31 T	14.1756	14.1734	2 T / 40 T
380	14.9606	14.9591	14.9615	14.9608		14.9618	14.9608		14.9622	14.9608		14.9630	14.9608	
400	15.7480	15.7465	15.7489	15.7482		15.7492	15.7482		15.7496	15.7482		15.7504	15.7482	
420	16.5354	16.5337	16.5364	16.5356		16.5367	16.5356	2 T / 30 T	16.5372	16.5356		16.5381	16.5356	2 T / 44 T
440	17.3228	17.3211	17.3238	17.3230		17.3241	17.3230		17.3246	17.3230	2 T / 35 T	17.3255	17.3230	
460	18.1102	18.1085	18.1112	18.1104	2 T / 28 T	18.1115	18.1104		18.1120	18.1104		18.1129	18.1104	
480	18.8976	18.8959	18.8986	18.8978		18.8989	18.8978		18.8994	18.8978		18.9003	18.8978	
500	19.6850	19.6833	19.6860	19.6852		19.6863	19.6852		19.6868	19.6852		19.6877	19.6852	
530	20.8661	20.8642				20.8673	20.8661	0T/ 31T	20.8679	20.8661		20.8689	20.8661	
560	22.0472	22.0453				22.0484	22.0472		22.0490	22.0472	0 T / 37 T	22.0500	22.0472	0 T / 47 T
600	23.6220	23.6201				23.6232	23.6220		23.6238	23.6220	01/ 5/ 1	23.6248	23.6220	
630	24.8031	24.8012				24.8043	24.8031		24.8049	24.8031		24.8059	24.8031	
670	26.3780	26.3750				26.3792	26.3780		26.3799	26.3780		26.3811	26.3780	0 T / 61 T
710	27.9528	27.9498				27.9540	27.9528	0 T / 42 T	27.9547	27.9528	0 T / 49 T	27.9559	27.9528	
750	29.5276	29.5246				29.5288	29.5276	01/421	29.5295	29.5276	01/471	29.5307	29.5276	
800	31.4961	31.4931				31.4973	31.4961		31.4980	31.4961		31.4992	31.4961	
850	33.4646	33.4606				33.4660	33.4646		33.4668	33.4646		33.4681	33.4646	
900	35.4331	35.4291				35.4345	35.4331	0 T / 54 T	35.4353	35.4331	0T/61T	35.4366	35.4331	0 T / 75 T
950	37.4016	37.3976				37.4030	37.4016	01/ 341	37.4038	37.4016	01/011	37.4051	37.4016	01/751
1000	39.3701	39.3661				39.3715	39.3701		39.3723	39.3701		39.3736	39.3701	
1060	41.7323	41.7274				41.7339	41.7323		41.7349	41.7323		41.7364	41.7323	0T/91T
1120	44.0945	44.0896				44.0961	44.0945	0 T / 66 T	44.0971	44.0945	0 T / 75 T	44.0986	44.0945	
1180	46.4567	46.4518				46.4583	46.4567	01/001	46.4593	46.4567	0 T / 75 T	46.4608	46.4567	01/911
1250	49.2126	49.2077				49.2143	49.2126		49.2152	49.2126		49.2167	49.2126	

Table 12 - Shaft Diameters and Resulting Fits

BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	mm i		in m5		RESULTING m6		16	RESULTING		n5		n6		RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	RESULTING FIT	max	min	FIT
4	0.1575	0.1572	0.1578	0.1576		0.1580	0.1576		0.1580	0.1578		0.1581	0.1578	
5	0.1969	0.1965	0.1972	0.1970	2 T / 7 T	0.1973	0.1970	2 T / 8 T	0.1974	0.1972	3 T / 8 T	0.1975	0.1972	3T/9T
6	0.2362	0.2359	0.2366	0.2364	2 . , , , .	0.2367	0.2364	21/01	0.2367	0.2365	5.701	0.2369	0.2365	51/51
7	0.2756	0.2753	0.2761	0.2758		0.2762	0.2758		0.2762	0.2760		0.2763	0.2760	
8	0.3150	0.3146	0.3154	0.3152		0.3156	0.3152		0.3156	0.3154		0.3157	0.3154	4 T / 11 T
9	0.3543	0.3540	0.3548	0.3546	2 T / 8 T	0.3549	0.3546	2 T / 9 T	0.3550	0.3547	4 T / 9 T	0.3551	0.3547	
10	0.3937	0.3934	0.3942	0.3939		0.3943	0.3939		0.3943	0.3941		0.3944	0.3941	
12	0.4724	0.4721	0.4730	0.4727		0.4731	0.4727		0.4732	0.4729		0.4733	0.4729	
15	0.5906	0.5902	0.5911	0.5908	3 T / 9 T	0.5913	0.5908	3 T / 10 T	0.5913	0.5910	5 T / 11 T	0.5915	0.5910	5 T / 12 T
17	0.6693	0.6690	0.6699	0.6696	,	0.6700	0.6696	. '	0.6701	0.6698	,	0.6702	0.6698	51/121
20	0.7874	0.7870	0.7881	0.7877		0.7882	0.7877		0.7883	0.7880		0.7885	0.7880	
25	0.9843	0.9839	0.9849	0.9846	3 T / 11 T	0.9851	0.9846	3 T / 12 T	0.9852	0.9848	6 T / 13 T	0.9854	0.9848	6 T / 15 T
30	1.1811	1.1807	1.1818	1.1814		1.1819	1.1814	,	1.1820	1.1817	,	1.1822	1.1817	
35	1.3780	1.3775	1.3787	1.3783		1.3789	1.3783	4 T / 15 T	1.3791	1.3786	7 T / 16 T	1.3793	1.3786	
40	1.5748	1.5743	1.5756	1.5752	4 T / 13 T	1.5758	1.5752		1.5759	1.5755		1.5761	1.5755	
45	1.7717	1.7712	1.7724	1.7720		1.7726	1.7720		1.7728	1.7723		1.7730	1.7723	7 T / 18 T
50	1.9685	1.9680	1.9693	1.9689		1.9695	1.9689		1.9696	1.9692		1.9698	1.9692	
55	2.1654	2.1648	2.1663	2.1658	4 T / 15 T	2.1665	2.1658	4 T / 18 T	2.1667	2.1661		2.1669	2.1661	
60	2.3622	2.3616	2.3631	2.3626		2.3634	2.3626		2.3635	2.3630		2.3637	2.3630	
65	2.5591	2.5585	2.5600	2.5595		2.5602	2.5595		2.5604	2.5598	(2.5606	2.5598	/
70	2.7559	2.7553	2.7569	2.7563		2.7571	2.7563		2.7572	2.7567	8 T / 19 T	2.7574	2.7567	8 T / 21 T
75	2.9528	2.9522	2.9537	2.9532		2.9539	2.9532		2.9541	2.9535		2.9543	2.9535	
80	3.1496	3.1490	3.1506	3.1500		3.1508	3.1500		3.1509	3.1504		3.1511	3.1504	
85	3.3465	3.3457	3.3476	3.3470		3.3478	3.3470		3.3480	3.3474	9 T / 23 T	3.3482	3.3474	9 T / 26 T
90	3.5433	3.5425	3.5444	3.5438		3.5447	3.5438		3.5448	3.5442		3.5451	3.5442	
95	3.7402	3.7394	3.7413	3.7407		3.7415	3.7407		3.7417	3.7411		3.7419	3.7411	
100	3.9370	3.9362	3.9381	3.9375	5 T / 19 T	3.9384	3.9375	5 T / 22 T	3.9385	3.9379		3.9388	3.9379	
105	4.1339	4.1331	4.1350	4.1344		4.1352	4.1344		4.1354	4.1348		4.1356	4.1348	
110	4.3307	4.3299	4.3318	4.3312		4.3321	4.3312		4.3322	4.3316		4.3325	4.3316	
120	4.7244	4.7236	4.7255	4.7249		4.7258	4.7249		4.7259	4.7253		4.7262	4.7253	
130	5.1181	5.1171	5.1194	5.1187		5.1197	5.1187		5.1199	5.1192		5.1202	5.1192	
140	5.5118	5.5108	5.5131	5.5124		5.5134	5.5124		5.5136	5.5129		5.5139	5.5129	
150	5.9055	5.9045	5.9068	5.9061	6 T / 23 T	5.9071	5.9061	6 T / 26 T	5.9073	5.9066	11 T / 28 T	5.9076	5.9066	11 T / 30 T
160	6.2992	6.2982	6.3005	6.2998	0.7251	6.3008	6.2998	0.7201	6.3010	6.3003	, 201	6.3013	6.3003	
170	6.6929	6.6919	6.6942	6.6935		6.6945	6.6935		6.6947	6.6940		6.6950	6.6940	
180	7.0866	7.0856	7.0879	7.0872		7.0882	7.0872		7.0884	7.0877		7.0887	7.0877	
190	7.4803	7.4791	7.4818	7.4810		7.4821	7.4810		7.4823	7.4815		7.4827	7.4815	
200	7.8740	7.8728	7.8755	7.8747	7 T / 26 T	7.8758	7.8747	7 T / 30 T	7.8760	7.8752	12 T / 32 T	7.8764	7.8752	12 T / 35 T
220	8.6614	8.6602	8.6629	8.6621	, _0 .	8.6632	8.6621		8.6634	8.6626	121/321	8.6638	8.6626	121/331
240	9.4488	9.4476	9.4503	9.4495		9.4506	9.4495		9.4508	9.4500		9.4512	9.4500	
260	10.2362	10.2348	10.2379	10.2370		10.2383	10.2370		10.2385	10.2376		10.2388	10.2376	
280	11.0236	11.0222	11.0253	11.0244	8 T / 31 T	11.0257	11.0244	8 T / 34 T	11.0259	11.0250	13 T / 36 T	11.0262	11.0250	13 T / 40 T
300	11.8110	11.8096	11.8127	11.8118		11.8131	11.8118		11.8133	11.8124		11.8136	11.8124	



BEARI	NG BORE DIA	METER					SHAFT	DIAMETER / RE	SULTING FIT	(0.0001″)				
mm	i	n	m	15	RESULTING	m	16	RESULTING	n	5	RESULTING	n	6	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.6002	12.5993		12.6007	12.5993		12.6009	12.5999		12.6013	12.5999	
340	13.3858	13.3843	13.3876	13.3867		13.3881	13.3867		13.3883	13.3873		13.3887	13.3873	
360	14.1732	14.1717	14.1750	14.1741	8 / 34 T	14.1755	14.1741	8 T / 38 T	14.1757	14.1747	15 T / 40 T	14.1761	14.1747	15 T / 44 T
380	14.9606	14.9591	14.9624	14.9615		14.9629	14.9615		14.9631	14.9621		14.9635	14.9621	
400	15.7480	15.7465	15.7498	15.7489		15.7503	15.7489		15.7505	15.7495		15.7509	15.7495	
420	16.5354	16.5337	16.5374	16.5363		16.5379	16.5363		16.5381	16.5370		16.5386	16.5370	
440	17.3228	17.3211	17.3248	17.3237		17.3253	17.3237		17.3255	17.3244		17.3260	17.3244	
460	18.1102	18.1085	18.1122	18.1111	9 T / 37 T	18.1127	18.1111	9 T / 43 T	18.1129	18.1118	16 T / 44 T	18.1134	18.1118	16 T / 49 T
480	18.8976	18.8959	18.8996	18.8985		18.9001	18.8985		18.9003	18.8992		18.9008	18.8992	
500	19.6850	19.6833	19.6870	19.6859		19.6875	19.6859		19.6877	19.6866		19.6882	19.6866	
530	20.8661	20.8642	20.8683	20.8672		20.8689	20.8672		20.8690	20.8679		20.8696	20.8679	
560	22.0472	22.0453	22.0494	22.0483	10 T / 41 T	22.0500	22.0483	10 T / 47 T	22.0501	22.0490	17 T / 48 T	22.0507	22.0490	17 T / 54 T
600	23.6220	23.6201	23.6242	23.6231	101/411	23.6248	23.6231	101/4/1	23.6249	23.6238	17 1 / 40 1	23.6255	23.6238	171/341
630	24.8031	24.8012	24.8053	24.8042		24.8059	24.8042		24.8060	24.8049		24.8066	24.8049	
670	26.3780	26.3750	26.3804	26.3791		26.3811	26.3791		26.3812	26.3799		26.3819	26.3799	
710	27.9528	27.9498	27.9552	27.9539	12 T / 54 T	27.9559	27.9539	12 T / 61 T	27.9560	27.9547	20 T / 62 T	27.9567	27.9547	20 T / 69 T
750	29.5276	29.5246	29.5300	29.5287	121/341	29.5307	29.5287	121/011	29.5308	29.5295	2017 021	29.5315	29.5295	2017 071
800	31.4961	31.4931	31.4985	31.4972		31.4992	31.4972		31.4993	31.4980		31.5000	31.4980	
850	33.4646	33.4606	33.4673	33.4659		33.4681	33.4659		33.4682	33.4668		33.4690	33.4668	
900	35.4331	35.4291	35.4358	35.4344	13 T / 67 T	35.4366	35.4344	13 T / 75 T	35.4367	35.4353	22 T / 76 T	35.4375	35.4353	22 T / 83 T
950	37.4016	37.3976	37.4043	37.4029	131/071	37.4051	37.4029	131/131	37.4052	37.4038	221/701	37.4060	37.4038	221/001
1000	39.3701	39.3661	39.3728	39.3714		39.3736	39.3714		39.3737	39.3723		39.3745	39.3723	
1060	41.7323	41.7274	41.7355	41.7339		41.7365	41.7339		41.7365	41.7349		41.7375	41.7349	
1120	44.0945	44.0896	44.0977	44.0961	16 T / 81 T	44.0987	44.0961	16 T / 91 T	44.0987	44.0971	26 T / 92 T	44.0997	44.0971	26 T / 101 T
1180	46.4567	46.4518	46.4599	46.4583	101/011	46.4609	46.4583	101/911	46.4609	46.4593	201/921	46.4619	46.4593	2017 1011
1250	49.2126	49.2077	49.2158	49.2142		49.2168	49.2142		49.2169	49.2152		49.2178	49.2152	

SHAFT BEARING-SEAT DIAMETERS

Table 12 - Shaft Diameters and Resulting Fits

Units: inch

BEARI	NG BORE DIA	METER			SH	IAFT DIAMET	ER / RESULT	ING FIT (0.0001	l″)		
mm	i	n	Р	6	RESULTING	r	6	RESULTING	r	7	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT
4	0.1575	0.1572	0.1583	0.1580		0.1584	0.1581		0.1585	0.1581	
5	0.1969	0.1965	0.1976	0.1973	5 T / 11 T	0.1978	0.1974	6 T / 12 T	0.1979	0.1974	6 T / 14 T
6	0.2362	0.2359	0.2370	0.2367		0.2371	0.2368	, ,	0.2373	0.2368	,
7	0.2756	0.2753	0.2765	0.2762		0.2767	0.2763		0.2769	0.2763	
8	0.3150	0.3146	0.3159	0.3156		0.3161	0.3157		0.3163	0.3157	
9	0.3543	0.3540	0.3553	0.3549	6 T / 13 T	0.3554	0.3551	7 T / 14 T	0.3557	0.3551	7 T / 17 T
10	0.3937	0.3934	0.3946	0.3943		0.3948	0.3944		0.3950	0.3944	
12	0.4724	0.4721	0.4736	0.4731		0.4738	0.4733		0.4741	0.4733	
15	0.5906	0.5902	0.5917	0.5913	7 T / 15 T	0.5919	0.5915	9 T / 17 T	0.5922	0.5915	9 T / 19 T
17	0.6693	0.6690	0.6704	0.6700		0.6706	0.6702		0.6709	0.6702	
20	0.7874	0.7870	0.7888	0.7883		0.7890	0.7885		0.7893	0.7885	
25	0.9843	0.9839	0.9856	0.9851	9 T / 18 T	0.9859	0.9854	11 T / 20 T	0.9862	0.9854	11 T / 23 T
30	1.1811	1.1807	1.1825	1.1820		1.1827	1.1822		1.1830	1.1822	
35	1.3780	1.3775	1.3796	1.3790		1.3799	1.3793		1.3803	1.3793	
40	1.5748	1.5743	1.5765	1.5758	40 T (24 T	1.5768	1.5761	42 T (24 T	1.5771	1.5761	40 T (00 T
45	1.7717	1.7712	1.7733	1.7727	10 T / 21 T 13 T / 26 T	1.7736	1.7730	13 T / 24 T	1.7740	1.7730	13 T / 28 T
50	1.9685	1.9680	1.9702	1.9695		1.9705	1.9698		1.9708	1.9698	
55	2.1654	2.1648	2.1674	2.1666		2.1677	2.1670		2.1681	2.1670	
60	2.3622	2.3616	2.3642	2.3635		2.3646	2.3638		2.3650	2.3638	
65	2.5591	2.5585	2.5611	2.5603	10 T / 0/ T	2.5614	2.5607	14 T / 20 T	2.5619	2.5607	14 7 / 24 7
70	2.7559	2.7553	2.7579	2.7572	131/201	2.7583	2.7576	16 T / 30 T	2.7588	2.7576	16 T / 34 T
75	2.9528	2.9522	2.9548	2.9540		2.9552	2.9544		2.9556	2.9544	
80	3.1496	3.1490	3.1516	3.1509		3.1520	3.1513		3.1525	3.1513	
85	3.3465	3.3457	3.3488	3.3479		3.3493	3.3485		3.3498	3.3485	
90	3.5433	3.5425	3.5456	3.5448		3.5462	3.5453		3.5467	3.5453	
95	3.7402	3.7394	3.7425	3.7416		3.7430	3.7422		3.7435	3.7422	
100	3.9370	3.9362	3.9393	3.9385	15 T / 31 T	3.9399	3.9390	20 T / 37 T	3.9404	3.9390	20 T / 42 T
105	4.1339	4.1331	4.1362	4.1353		4.1369	4.1360		4.1374	4.1360	
110	4.3307	4.3299	4.3330	4.3322		4.3337	4.3328		4.3342	4.3328	
120	4.7244	4.7236	4.7267	4.7259		4.7274	4.7265		4.7279	4.7265	
130	5.1181	5.1171	5.1208	5.1198		5.1216	5.1206		5.1222	5.1206	
140	5.5118	5.5108	5.5145	5.5135		5.5153	5.5143		5.5159	5.5143	
150	5.9055	5.9045	5.9082	5.9072	17 T / 37 T	5.9091	5.9081	25 T / 44 T	5.9096	5.9081	25 T / 50 T
160	6.2992	6.2982	6.3019	6.3009	,	6.3028	6.3018	,	6.3033	6.3018	,
170	6.6929	6.6919	6.6956	6.6946		6.6966	6.6956		6.6972	6.6956	
180	7.0866	7.0856	7.0893	7.0883		7.0903	7.0893		7.0909	7.0893	
190	7.4803	7.4791	7.4834	7.4823		7.4845	7.4833		7.4852	7.4833	
200	7.8740	7.8728	7.8771	7.8760	20 T / 43 T	7.8782	7.8770	30 T / 54 T	7.8789	7.8770	30 T / 60 T
220	8.6614	8.6602	8.6645	8.6634		8.6657	8.6646		8.6664	8.6646	
240	9.4488	9.4476	9.4519	9.4508		9.4533	9.4521		9.4539	9.4521	
260	10.2362	10.2348	10.2397	10.2384		10.2412	10.2399		10.2420	10.2399	
280	11.0236	11.0222	11.0271	11.0258	22 T / 48 T	11.0286	11.0273	37 T / 63 T	11.0294	11.0273	37 T / 71 T
300	11.8110	11.8096	11.8145	11.8132		11.8161	11.8149		11.8169	11.8149	



BEARI	NG BORE DIA	METER			SH	IAFT DIAMET	'ER / RESULT	'ING FIT (0.0001	")		
mm	i	n	Р	6	RESULTING	r	6	RESULTING	r	7	RESULTING
Shaft	max	min	max	min	FIT	max	min	FIT	max	min	FIT
320	12.5984	12.5969	12.6023	12.6009		12.6041	12.6027		12.6049	12.6027	
340	13.3858	13.3843	13.3897	13.3883		13.3915	13.3901		13.3923	13.3901	
360	14.1732	14.1717	14.1771	14.1757	24 T / 54 T	14.1791	14.1777	43 T / 72 T	14.1800	14.1777	43 T / 81 T
380	14.9606	14.9591	14.9645	14.9631		14.9665	14.9651		14.9674	14.9651	
400	15.7480	15.7465	15.7519	15.7505		15.7539	15.7525		15.7548	15.7525	
420	16.5354	16.5337	16.5397	16.5381		16.5420	16.5404		16.5429	16.5404	
440	17.3228	17.3211	17.3271	17.3255		17.3294	17.3278		17.3303	17.3278	
460	18.1102	18.1085	18.1145	18.1129	27 T / 60 T	18.1170	18.1154	50 T / 83 T	18.1179	18.1154	50 T / 92 T
480	18.8976	18.8959	18.9019	18.9003		18.9044	18.9028		18.9053	18.9028	
500	19.6850	19.6833	19.6893	19.6877		19.6918	19.6902		19.6927	19.6902	
530	20.8661	20.8642	20.8709	20.8692		20.8738	20.8720		20.8748	20.8720	
560	22.0472	22.0453	22.0520	22.0503	21 T / (0 T	22.0549	22.0531	59 T / 96 T	22.0559	22.0531	FO T / 10/ T
600	23.6220	23.6201	23.6269	23.6251	31 T / 68 T	23.6299	23.6281	591/901	23.6309	23.6281	59 T / 106 T
630	24.8031	24.8012	24.8080	24.8062		24.8110	24.8093		24.8120	24.8093	
670	26.3780	26.3750	26.3834	26.3814		26.3868	26.3848		26.3880	26.3848	
710	27.9528	27.9498	27.9582	27.9562	35 T / 84 T	27.9616	27.9596	69 T / 118 T	27.9628	27.9596	69 T / 130 T
750	29.5276	29.5246	29.5330	29.5310	331/041	29.5368	29.5348	1 1 1 1 1 1 1 1 1	29.5380	29.5348	1001 / 1001
800	31.4961	31.4931	31.5015	31.4995		31.5053	31.5033		31.5065	31.5033	
850	33.4646	33.4606	33.4707	33.4685		33.4750	33.4728		33.4764	33.4728	
900	35.4331	35.4291	35.4392	35.4370	39 T / 101 T	35.4435	35.4413	83 T / 144 T	35.4449	35.4413	02 T / 1E7 T
950	37.4016	37.3976	37.4077	37.4055	571/1011	37.4124	37.4102	051/1441	37.4138	37.4102	83 T / 157 T
1000	39.3701	39.3661	39.3762	39.3740		39.3809	39.3787		39.3823	39.3787	
1060	41.7323	41.7274	41.7396	41.7370		41.7447	41.7421		41.7463	41.7421	
1120	44.0945	44.0896	44.1018	44.0992	47 T / 100 T	44.1069	44.1043	00 T / 174 T	44.1085	44.1043	00 T / 100 T
1180	46.4567	46.4518	46.4640	46.4614	47 T / 122 T	46.4695	46.4669	98 T / 174 T	46.4711	46.4669	98 T / 189 T
1250	49.2126	49.2077	49.2199	49.2173		49.2254	49.2228		49.2270	49.2228	

BEARING OUTSIDE DIAMETER HOUSING BORE / RESULTING FIT (0.0001") mm in F7 G6 G7 H6 RESULTING RESULTING RESULTING RESULTING FIT 17 L / 6 L 10 L / 2 L 13 L / 2 L 7 L / O T 0.6299 0.6296 0.6313 0.6306 0.6302 0.6309 0.6302 0.6304 0.6299 16 0.6306 19 0.7480 0.7477 0.7496 0.7488 0.7488 0.7483 0.7491 0.7483 0.7485 0.7480 22 0.8661 0.8658 0.8678 0.8669 0.8669 0.8664 0.8672 0.8664 0.8667 0.8661 24 0.9449 0.9445 0.9465 0.9457 0.9457 0.9452 0.9460 0.9452 0.9454 0.9449 9 L / O T 20 L / 8 L 11 L / 3 L 15 L / 3 L 26 1.0236 1.0233 1.0252 1.0244 1.0244 1.0239 1.0247 1.0239 1.0241 1.0236 28 1.1024 1.1020 1.1040 1.1031 1.1031 1.1026 1.1035 1.1026 1.1029 1.1024 30 1 1811 1 1807 1 1827 1 1819 1 1819 1 1814 1 1877 1 1814 1 1816 1 1811 32 1.2598 1.2594 1.2618 1.2608 1.2608 1.2602 1.2612 1.2602 1.2605 1.2598 35 1.3780 1.3775 1.3799 1.3789 1.3789 1.3783 1.3793 1.3783 1.3786 1.3780 37 1.4567 1.4563 1.4587 1.4577 1.4577 1.4570 1.4580 1.4570 1.4573 1.4567 24 L / 10 L 14 L / 4 L 18 L / 4 L 11 L / O T 40 1.5748 1.5744 1.5758 1.5758 1.5761 1.5752 1.5754 1.5748 1.5768 1.5752 42 1.6545 1.6549 1.6535 1.6531 1.6555 1.6545 1.6539 1.6539 1.6542 1.6535 47 1.8504 1.8500 1.8524 1.8514 1.8514 1.8507 1.8517 1.8507 1.8510 1.8504 52 2.0472 2.0467 2.0496 2.0484 2.0484 2.0476 2.0488 2.0476 2.0480 2.0472 55 2.1654 2.1648 2.1677 2.1665 2.1665 2.1657 2.1669 2.1657 2.1661 2.1654 62 2.4409 2.4404 2.4433 2.4421 2.4421 2.4413 2.4425 2.4413 2.4417 2.4409 68 2.6772 2.6767 2.6795 2.6783 29 L / 12 L 2.6783 2.6776 17 L / 4 L 2.6787 2.6776 21 L / 4 L 2.6779 2.6772 13 L / O T 72 2 8346 2 8341 2 8370 2 8358 2 8358 2 8350 2 8362 2 8350 2 8354 2 8346 75 2.9528 2.9522 2.9551 2.9539 2.9539 2.9531 2.9543 2.9531 2.9535 2.9528 80 3.1496 3.1491 3.1520 3.1508 3.1507 3.1500 3.1512 3.1500 3.1504 3.1496 85 3.3465 3.3459 3.3493 3.3479 3.3478 3.3469 3.3483 3.3469 3.3473 3.3465 90 3.5433 3.5427 3.5461 3.5447 3.5446 3.5438 3.5452 3.5438 3.5442 3.5433 95 3.7396 3.7430 3.7415 3.7420 3.7402 3.7416 3.7406 3.7406 3.7410 3.7402 100 3.9370 3.9364 3.9398 3.9384 34 L / 14 L 3.9383 3.9375 19 L / 5 L 3.9389 3.9375 24 L / 5 L 3.9379 3.9370 15 L / O T 4.3307 4.3301 110 4.3335 4.3321 4.3320 4.3312 4.3326 4.3312 4.3316 4.3307 115 4.5270 4.5304 4.5289 4.5294 4.5284 4.5276 4.5290 4.5280 4.5280 4.5276 120 4.7244 4.7238 4.7272 4.7258 4.7257 4.7249 4.7263 4.7249 4.7253 4.7244 125 4.9213 4.9206 4.9245 4.9230 4.9228 4.9218 4.9234 4.9218 4.9222 4 9213 5 1181 5 1174 5 1198 5 1202 5 1 1 9 1 130 5 1214 5 1196 5 1 1 8 7 5 1 1 8 7 5 1181 140 5.5118 5.5111 5.5151 5.5135 40 L / 17 L 5.5133 5.5124 22 L / 6 L 5.5139 5.5124 28 L / 6 L 5.5128 5.5118 17 L / O T 5.7087 5.7080 5.7119 5.7104 5.7102 5.7108 5.7092 145 5.7092 5.7096 5.7087 5.9088 5.9070 150 5 9055 5 9048 5 9072 5 9061 5 9076 5 9061 5 9065 5 9055 160 6.2992 6.2982 6.3025 6.3009 6.3007 6.2998 6.3013 6.2998 6.3002 6.2992 165 6.4961 6.4951 6.4993 6.4976 6.4966 6.4982 6.4970 6.4961 6.4978 6.4966 43 | / 17 | 31 L / 6 L 20 L / 0 T 25 L / 6 L 170 6.6929 6.6919 6.6962 6.6946 6.6944 6.6935 6.6950 6.6935 6.6939 6.6929 180 7.0866 7.0856 7.0899 7.0883 7.0881 7.0872 7.0887 7.0872 7.0876 7.0866 7.4803 7.4791 7.4820 7.4827 7.4815 7.4803 190 7.4841 7.4823 7.4809 7.4809 200 7.8740 7.8728 7.8778 7.8760 7.8757 7.8746 7.8764 7.8746 7.8752 7.8740 210 8.2677 8.2665 8.2715 8.2697 8.2694 8.2683 8.2701 8.2683 8.2689 8.2677 215 8 4646 8 4634 8 4683 8 4663 8 4652 8 4670 8 4652 8 4657 8 4646 8 4 6 6 5 220 8.6602 50 L / 20 L 29 L / 6 L 8.6638 36 L / 6 L 23 L / O T 8.6614 8.6652 8.6634 8.6631 8.6620 8.6620 8.6626 8.6614 225 8.8583 8.8571 8.8607 8.8620 8.8602 8.8600 8.8589 8.8589 8.8594 8.8583 230 9 0551 9.0539 9 0 5 7 1 9 05 75 9.0589 9 0 5 6 9 9 0 5 5 7 9 0 5 5 7 9.0563 9 0 5 5 1 240 9.4488 9.4476 9.4526 9.4508 9.4506 9.4494 9.4512 9.4494 9.4488 9.4500 250 9.8425 9.8413 9.8463 9.8445 9.8443 9.8431 9.8449 9.8431 9.8437 9.8425 260 10.2362 10.2348 10.2405 10.2384 10.2381 10.2369 10.2389 10.2369 10.2375 10.2362 56 L / 22 L 33 L / 7 L 41 L / 7 L 26 L / 0 T 270 10.6299 10.6285 10.6342 10.6321 10.6319 10.6306 10.6326 10.6306 10.6312 10.6299

Units: inch

Table 13 - Housing Bore Diameters and Resulting Fits



BEARIN	G OUTSIDE DI	IAMETER					HOUSI	NG BORE / RES	ULTING FIT (0.0001″)				
mm	i	n	F	7	RESULTING	G	6	RESULTING	G	7	RESULTING	н	6	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
280	11.0236	11.0222	11.0279	11.0258		11.0256	11.0243		11.0263	11.0243		11.0249	11.0236	
290	11.4173	11.4159	11.4216	11.4195		11.4193	11.4180		11.4200	11.4180		11.4186	11.4173	
300	11.8110	11.8096	11.8153	11.8132	56 L / 22 L	11.8130	11.8117	33 L / 7 L	11.8137	11.8117	41 L / 7 L	11.8123	11.8110	26 L / 0 T
310	12.2047	12.2033	12.2090	12.2069		12.2067	12.2054		12.2074	12.2054		12.2060	12.2047	
320	12.5984	12.5969	12.6031	12.6009		12.6006	12.5991		12.6014	12.5991		12.5998	12.5984	
340	13.3858	13.3843	13.3905	13.3883		13.3880	13.3865		13.3888	13.3865		13.3872	13.3858	
360	14.1732	14.1717	14.1779	14.1757		14.1754	14.1739		14.1762	14.1739		14.1746	14.1732	
370	14.5669	14.5654	14.5716	14.5694	63 L / 24 L	14.5691	14.5676	37 L / 7 L	14.5699	14.5676	45 L / 7 L	14.5683	14.5669	30 L / O T
380	14.9606	14.9591	14.9653	14.9631		14.9628	14.9613		14.9636	14.9613		14.9620	14.9606	
400	15.7480	15.7465	15.7527	15.7505		15.7502	15.7487		15.7510	15.7487		15.7494	15.7480	
420	16.5354	16.5337	16.5406	16.5381		16.5378	16.5362		16.5387	16.5362		16.5370	16.5354	
440	17.3228	17.3211	17.3280	17.3255		17.3252	17.3236		17.3261	17.3236		17.3244	17.3228	
460	18.1102	18.1085	18.1154	18.1129	69 L / 27 L	18.1126	18.1110	41 L / 8 L	18.1135	18.1110	50 L / 8 L	18.1118	18.1102	33 L / O T
480	18.8976	18.8959	18.9028	18.9003		18.9000	18.8984		18.9009	18.8984		18.8992	18.8976	
500	19.6850	19.6833	19.6902	19.6877		19.6874	19.6858		19.6883	19.6858		19.6866	19.6850	
520	20.4724	20.4705	20.4782	20.4754		20.4750	20.4733		20.4761	20.4733		20.4742	20.4724	
540	21.2598	21.2579	21.2656	21.2628		21.2624	21.2607		21.2635	21.2607		21.2616	21.2598	
560	22.0472	22.0453	22.0530	22.0502	771 (201	22.0498	22.0481	441.401	22.0509	22.0481	541 /01	22.0490	22.0472	271 (07
580	22.8346	22.8327	22.8404	22.8376	77 L / 30 L	22.8372	22.8355	46 L / 9 L	22.8383	22.8355	56 L / 9 L	22.8364	22.8346	37 L / O T
600	23.6220	23.6201	23.6278	23.6250		23.6246	23.6229		23.6257	23.6229		23.6238	23.6220	
620	24.4094	24.4075	24.4152	24.4124		24.4120	24.4103		24.4131	24.4103		24.4112	24.4094	
650	25.5906	25.5876	25.5969	25.5937		25.5935	25.5915		25.5946	25.5915		25.5925	25.5906	
670	26.3780	26.3750	26.3843	26.3811		26.3809	26.3789		26.3820	26.3789		26.3799	26.3780	
680	26.7717	26.7687	26.7780	26.7748		26.7746	26.7726		26.7757	26.7726		26.7736	26.7717	
700	27.5591	27.5561	27.5654	27.5622		27.5620	27.5600		27.5631	27.5600		27.5610	27.5591	
720	28.3465	28.3435	28.3528	28.3496	021/211	28.3494	28.3474	501 /01	28.3506	28.3474	701 / 01	28.3484	28.3465	40 L / 0 T
750	29.5276	29.5246	29.5339	29.5307	93 L / 31 L	29.5305	29.5285	59 L / 9 L	29.5317	29.5285	70 L / 9 L	29.5295	29.5276	49 L / O T
760	29.9213	29.9183	29.9276	29.9244		29.9242	29.9222		29.9254	29.9222		29.9232	29.9213	
780	30.7087	30.7057	30.7150	30.7118		30.7116	30.7096		30.7128	30.7096		30.7106	30.7087	
790	31.1024	31.0994	31.1087	31.1055		31.1053	31.1033		31.1065	31.1033		31.1043	31.1024	
800	31.4961	31.4931	31.5024	31.4992		31.4990	31.4970		31.5002	31.4970		31.4980	31.4961	
820	32.2835	32.2795	32.2904	32.2869		32.2867	32.2845		32.2880	32.2845		32.2857	32.2835	
830	32.6772	32.6732	32.6841	32.6806		32.6804	32.6782		32.6817	32.6782		32.6794	32.6772	
850	33.4646	33.4606	33.4715	33.4680		33.4678	33.4656		33.4691	33.4656		33.4668	33.4646	
870	34.2520	34.2480	34.2589	34.2554	109 L / 34 L	34.2552	34.2530	72 L / 10 L	34.2565	34.2530	85 L / 10 L	34.2542	34.2520	61 L / O T
920	36.2205	36.2165	36.2274	36.2239	107 17 541	36.2237	36.2215	12 17 10 1	36.2250	36.2215	0017101	36.2227	36.2205	0.2701
950	37.4016	37.3976	37.4085	37.4050		37.4048	37.4026		37.4061	37.4026		37.4038	37.4016	
980	38.5827	38.5787	38.5896	38.5861		38.5859	38.5837		38.5872	38.5837		38.5849	38.5827	
1000	39.3701	39.3661	39.3770	39.3735		39.3733	39.3711		39.3746	39.3711		39.3723	39.3701	
1150	45.2756	45.2707	45.2836	45.2794	129 L / 39 L	45.2793	45.2767	86 L / 11 L	45.2808	45.2767	102 L / 11 L	45.2782	45.2756	75 L / 0 T
1250	49.2126	49.2077	49.2206	49.2165		49.2163	49.2137	002/112	49.2178	49.2137		49.2152	49.2126	
1400	55.1181	55.1118	55.1274	55.1224	156 L / 43 L	55.1224	55.1193	106 L / 12 L	55.1242	55.1193	124 L / 12 L	55.1212	55.1181	94 L / O T
1600	62.9921	62.9858	63.0014	62.9965		62.9964	62.9933		62.9982	62.9933		62.9952	62.9921	,, 01
1800	70.8661	70.8583	70.8768	70.8709	185 L / 47 L	70.8710	70.8674	128 L / 13 L	70.8733	70.8674	150 L / 13 L	70.8698	70.8661	115 L / O T
2000	78.7402	78.7323	78.7508	78.7449		78.7450	78.7414		78.7473	78.7414		78.7438	78.7402	
2300	90.5512	90.5413	90.5632	90.5563	219 L / 51 L	90.5569	90.5525	155 L / 13 L	90.5594	90.5525	181 L / 13 L	90.5555	90.5512	142 L / O T
2500	98.4252	98.4154	98.4372	98.4303	2.7.27.511	98.4309	98.4265		98.4334	98.4265		98.4295	98.4252	122/01

Table 13 - Housing Bore Diameters and Resulting Fits

BEARIN	G OUTSIDE DI	AMETER					HOUSI	ING BORE / RES	ULTING FIT (0.0001″)				
mm	i	n	н	7	RESULTING	н	8	RESULTING	н	9	RESULTING	н	10	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
16	0.6299	0.6296	0.6306	0.6299	10 L / 0 T	0.6310	0.6299	14 L / O T	0.6316	0.6299	20 L / 0 T	0.6327	0.6299	31 L / O T
19	0.7480	0.7477	0.7489	0.7480	,	0.7493	0.7480	,	0.7501	0.7480	,	0.7513	0.7480	,
22	0.8661	0.8658	0.8670	0.8661		0.8674	0.8661		0.8682	0.8661		0.8694	0.8661	
24	0.9449	0.9445	0.9457	0.9449		0.9462	0.9449		0.9469	0.9449		0.9482	0.9449	
26	1.0236	1.0233	1.0244	1.0236	12 L / O T	1.0249	1.0236	17 L / O T	1.0257	1.0236	24 L / O T	1.0269	1.0236	37 L / O T
28	1.1024	1.1020	1.1032	1.1024		1.1037	1.1024		1.1044	1.1024		1.1057	1.1024	
30	1.1811	1.1807	1.1819	1.1811		1.1824	1.1811		1.1831	1.1811		1.1844	1.1811	
32	1.2598	1.2594	1.2608	1.2598		1.2614	1.2598		1.2623	1.2598		1.2638	1.2598	
35	1.3780	1.3775	1.3789	1.3780		1.3795	1.3780		1.3804	1.3780		1.3819	1.3780	
37	1.4567	1.4563	1.4577	1.4567		1.4582	1.4567		1.4591	1.4567		1.4606	1.4567	
40	1.5748	1.5744	1.5758	1.5748	14 L / O T	1.5763	1.5748	20 L / 0 T	1.5772	1.5748	29 L / O T	1.5787	1.5748	44 L / O T
42	1.6535	1.6531	1.6545	1.6535		1.6551	1.6535		1.6560	1.6535		1.6575	1.6535	
47	1.8504	1.8500	1.8514	1.8504		1.8519	1.8504		1.8528	1.8504		1.8543	1.8504	
52	2.0472	2.0467	2.0484	2.0472		2.0491	2.0472		2.0502	2.0472		2.0520	2.0472	
55	2.1654	2.1648	2.1665	2.1654		2.1672	2.1654		2.1683	2.1654		2.1701	2.1654	
62	2.4409	2.4404	2.4421	2.4409		2.4428	2.4409		2.4439	2.4409		2.4457	2.4409	
68	2.6772	2.6767	2.6783	2.6772	17 L / O T	2.6790	2.6772	23 L / 0 T	2.6801	2.6772	34 L / O T	2.6819	2.6772	52 L / O T
72	2.8346	2.8341	2.8358	2.8346		2.8365	2.8346	232701	2.8376	2.8346	512/01	2.8394	2.8346	52 27 01
75	2.9528	2.9522	2.9539	2.9528		2.9546	2.9528		2.9557	2.9528		2.9575	2.9528	
80	3.1496	3.1491	3.1508	3.1496		3.1514	3.1496		3.1525	3.1496		3.1543	3.1496	
85	3.3465	3.3459	3.3478	3.3465		3.3486	3.3465		3.3499	3.3465		3.3520	3.3465	
90	3.5433	3.5427	3.5447	3.5433		3.5454	3.5433		3.5467	3.5433		3.5488	3.5433	
95	3.7402	3.7396	3.7415	3.7402		3.7423	3.7402		3.7436	3.7402		3.7457	3.7402	
100	3.9370	3.9364	3.9384	3.9370	20 L / 0 T	3.9391	3.9370	27 L / 0 T	3.9404	3.9370	40 L / 0 T	3.9425	3.9370	61 L / O T
110	4.3307	4.3301	4.3321	4.3307	201/01	4.3328	4.3307	27 1 7 0 1	4.3341	4.3307	401/01	4.3362	4.3307	0112/01
115	4.5276	4.5270	4.5289	4.5276		4.5297	4.5276		4.5310	4.5276		4.5331	4.5276	
120	4.7244	4.7238	4.7258	4.7244		4.7265	4.7244		4.7278	4.7244		4.7299	4.7244	
125	4.9213	4.9206	4.9228	4.9213		4.9237	4.9213		4.9252	4.9213		4.9276	4.9213	
125	5.1181	5.1174	5.1197	5.1181		5.1206	5.1181		5.1220	5.1181		5.1244	5.1181	
140	5.5118	5.5111	5.5134	5.5118	23 L / O T	5.5143	5.5118	32 L / O T	5.5157	5.5118	46 L / O T	5.5181	5.5118	70 L / 0 T
140	5.7087	5.7080	5.7102	5.7087	231/01	5.7111	5.7087	JZ L / U I	5.7126	5.7087	40 L / 0 I	5.7150	5.7087	701701
145	5.9055	5.9048	5.7102	5.9055		5.9080	5.9055		5.7126	5.7087		5.7150	5.7087	
160	6.2992	6.2982	6.3008	6.2992		6.3017	6.2992		6.3031	6.2992		6.3055	6.2992	
	6.4961	6.4951	6.4976	6.4961		6.4985	6.4961		6.5000	6.4961		6.5024	6.4961	
165					26 L / 0 T			35 L / O T			49 L / O T			73 L / O T
170 180	6.6929 7.0866	6.6919 7.0856	6.6945 7.0882	6.6929 7.0866		6.6954 7.0891	6.6929 7.0866		6.6969 7.0906	6.6929 7.0866		6.6992 7.0929	6.6929 7.0866	
190	7.4803	7.4791	7.4821	7.4803		7.4831	7.4803		7.4848	7.4803		7.4876	7.4803	
200	7.8740	7.8728	7.8758	7.8740		7.8769	7.8740		7.8785	7.8740		7.8813	7.8740	
210	8.2677	8.2665	8.2695	8.2677		8.2706	8.2677		8.2722	8.2677		8.2750	8.2677	
215	8.4646	8.4634	8.4664	8.4646	201/07	8.4674	8.4646	40 L / 0 T	8.4691	8.4646	ET L / O T	8.4719	8.4646	REL (OT
220	8.6614	8.6602	8.6632	8.6614	30 L / O T	8.6643	8.6614	40 L / 0 T	8.6659	8.6614	57 L / O T	8.6687	8.6614	85 L / O T
225	8.8583	8.8571	8.8601	8.8583		8.8611	8.8583		8.8628	8.8583		8.8656	8.8583	
230	9.0551	9.0539	9.0569	9.0551		9.0580	9.0551		9.0596	9.0551		9.0624	9.0551	
240	9.4488	9.4476	9.4506	9.4488		9.4517	9.4488		9.4533	9.4488		9.4561	9.4488	
250	9.8425	9.8413	9.8443	9.8425		9.8454	9.8425		9.8470	9.8425		9.8498	9.8425	
260	10.2362	10.2348	10.2383	10.2362	34 L / O T	10.2394	10.2362	46 L / 0 T	10.2413	10.2362	65 L / 0 T	10.2445	10.2362	96 L / 0 T
270	10.6299	10.6285	10.6320	10.6299		10.6331	10.6299	,	10.6350	10.6299	· · · · · · · · · · · · · · · · · · ·	10.6382	10.6299	,

Units: inch

C41



BEARIN	G OUTSIDE D	IAMETER					HOUSI	NG BORE / RES	ULTING FIT (0.0001″)				
mm	i	n	н	17	RESULTING	н	18	RESULTING	н	9	RESULTING	H	10	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
280	11.0236	11.0222	11.0257	11.0236		11.0268	11.0236		11.0287	11.0236		11.0319	11.0236	
290	11.4173	11.4159	11.4194	11.4173		11.4205	11.4173		11.4224	11.4173		11.4256	11.4173	
300	11.8110	11.8096	11.8131	11.8110	34 L / O T	11.8142	11.8110	46 L / 0 T	11.8161	11.8110	65 L / O T	11.8193	11.8110	96 L / 0 T
310	12.2047	12.2033	12.2068	12.2047		12.2079	12.2047		12.2098	12.2047		12.2130	12.2047	
320	12.5984	12.5969	12.6007	12.5984		12.6019	12.5984		12.6039	12.5984		12.6075	12.5984	
340	13.3858	13.3843	13.3881	13.3858		13.3893	13.3858		13.3913	13.3858		13.3949	13.3858	
360	14.1732	14.1717	14.1755	14.1732		14.1767	14.1732		14.1787	14.1732		14.1823	14.1732	
370	14.5669	14.5654	14.5692	14.5669	38 L / O T	14.5704	14.5669	51 L / O T	14.5724	14.5669	71 L / O T	14.5760	14.5669	106 L / 0 T
380	14.9606	14.9591	14.9629	14.9606		14.9641	14.9606		14.9661	14.9606		14.9697	14.9606	
400	15.7480	15.7465	15.7503	15.7480		15.7515	15.7480		15.7535	15.7480		15.7571	15.7480	
420	16.5354	16.5337	16.5379	16.5354		16.5393	16.5354		16.5415	16.5354		16.5453	16.5354	
440	17.3228	17.3211	17.3253	17.3228		17.3267	17.3228		17.3289	17.3228		17.3327	17.3228	
460	18.1102	18.1085	18.1127	18.1102	43 L / O T	18.1141	18.1102	56 L / O T	18.1163	18.1102	79 L / O T	18.1201	18.1102	116 L / O T
480	18.8976	18.8959	18.9001	18.8976		18.9015	18.8976		18.9037	18.8976	,	18.9075	18.8976	
500	19.6850	19.6833	19.6875	19.6850		19.6889	19.6850		19.6911	19.6850		19.6949	19.6850	
520	20.4724	20.4705	20.4752	20.4724		20.4768	20.4724		20.4793	20.4724		20.4835	20.4724	
540	21.2598	21.2579	21.2626	21.2598		21.2642	21.2598		21.2667	21.2598		21.2709	21.2598	
560	22.0472	22.0453	22.0500	22.0472		22.0516	22.0472		22.0541	22.0472		22.0583	22.0472	
580	22.8346	22.8327	22.8374	22.8346	47 L / O T	22.8390	22.8346	63 L / O T	22.8415	22.8346	89 L / O T	22.8457	22.8346	130 L / 0 T
600	23.6220	23.6201	23.6248	23.6220		23.6264	23.6220		23.6289	23.6220		23.6331	23.6220	
620	24.4094	24.4075	24.4122	24.4094		24.4138	24.4094		24.4163	24.4094		24.4205	24.4094	
650	25.5906	25.5876	25.5937	25.5906		25.5955	25.5906		25.5984	25.5906		25.6031	25.5906	
670	26.3780	26.3750	26.3811	26.3780		26.3829	26.3780		26.3858	26.3780		26.3906	26.3780	
680	26.7717	26.7687	26.7748	26.7717		26.7766	26.7717		26.7795	26.7717		26.7843	26.7717	
700	27.5591	27.5561	27.5622	27.5591		27.5640	27.5591		27.5669	27.5591		27.5717	27.5591	
720	28.3465	28.3435	28.3496	28.3465		28.3514	28.3465		28.3543	28.3465		28.3591	28.3465	
750	29.5276	29.5246	29.5307	29.5276	61 L / O T	29.5325	29.5276	79 L / O T	29.5354	29.5276	108 L / 0 T	29.5402	29.5276	156 L / 0 T
760	29.9213	29.9183	29.9244	29.9213		29.9262	29.9213		29.9291	29.9213		29.9339	29.9213	
780	30.7087	30.7057	30.7118	30.7087		30.7136	30.7087		30.7165	30.7087		30.7213	30.7087	
790	31.1024	31.0994	31.1055	31.1024		31.1073	31.1024		31.1102	31.1024		31.1150	31.1024	
800	31.4961	31.4931	31.4992	31.4961		31.5010	31.4961		31.5039	31.4961		31.5087	31.4961	
820	32.2835	32.2795	32.2870	32.2835		32.2890	32.2835		32.2925	32.2835		32.2976	32.2835	
830	32.6772	32.6732	32.6807	32.6772		32.6827	32.6772		32.6862	32.6772		32.6913	32.6772	
850	33.4646	33.4606	33.4681	33.4646		33.4701	33.4646		33.4736	33.4646		33.4787	33.4646	
870	34.2520	34.2480	34.2555	34.2520		34.2575	34.2520		34.2610	34.2520		34.2661	34.2520	
920	36.2205	36.2165	36.2240	36.2205	75 L / O T	36.2260	36.2205	94 L / O T	36.2295	36.2205	130 L / 0 T	36.2346	36.2205	181 L / O T
950	37.4016	37.3976	37.4051	37.4016		37.4071	37.4016		37.4106	37.4016		37.4157	37.4016	
980	38.5827	38.5787	38.5862	38.5827		38.5882	38.5827		38.5917	38.5827		38.5969	38.5827	
1000	39.3701	39.3661	39.3736	39.3701		39.3756	39.3701		39.3791	39.3701		39.3843	39.3701	
1150	45.2756	45.2707	45.2797	45.2756		45.2821	45.2756		45.2858	45.2756		45.2921	45.2756	
1250	49.2126	49.2077	49.2167	49.2126	91 L / O T	49.2191	49.2126	114 L / O T	49.2228	49.2126	152 L / O T	49.2291	49.2126	215 L / O T
1400	55.1181	55.1118	55.1230	55.1181		55.1258	55.1181		55.1303	55.1181		55.1378	55.1181	
1600	62.9921	62.9858	62.9970	62.9921	112 L / O T	62.9998	62.9921	140 L / O T	63.0043	62.9921	185 L / O T	63.0118	62.9921	260 L / 0 T
1800	70.8661	70.8583	70.8720	70.8661		70.8752	70.8661		70.8807	70.8661		70.8898	70.8661	
2000	78.7402	78.7323	78.7461	78.7402	138 L / O T	78.7492	78.7402	169 L / O T	78.7547	78.7402	224 L / O T	78.7638	78.7402	315 L / O T
2300	90.5512	90.5413	90.5581	90.5512		90.5622	90.5512		90.5685	90.5512		90.5787	90.5512	
2500	98.4252	98.4154	98.4321	98.4252	167 L / O T	98.4362	98.4252	209 L / 0 T	98.4425	98.4252	272 L / O T	98.4528	98.4252	374 L / O T
2300	70.1LJL	20.1101	, J. I.J.L.I	,LJL		, J. 1302	, J. 1252		20.1123	, J. 12.52		20.1520	, , , , LJL	

BEARING OUTSIDE DIAMETER HOUSING BORE / RESULTING FIT (0.0001") mm in J6 J7 155 JS6 RESULTING RESULTING RESULTING RESULTING FIT 6 L / 2 T 7 L / 3 T 5 L / 2 T 5 L / 2 T 0.6299 0.6296 0.6302 0.6297 0.6303 0.6296 0.6301 0.6298 0.6301 0.6297 16 19 0.7480 0.7477 0.7483 0.7478 0.7485 0.7477 0.7482 0.7479 0.7483 0.7478 22 0.8661 0.8658 0.8665 0.8659 0.8666 0.8658 0.8663 0.8660 0.8664 0.8659 24 0.9449 0.9445 0.9452 0.9447 0.9454 0.9445 0.9451 0.9447 0.9451 0.9446 7 L / 2 T 8L/4T 5 L / 2 T 6L/3T 26 1.0236 1.0233 1.0239 1.0234 1.0241 1.0233 1.0238 1.0234 1.0239 1.0234 28 1.1024 1.1020 1.1027 1.1022 1.1028 1.1020 1.1025 1.1022 1.1026 1.1021 30 1 1811 1 1807 1 1814 1 1809 1 1816 1 1807 1 1813 1 1809 1 1814 1 1808 32 1.2598 1.2594 1.2602 1.2596 1.2604 1.2594 1.2601 1.2596 1.2602 1.2595 35 1.3780 1.3775 1.3783 1.3777 1.3785 1.3775 1.3782 1.3777 1.3783 1.3776 37 1.4567 1.4563 1.4571 1.4565 1.4572 1.4563 1.4569 1.4565 1.4570 1.4564 8 L / 2 T 10 L / 4 T 6 L / 2 T 7 L / 3 T 40 1.5748 1.5744 1.5752 1.5746 1.5754 1.5744 1.5750 1.5746 1.5751 1.5745 42 1.6541 1.6538 1.6535 1.6531 1.6539 1.6533 1.6531 1.6533 1.6539 1.6532 47 1.8504 1.8500 1.8508 1.8502 1.8509 1.8500 1.8506 1.8502 1.8507 1.8501 52 2.0472 2.0467 2.0478 2.0470 2.0480 2.0468 2.0475 2.0470 2.0476 2.0469 55 2.1649 2.1650 2.1654 2.1648 2.1659 2.1651 2.1661 2.1656 2.1651 2.1657 62 2.4409 2.4404 2.4415 2.4407 2.4417 2.4405 2.4412 2.4407 2.4413 2.4406 68 2.6772 2.6767 2.6777 2.6769 10 L / 2 T 2.6779 2.6767 12 L / 5 T 2.6774 2.6769 8 L / 3 T 2.6775 2.6768 9 L / 4 T 72 2 8346 2 8341 2 8352 2 8344 2 8354 2 8342 2 8349 2 8344 2 8350 2 8343 75 2.9528 2.9522 2.9533 2.9525 2.9535 2.9523 2.9530 2.9525 2.9531 2.9524 80 3.1496 3.1491 3.1501 3.1494 3.1503 3.1491 3.1499 3.1494 3.1500 3.1492 85 3.3465 3.3459 3.3471 3.3462 3.3473 3.3459 3.3468 3.3462 3.3469 3.3460 90 3.5433 3.5427 3.5439 3.5431 3.5442 3.5436 3.5430 3.5437 3.5428 3.5429 95 3.7396 3.7408 3.7410 3.7402 3.7399 3.7396 3.7405 3.7399 3.7406 3.7397 100 3.9370 3.9364 3.9376 3.9368 12 L / 2 T 3.9379 3.9365 15 L / 5 T 3.9373 3.9367 9 L / 3 T 3.9374 3.9366 10 L / 4 T 4.3307 4.3301 110 4.3313 4.3305 4.3316 4.3302 4.3310 4.3304 4.3311 4.3303 115 4.5270 4.5284 4.5270 4.5279 4.5271 4.5276 4.5282 4.5273 4.5273 4.5280 120 4.7244 4.7238 4.7250 4.7242 4.7253 4.7239 4.7247 4.7241 4.7248 4.7240 125 4.9213 4.9206 4.9220 4.9210 4.9223 4.9207 4.9216 4.9209 4.9218 4 9208 130 5 1181 5 1174 5 1191 5 1185 5 1 1 8 6 5 1188 5 1178 5 1176 5 1178 5 1176 140 5.5118 5.5111 5.5125 5.5115 14 L / 3 T 5.5128 5.5113 17 L / 6 T 5.5122 5.5115 11 L / 4 T 5.5123 5.5113 12 L / 5 T 5.7087 5.7080 5.7094 5.7090 5.7083 145 5.7084 5.7097 5.7081 5.7092 5.7082 150 5 9055 5 9048 5 9062 5 9052 5 9065 5 9050 5 9059 5 9052 5 9060 5 9050 160 6.2992 6.2982 6.2999 6.2989 6.3002 6.2987 6.2996 6.2989 6.2997 6.2987 165 6.4961 6.4951 6.4968 6.4958 6.4971 6.4955 6.4964 6.4957 6.4956 6.4966 17 L / 3 T 20 L / 6 T 13 L / 4 T 15 L / 5 T 170 6.6929 6.6919 6.6936 6.6926 6.6939 6.6924 6.6933 6.6926 6.6934 6.6924 180 7.0866 7.0856 7.0873 7.0863 7.0876 7.0861 7.0870 7.0863 7.0871 7.0861 7.4803 7.4791 7.4812 7.4815 7.4797 190 7.4800 7.4797 7.4807 7.4799 7.4809 200 7.8740 7.8728 7.8749 7.8737 7.8752 7.8734 7.8744 7.8736 7.8746 7.8734 210 8.2677 8.2665 8.2686 8.2674 8.2689 8.2671 8.2681 8.2673 8.2683 8.2671 215 8 4646 8 4634 8 4654 8 4 6 4 3 8 4657 8 4639 8 4650 8 4647 8 4651 8 4640 220 8.6602 20 L / 3 T 8.6608 24 L / 6 T 8.6618 16 L / 4 T 18 L / 6 T 8.6614 8.6623 8.6611 8.6626 8.6610 8.6620 8.6608 225 8.8583 8.8571 8.8591 8.8580 8.8594 8.8576 8.8587 8.8579 8.8588 8.8577 230 9 0551 9.0539 9 0 5 5 5 9.0560 9 0 5 4 8 9 0 5 6 3 9 0 5 4 5 9 0 5 4 7 9 0 5 5 7 9 0 5 4 5 240 9.4488 9.4476 9.4497 9.4485 9.4500 9.4482 9.4492 9.4484 9.4494 9.4482 250 9.8425 9.8413 9.8434 9.8422 9.8437 9.8419 9.8429 9.8421 9.8431 9.8419 260 10.2362 10.2348 10.2372 10.2359 10.2376 10.2356 10.2367 10.2358 10.2369 10.2356 24 L / 3 T 28 L / 6 T 18 L / 5 T 20 L / 6 T 270 10.6299 10.6285 10.6309 10.6296 10.6313 10.6293 10.6304 10.6295 10.6306 10.6293

Units: inch

Table 13 - Housing Bore Diameters and Resulting Fits



BEARIN	G OUTSIDE D	IAMETER					HOUSI	NG BORE / RES	SULTING FIT (0.0001″)				
mm	i	n	J	6	RESULTING	J	7	RESULTING	ور	5	RESULTING	ور	6	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
280	11.0236	11.0222	11.0246	11.0233		11.0250	11.0230		11.0241	11.0232		11.0243	11.0230	
290	11.4173	11.4159	11.4183	11.4170		11.4187	11.4167		11.4178	11.4169		11.4180	11.4167	
300	11.8110	11.8096	11.8120	11.8107	24 L / 3 T	11.8124	11.8104	28 L / 6 T	11.8115	11.8106	18 L / 5 T	11.8117	11.8104	20 L / 6 T
310	12.2047	12.2033	12.2057	12.2044		12.2061	12.2041		12.2052	12.2043		12.2054	12.2041	
320	12.5984	12.5969	12.5996	12.5981		12.6000	12.5977		12.5989	12.5979		12.5991	12.5977	
340	13.3858	13.3843	13.3870	13.3856		13.3874	13.3851		13.3863	13.3853		13.3865	13.3851	
360	14.1732	14.1717	14.1744	14.1730		14.1748	14.1725		14.1737	14.1727		14.1739	14.1725	
370	14.5669	14.5654	14.5681	14.5667	27 L / 3 T	14.5685	14.5662	31 L / 7 T	14.5674	14.5664	21 L / 5 T	14.5676	14.5662	23 L / 7 T
380	14.9606	14.9591	14.9618	14.9604		14.9622	14.9599		14.9611	14.9601		14.9613	14.9599	
400	15.7480	15.7465	15.7492	15.7478		15.7496	15.7473		15.7485	15.7475		15.7487	15.7473	
420	16.5354	16.5337	16.5367	16.5352		16.5371	16.5346		16.5360	16.5349		16.5362	16.5346	
440	17.3228	17.3211	17.3241	17.3226		17.3245	17.3220		17.3234	17.3223		17.3236	17.3220	
460	18.1102	18.1085	18.1115	18.1100	31 L / 3 T	18.1119	18.1094	35 L / 8 T	18.1108	18.1097	23 L / 5 T	18.1110	18.1094	26 L / 8 T
480	18.8976	18.8959	18.8989	18.8974		18.8993	18.8969		18.8982	18.8971		18.8984	18.8969	
500	19.6850	19.6833	19.6863	19.6848		19.6867	19.6843		19.6856	19.6845		19.6858	19.6843	
520	20.4724	20.4705							20.4730	20.4719		20.4733	20.4716	
540	21.2598	21.2579							21.2604	21.2593		21.2607	21.2590	
560	22.0472	22.0453							22.0478	22.0467		22.0481	22.0464	
580	22.8346	22.8327							22.8352	22.8341	25 L / 6 T	22.8355	22.8338	28 L / 9 T
600	23.6220	23.6201							23.6226	23.6215		23.6229	23.6212	
620	24.4094	24.4075							24.4100	24.4089		24.4103	24.4086	
650	25.5906	25.5876							25.5912	25.5899		25.5915	25.5896	
670	26.3780	26.3750							26.3786	26.3773		26.3789	26.3770	
680	26.7717	26.7687							26.7723	26.7710		26.7726	26.7707	
700	27.5591	27.5561							27.5597	27.5584		27.5600	27.5581	
720	28.3465	28.3435							28.3471	28.3458	241 / 47	28.3474	28.3455	201 / 10 T
750	29.5276	29.5246							29.5282	29.5269	36 L / 6 T	29.5285	29.5266	39 L / 10 T
760	29.9213	29.9183							29.9219	29.9206		29.9222	29.9203	
780	30.7087	30.7057							30.7093	30.7080		30.7096	30.7077	
790	31.1024	31.0994							31.1030	31.1017		31.1033	31.1014	
800	31.4961	31.4931							31.4967	31.4954		31.4970	31.4951	
820	32.2835	32.2795							32.2842	32.2828		32.2846	32.2824	
830	32.6772	32.6732							32.6779	32.6765		32.6783	32.6761	
850	33.4646	33.4606							33.4653	33.4639		33.4657	33.4635	
870	34.2520	34.2480							34.2527	34.2513	46 L / 7 T	34.2531	34.2509	50 L / 11 T
920	36.2205	36.2165							36.2212	36.2198	10 2 / 7 1	36.2216	36.2194	50 2 / 111
950	37.4016	37.3976							37.4023	37.4009		37.4027	37.4005	
980	38.5827	38.5787							38.5834	38.5820		38.5838	38.5816	
1000	39.3701	39.3661							39.3708	39.3694		39.3712	39.3690	
1150	45.2756	45.2707							45.2764	45.2748	57 L / 8 T	45.2769	45.2743	62 L / 13 T
1250	49.2126	49.2077							49.2134	49.2118	57 27 01	49.2139	49.2113	02 1 / 1 5 1
1400	55.1181	55.1118							55.1191	55.1171	73 L / 10 T	55.1196	55.1166	78 L / 15 T
1600	62.9921	62.9858							62.9931	62.9911	15 27 101	62.9937	62.9906	102/101
1800	70.8661	70.8583							70.8673	70.8650	91 L / 12 T	70.8680	70.8643	97 L / 18 T
2000	78.7402	78.7323							78.7413	78.7390	712/121	78.7420	78.7383	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
2300	90.5512	90.5413							90.5526	90.5498	112 L / 14 T	90.5533	90.5490	120 L / 22 T
2500	98.4252	98.4154							98.4266	98.4238		98.4274	98.4230	

BEARING OUTSIDE DIAMETER HOUSING BORE / RESULTING FIT (0.0001") mm in JS7 К5 K6 К7 RESULTING RESULTING RESULTING RESULTING FIT 7 L / 4 T 4 L / 2 T 4 L / 4 T 6 L / 5 T 0.6299 0.6296 0.6303 0.6296 0.6300 0.6297 0.6300 0.6296 0.6302 0.6294 16 19 0.7480 0.7477 0.7484 0.7476 0.7481 0.7477 0.7481 0.7476 0.7483 0.7474 22 0.8661 0.8658 0.8666 0.8657 0.8662 0.8658 0.8662 0.8657 0.8664 0.8656 24 0.9449 0.9445 0.9453 0.9445 0.9449 0.9446 0.9450 0.9444 0.9451 0.9443 8 L / 4 T 4 L / 4 T 4L/3T 6L/6T 26 1.0236 1.0233 1.0240 1.0232 1.0237 1.0233 1.0237 1.0232 1.0239 1.0230 28 1.1024 1.1020 1.1028 1.1019 1.1024 1.1020 1.1024 1.1019 1.1026 1.1018 30 1 1811 1 1807 1 1815 1 1807 1 1811 1 1808 1 1812 1 1807 1 1813 1 1805 32 1.2598 1.2594 1.2603 1.2594 1.2599 1.2595 1.2600 1.2593 1.2601 1.2591 35 1.3780 1.3775 1.3784 1.3775 1.3780 1.3776 1.3781 1.3774 1.3782 1.3772 37 1.4567 1.4563 1.4572 1.4562 1.4568 1.4563 1.4568 1.4562 1.4570 1.4560 9 L / 5 T 5 L / 4 T 6 L / 5 T 7 L / 7 T 40 1.5748 1.5744 1.5753 1.5743 1.5749 1.5744 1.5749 1.5743 1.5751 1.5741 42 1.6537 1.6535 1.6531 1.6540 1.6531 1.6536 1.6532 1.6530 1.6538 1.6528 47 1.8504 1.8500 1.8509 1.8499 1.8505 1.8500 1.8505 1.8499 1.8507 1.8497 52 2.0472 2.0467 2.0478 2.0467 2.0474 2.0469 2.0474 2.0467 2.0476 2.0464 55 2.1655 2.1655 2.1654 2.1648 2.1659 2.1648 2.1650 2.1648 2.1657 2.1645 2.4404 62 2.4409 2.4404 2.4415 2.4411 2.4406 2.4411 2.4404 2.4413 2.4401 68 2.6772 2.6767 2.6778 2.6766 11 L / 6 T 2.6773 2.6768 6 L / 4 T 2.6773 2.6766 7 L / 6 T 2.6775 2.6763 9L/8T 72 2 8346 2 8341 2 8352 2 8341 2 8348 2 8343 2 8348 2 8341 2 8350 2 8338 75 2.9528 2.9522 2.9533 2.9522 2.9529 2.9524 2.9529 2.9522 2.9531 2.9519 80 3.1496 3.1491 3.1502 3.1490 3.1497 3.1492 3.1498 3.1490 3.1500 3.1488 85 3.3465 3.3459 3.3471 3.3458 3.3465 3.3459 3.3466 3.3457 3.3469 3.3455 90 3.5433 3.5427 3.5440 3.5434 3.5428 3.5435 3.5426 3.5437 3.5426 3.5423 95 3.7396 3.7402 3.7394 3.7402 3.7408 3.7395 3.7396 3.7403 3.7406 3.7392 100 3.9370 3.9364 3.9377 3.9363 13 L / 7 T 3.9371 3.9365 7L/5T 3.9372 3.9363 7 L / 7 T 3.9374 3.9360 10 L / 10 T 4.3307 4.3301 4.3314 110 4.3300 4.3308 4.3302 4.3309 4.3300 4.3311 4.3297 115 4.5270 4.5282 4.5276 4.5270 4.5277 4.5276 4.5269 4.5269 4.5280 4.5266 120 4.7244 4.7238 4.7251 4.7237 4.7245 4.7239 4.7246 4.7237 4.7248 4.7234 125 4.9213 4.9206 4.9220 4.9205 4.9214 4.9207 4.9214 4.9204 4.9217 4 9202 130 5 1181 5 1174 5 1183 5 1 1 8 6 5 1170 5 1189 5 1173 5 1182 5 1175 5 1173 140 5.5118 5.5111 5.5126 5.5110 15 L / 8 T 5.5119 5.5112 8 L / 6 T 5.5120 5.5110 9 L / 8 T 5.5123 5.5107 12 L / 5 T 145 5.7087 5.7080 5.7094 5.7079 5.7088 5.7078 5.7088 5.7081 5.7091 5.7076 150 5 9055 5 9048 5.9063 5 9047 5 9056 5 9049 5 9057 5 9047 5 9060 5 9044 160 6.2992 6.2982 6.3000 6.2984 6.2993 6.2986 6.2994 6.2984 6.2997 6.2981 165 6.4961 6.4951 6.4969 6.4953 6.4962 6.4955 6.4962 6.4952 6.4950 6.4965 18 L / 8 T 11 L / 6 T 11 L / 8 T 15 L / 11 T 6.6934 170 6.6929 6.6919 6.6937 6.6921 6.6930 6.6923 6.6931 6.6921 6.6918 180 7.0866 7.0856 7.0874 7.0858 7.0867 7.0860 7.0868 7.0858 7.0871 7.0855 190 7.4803 7.4791 7.4812 7.4804 7.4805 7.4790 7.4794 7.4796 7.4794 7.4808 200 7.8740 7.8728 7.8749 7.8731 7.8741 7.8733 7.8742 7.8731 7.8745 7.8727 210 8.2677 8.2665 8.2686 8.2668 8.2678 8.2670 8.2679 8.2668 8.2682 8.2664 215 8 4646 8 4634 8 4655 8 4637 8 4646 8 4639 8 4648 8 4636 8 4651 8 4633 220 8.6602 8.6605 21 L / 9 T 8.6607 13 L / 7 T 14 L / 9 T 17 L / 13 T 8.6614 8.6623 8.6615 8.6616 8.6605 8.6619 8.6601 225 8.8583 8.8571 8.8592 8.8574 8.8583 8.8576 8.8585 8.8573 8.8588 8.8570 230 9 0551 9.0539 9 0 5 4 2 9 0 5 5 2 9.0553 9.0560 9 0 5 4 4 9 0 5 4 2 9 0 5 5 6 9.0538 240 9.4488 9.4476 9.4497 9.4479 9.4489 9.4481 9.4490 9.4479 9.4493 9.4475 250 9.8425 9.8413 9.8434 9.8416 9.8426 9.8418 9.8427 9.8416 9.8430 9.8412 260 10.2362 10.2348 10.2372 10.2352 10.2363 10.2354 10.2364 10.2352 10.2369 10.2348 24 L / 10 T 15 L / 8 T 16 L / 11 T 20 L / 14 T 270 10.6299 10.6285 10.6309 10.6289 10.6300 10.6291 10.6301 10.6289 10.6306 10.6285

Table 13 - Housing Bore Diameters and Resulting Fits

Units: inch



BEARIN	IG OUTSIDE D	IAMETER					HOUSI	NG BORE / RES	ULTING FIT (0.0001″)				
mm	i	n	JS	57	RESULTING	к	5	RESULTING	к	6	RESULTING	к	7	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
280	11.0236	11.0222	11.0246	11.0226		11.0237	11.0228		11.0238	11.0226		11.0243	11.0222	
290	11.4173	11.4159	11.4183	11.4163		11.4174	11.4165		11.4175	11.4163		11.4180	11.4159	
300	11.8110	11.8096	11.8120	11.8100	24 L / 10 T	11.8111	11.8102	15 L / 8 T	11.8112	11.8100	16 L / 11 T	11.8117	11.8096	20 L / 14 T
310	12.2047	12.2033	12.2057	12.2037		12.2048	12.2039		12.2049	12.2037		12.2054	12.2033	
320	12.5984	12.5969	12.5995	12.5973		12.5985	12.5976		12.5987	12.5973		12.5991	12.5969	
340	13.3858	13.3843	13.3869	13.3847		13.3859	13.3850		13.3861	13.3847		13.3865	13.3843	
360	14.1732	14.1717	14.1744	14.1721		14.1733	14.1724		14.1735	14.1721		14.1739	14.1717	
370	14.5669	14.5654	14.5681	14.5658	27 L / 11 T	14.5670	14.5661	17 L / 9 T	14.5672	14.5658	19 L / 11 T	14.5676	14.5654	22 L / 16 T
380	14.9606	14.9591	14.9618	14.9595		14.9607	14.9598		14.9609	14.9595		14.9613	14.9591	
400	15.7480	15.7465	15.7492	15.7469		15.7481	15.7472		15.7483	15.7469		15.7487	15.7465	
420	16.5354	16.5337	16.5367	16.5342		16.5355	16.5344		16.5357	16.5342		16.5361	16.5337	
440	17.3228	17.3211	17.3241	17.3216		17.3229	17.3219		17.3231	17.3216		17.3235	17.3211	
460	18.1102	18.1085	18.1115	18.1090	30 L / 12 T	18.1103	18.1093	19 L / 10 T	18.1106	18.1090	21 L / 13 T	18.1109	18.1085	25 L / 18 T
480	18.8976	18.8959	18.8989	18.8964	,	18.8977	18.8967		18.8980	18.8964	, -	18.8983	18.8959	- / -
500	19.6850	19.6833	19.6863	19.6838		19.6851	19.6841		19.6854	19.6838		19.6857	19.6833	
520	20.4724	20.4705	20.4738	20.4711					20.4724	20.4707		20.4724	20.4697	
540	21.2598	21.2579	21.2612	21.2585					21.2598	21.2581		21.2598	21.2571	
560	22.0472	22.0453	22.0486	22.0459					22.0472	22.0455		22.0472	22.0445	
580	22.8346	22.8327	22.8360	22.8333	33 L / 14 T				22.8346	22.8329	20 L / 17 T	22.8346	22.8319	20 L / 28 T
600	23.6220	23.6201	23.6234	23.6207					23.6220	23.6203		23.6220	23.6193	
620	24.4094	24.4075	24.4108	24.4081					24.4094	24.4077		24.4094	24.4067	
650	25.5906	25.5876	25.5921	25.5890					25.5906	25.5886		25.5906	25.5874	
670	26.3780	26.3750	26.3795	26.3764					26.3780	26.3760		26.3780	26.3748	
680	26.7717	26.7687	26.7732	26.7701					26.7717	26.7697		26.7717	26.7685	
700	27.5591	27.5561	27.5606	27.5575					27.5591	27.5571		27.5591	27.5559	
720	28.3465	28.3435	28.3480	28.3449					28.3465	28.3445		28.3465	28.3433	
750	29.5276	29.5246	29.5291	29.5260	45 L / 16 T				29.5276	29.5256	30 L / 20 T	29.5276	29.5244	30 L / 31 T
760	29.9213	29.9183	29.9228	29.9197					29.9213	29.9193		29.9213	29.9181	
780	30.7087	30.7057	30.7102	30.7071					30.7087	30.7067		30.7087	30.7055	
790	31.1024	31.0994	31.1039	31.1008					31.1024	31.1004		31.1024	31.0992	
800	31.4961	31.4931	31.4976	31.4945					31.4961	31.4941		31.4961	31.4929	
820	32.2835	32.2795	32.2852	32.2817					32.2835	32.2813		32.2835	32.2799	
830	32.6772	32.6732	32.6789	32.6754					32.6772	32.6750		32.6772	32.6736	
850	33.4646			33.4628					33.4646			33.4646		
870	34.2520	34.2480	34.2537	34.2502					34.2520	34.2498		34.2520	34.2484	
920	36.2205	36.2165	36.2222	36.2187	57 L / 18 T				36.2205	36.2183	39 L / 22 T	36.2205	36.2169	39 L / 35 T
950	37.4016	37.3976	37.4033	37.3998					37.4016	37.3994		37.4016	37.3980	
980	38.5827	38.5787	38.5844	38.5809					38.5827	38.5805		38.5827	38.5791	
1000	39.3701	39.3661	39.3719	39.3683					39.3701	39.3679		39.3701	39.3665	
1150	45.2756	45.2707	45.2777	45.2735					45.2756	45.2730		45.2756	45.2715	
1250	49.2126	49.2077	49.2147	49.2105	70 L / 21 T				49.2126	49.2100	49 L / 26 T	49.2126	49.2085	49 L / 41 T
1400	55.1181	55.1118	55.1206	55.1156					55.1181	55.1150		55.1181	55.1132	
1600	62.9921	62.9858	62.9946	62.9897	88 L / 25 T				62.9921	62.9891	63 L / 31 T	62.9921	62.9872	63 L / 49 T
1800	70.8661	70.8583	70.8691	70.8632					70.8661	70.8625		70.8661	70.8602	
2000	78.7402	78.7323	78.7431	78.7372	108 L / 30 T				78.7402	78.7365	79 L / 36 T	78.7402	78.7343	79 L / 59 T
2300	90.5512	90.5413	90.5546	90.5477					90.5512	90.5469		90.5512	90.5443	
2500	98.4252	98.4154	98.4286	98.4218	133 L / 34 T				98.4252	98.4209	98 L / 43 T	98.4252	98.4183	98 L / 69 T
2300	, J. 1232	20.1121	20.1200	20.1210					,	,0.1207		, J. 12.52	20.1105	

BEARING OUTSIDE DIAMETER HOUSING BORE / RESULTING FIT (0.0001") mm in М5 Μ6 Μ7 N5 RESULTING RESULTING RESULTING RESULTING FIT 2 L / 5 T 2 L / 6 T 0.6292 3 L / 7 T 0 T / 7 T 0.6299 0.6296 0.6298 0.6294 0.6298 0.6293 0.6299 0.6296 0.6293 16 19 0.7480 0.7477 0.7478 0.7475 0.7479 0.7474 0.7480 0.7472 0.7476 0.7472 22 0.8661 0.8658 0.8659 0.8656 0.8660 0.8655 0.8661 0.8653 0.8657 0.8653 24 0.9449 0.9445 0.9447 0.9443 0.9447 0.9442 0.9449 0.9441 0.9444 0.9441 2 L / 6 T 2L/7T4L/8T 1T/8T 26 1.0236 1.0233 1.0234 1.0231 1.0235 1.0230 1.0236 1.0228 1.0231 1.0228 28 1.1024 1.1020 1.1022 1.1018 1.1022 1.1017 1.1024 1.1015 1.1019 1.1015 30 1 1811 1 1807 1 1809 1 1806 1 1809 1 1804 1 1811 1 1803 1 1806 1 1803 32 1.2598 1.2594 1.2596 1.2592 1.2597 1.2591 1.2598 1.2589 1.2593 1.2589 35 1.3780 1.3775 1.3778 1.3773 1.3778 1.3772 1.3780 1.3770 1.3774 1.3770 37 1.4567 1.4563 1.4565 1.4561 1.4565 1.4559 1.4567 1.4557 1.4562 1.4557 2 L / 6 T 3 L / 8 T 4 L / 10 T 1 T / 9 T 40 1.5748 1.5744 1.5746 1.5742 1.5746 1.5740 1.5748 1.5738 1.5743 1.5739 42 1.6535 1.6535 1.6531 1.6533 1.6529 1.6534 1.6528 1.6526 1.6530 1.6526 47 1.8504 1.8500 1.8502 1.8498 1.8502 1.8496 1.8504 1.8494 1.8499 1.8494 52 2.0472 2.0467 2.0470 2.0465 2.0470 2.0463 2.0472 2.0461 2.0467 2.0461 55 2.1652 2.1654 2.1654 2.1648 2.1651 2.1646 2.1644 2.1642 2.1648 2.1643 62 2.4409 2.4404 2.4407 2.4402 2.4407 2.4400 2.4409 2.4398 2.4404 2.4398 68 2.6772 2.6767 2.6769 2.6764 3 L / 7 T 2.6770 2.6762 3L/9T 2.6772 2.6760 5 L / 12 T 2.6766 2.6761 1 T / 11 T 72 2 8346 2 8341 2 8344 2 8339 2 8344 2 8337 2 8346 2 8335 2 8341 2 8335 75 2.9528 2.9522 2.9525 2.9520 2.9526 2.9518 2.9528 2.9516 2.9522 2.9517 80 3.1496 3.1491 3.1494 3.1489 3.1494 3.1487 3.1496 3.1484 3.1490 3.1485 85 3.3465 3.3459 3.3461 3.3456 3.3462 3.3454 3.3465 3.3451 3.3457 3.3452 90 3.5433 3.5427 3.5430 3.5424 3.5431 3.5433 3.5419 3.5422 3.5426 3.5420 95 3.7396 3.7402 3.7398 3.7393 3.7399 3.7391 3.7402 3.7388 3.7394 3.7389 100 3.9370 3.9364 3.9367 3.9361 3L/9T 3.9368 3.9359 4 L / 11 T 3.9370 3.9356 6 L / 14 T 3.9363 3.9357 1 T / 13 T 4.3307 4.3301 4.3304 110 4.3298 4.3305 4.3296 4.3307 4.3293 4.3300 4.3294 115 4.5270 4.5273 4.5276 4.5276 4.5272 4.5267 4.5265 4.5262 4.5269 4.5263 120 4.7244 4.7238 4.7241 4.7235 4.7242 4.7233 4.7244 4.7230 4.7237 4.7231 125 4.9213 4.9206 4.9209 4.9202 4.9209 4.9200 4.9213 4 9 1 9 7 4.9204 4 9 1 9 7 130 5 1181 5 1174 5 1181 5 1173 5 1178 5 1170 5 1178 5 1168 5 1165 5 1166 140 5.5118 5.5111 5.5115 5.5107 4 L / 11 T 5.5115 5.5105 4 L / 13 T 5.5118 5.5102 7 L / 16 T 5.5110 5.5103 1 T / 15 T 5.7087 5.7080 5.7074 5.7087 5.7071 5.7071 145 5.7083 5.7076 5.7083 5.7078 150 5 9055 5 9048 5 9052 5 9044 5 9052 5 9042 5 9055 5 9039 5 9047 5 9040 160 6.2992 6.2982 6.2989 6.2981 6.2989 6.2979 6.2992 6.2976 6.2984 6.2977 165 6.4961 6.4951 6.4957 6.4950 6.4957 6.4948 6.4961 6.4945 6.4945 6.4952 7 L / 13 T 6 L / 11 T 10 L / 16 T 2 L / 15 T 170 6.6929 6.6919 6.6926 6.6919 6.6926 6.6916 6.6929 6.6913 6.6921 6.6914 180 7.0866 7.0856 7.0863 7.0856 7.0863 7.0853 7.0866 7.0850 7.0858 7.0851 7.4803 7.4791 7.4799 7.4800 7.4803 7.4793 7.4785 190 7.4791 7.4789 7.4785 200 7.8740 7.8728 7.8736 7.8728 7.8737 7.8726 7.8740 7.8722 7.8730 7.8722 210 8.2677 8.2665 8.2673 8.2665 8.2674 8.2663 8.2677 8.2659 8.2667 8.2659 215 8 4646 8 4634 8 4641 8 4633 8 4643 8 4631 8 4646 8 4636 8 4628 8 4628 220 8.6602 7 L / 12 T 8.6600 9 L / 15 T 8.6614 12 L / 18 T 2 L / 18 T 8.6614 8.6610 8.6602 8.6611 8.6596 8.6604 8.6596 225 8.8583 8.8571 8.8578 8.8570 8.8580 8.8568 8.8583 8.8565 8.8573 8.8565 230 9 0551 9.0539 9.0539 9 0 5 5 1 9 0 5 4 7 9 0548 9.0537 9.0533 9 0 5 4 1 9.0533 240 9.4488 9.4476 9.4484 9.4476 9.4485 9.4474 9.4488 9.4470 9.4478 9.4470 250 9.8425 9.8413 9.8421 9.8413 9.8422 9.8411 9.8425 9.8407 9.8415 9.8407 260 10.2362 10.2348 10.2357 10.2348 10.2359 10.2346 10.2362 10.2342 10.2352 10.2343 9 L / 14 T 10 L / 16 T 14 L / 20 T 3 L / 20 T 270 10.6299 10.6285 10.6294 10.6285 10.6296 10.6283 10.6299 10.6279 10.6289 10.6280

Units: inch

Table 13 - Housing Bore Diameters and Resulting Fits



BEARIN	IG OUTSIDE DI	IAMETER					HOUSI	NG BORE / RES	ULTING FIT (0.0001″)				
mm	i	n	м	15	RESULTING	N	16	RESULTING	N	17	RESULTING	N	5	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
280	11.0236	11.0222	11.0231	11.0222		11.0233	11.0220		11.0236	11.0216		11.0226	11.0217	
290	11.4173	11.4159	11.4168	11.4159		11.4170	11.4157		11.4173	11.4153		11.4163	11.4154	
300	11.8110	11.8096	11.8105	11.8096	9 L / 14 T	11.8107	11.8094	10 L / 16 T	11.8110	11.8090	14 L / 20 T	11.8100	11.8091	3 L / 20 T
310	12.2047	12.2033	12.2042	12.2033		12.2044	12.2031		12.2047	12.2027		12.2037	12.2028	
320	12.5984	12.5969	12.5979	12.5969		12.5980	12.5966		12.5984	12.5962		12.5972	12.5963	
340	13.3858	13.3843	13.3853	13.3843		13.3854	13.3840		13.3858	13.3836		13.3846	13.3837	
360	14.1732	14.1717	14.1727	14.1717		14.1728	14.1714		14.1732	14.1710		14.1720	14.1711	
370	14.5669	14.5654	14.5664	14.5654	10 L / 15 T	14.5665	14.5651	12 L / 18 T	14.5669	14.5647	16 L / 22 T	14.5657	14.5648	4 L / 22 T
380	14.9606	14.9591	14.9601	14.9591		14.9602	14.9588		14.9606	14.9584		14.9594	14.9585	
400	15.7480	15.7465	15.7475	15.7465		15.7476	15.7462		15.7480	15.7458		15.7469	15.7459	
420	16.5354	16.5337	16.5348	16.5337		16.5350	16.5335		16.5354	16.5330		16.5341	16.5331	
440	17.3228	17.3211	17.3222	17.3211		17.3224	17.3209		17.3228	17.3204		17.3215	17.3205	
460	18.1102	18.1085	18.1096	18.1085	11 L / 17 T	18.1098	18.1083	14 L / 20 T	18.1102	18.1078	18 L / 25 T	18.1089	18.1079	5 L / 24 T
480	18.8976	18.8959	18.8970	18.8959	·	18.8972	18.8957	, .	18.8976	18.8952	, .	18.8963	18.8953	- /
500	19.6850	19.6833	19.6844	19.6833		19.6846	19.6831		19.6850	19.6826		19.6837	19.6827	
520	20.4724	20.4705				20.4714	20.4697		20.4714	20.4687				
540	21.2598	21.2579				21.2588	21.2571		21.2588	21.2561				
560	22.0472	22.0453				22.0462	22.0445		22.0462	22.0435				
580	22.8346	22.8327				22.8336	22.8319	9 L / 28 T	22.8336	22.8309	9 L / 38 T			
600	23.6220	23.6201				23.6210	23.6193		23.6210	23.6183				
620	24.4094	24.4075				24.4084	24.4067		24.4084	24.4057				
650	25.5906	25.5876				25.5894	25.5874		25.5894	25.5862				
670	26.3780	26.3750				26.3768	26.3748		26.3768	26.3736				
680	26.7717	26.7687				26.7705	26.7685		26.7705	26.7673				
700	27.5591	27.5561				27.5579	27.5559		27.5579	27.5547				
720	28.3465	28.3435				28.3453	28.3433		28.3453	28.3421				
750	29.5276	29.5246				29.5264	29.5244	18 L / 31 T	29.5264	29.5232	18 L / 43 T			
760	29.9213	29.9183				29.9201	29.9181		29.9201	29.9169				
780	30.7087	30.7057				30.7075	30.7055		30.7075	30.7043				
790	31.1024	31.0994				31.1012	31.0992		31.1012	31.0980				
800	31.4961	31.4931				31.4949	31.4929		31.4949	31.4917				
820	32.2835	32.2795				32.2821	32.2799		32.2821	32.2786				
830	32.6772	32.6732				32.6758	32.6736		32.6758	32.6723				
850	33.4646	33.4606				33.4632	33.4610		33.4632	33.4597				
870	34.2520	34.2480				34.2506	34.2484		34.2506	34.2471				
920	36.2205	36.2165				36.2191	36.2169	26 L / 35 T	36.2191	36.2156	26 L / 49 T			
950	37.4016	37.3976				37.4002	37.3980		37.4002	37.3967				
980	38.5827	38.5787				38.5813	38.5791		38.5813	38.5778				
1000	39.3701	39.3661				39.3687	39.3665		39.3687	39.3652				
1150	45.2756	45.2707				45.2740	45.2714		45.2740	45.2699				
1250	49.2126	49.2077				49.2110	49.2084	33 L / 42 T	49.2110	49.2069	33 L / 57 T			
1400	55.1181	55.1118				55.1162	55.1131		55.1162	55.1113				
1600	62.9921	62.9858				62.9902	62.9872	44 L / 50 T	62.9902	62.9853	44 L / 68 T			
1800	70.8661	70.8583				70.8639	70.8602		70.8639	70.8580				
2000	78.7402	78.7323				78.7379	78.7343	56 L / 59 T	78.7379	78.7320	56 L / 82 T			
2300	90.5512	90.5413				90.5485	90.5442		90.5485	90.5416				
2500	98.4252	98.4154				98.4225	98.4182	72 L / 70 T	98.4225	98.4156	72 L / 96 T			
						-								

Table 13 - Housing Bore Diameters and Resulting Fits

BEARIN	G OUTSIDE D	IAMETER					HOUS	ING BORE / RES	SULTING FIT (0.0001″)				
mm	i	n	N	6	RESULTING	N	17	RESULTING	Р	6	RESULTING	Р	7	RESULTING
0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT
16	0.6299	0.6296	0.6296	0.6291	0T/8T	0.6297	0.6290	1L/9T	0.6293	0.6289	3 T / 10 T	0.6295	0.6288	1 T / 11 T
19	0.7480	0.7477	0.7476	0.7471	- , -	0.7478	0.7469		0.7473	0.7468	- / -	0.7475	0.7467	/
22	0.8661	0.8658	0.8657	0.8652		0.8659	0.8650		0.8654	0.8649		0.8656	0.8648	
24	0.9449	0.9445	0.9444	0.9439		0.9446	0.9438		0.9442	0.9437		0.9443	0.9435	
26	1.0236	1.0233	1.0232	1.0227	1 T / 9 T	1.0233	1.0225	1 L / 11 T	1.0229	1.0224	4 T / 12 T	1.0231	1.0222	2 T / 14 T
28	1.1024	1.1020	1.1019	1.1014		1.1021	1.1013		1.1017	1.1011		1.1018	1.1010	
30	1.1811	1.1807	1.1807	1.1802		1.1808	1.1800		1.1804	1.1799		1.1806	1.1797	
32	1.2598	1.2594	1.2594	1.2587		1.2595	1.2585		1.2590	1.2584		1.2592	1.2582	
35	1.3780	1.3775	1.3775	1.3769		1.3776	1.3767		1.3771	1.3765		1.3773	1.3763	
37	1.4567	1.4563	1.4562	1.4556		1.4564	1.4554		1.4559	1.4552		1.4560	1.4550	
40	1.5748	1.5744	1.5743	1.5737	0 T / 11 T	1.5745	1.5735	1 L / 13 T	1.5740	1.5733	4 T / 15 T	1.5741	1.5731	2 T / 17 T
42	1.6535	1.6531	1.6531	1.6524		1.6532	1.6522		1.6527	1.6521		1.6529	1.6519	
47	1.8504	1.8500	1.8499	1.8493		1.8501	1.8491		1.8496	1.8489		1.8497	1.8487	
52	2.0472	2.0467	2.0467	2.0459		2.0469	2.0457		2.0462	2.0455		2.0464	2.0452	
55	2.1654	2.1648	2.1648	2.1641		2.1650	2.1638		2.1643	2.1636		2.1645	2.1633	
62	2.4409	2.4404	2.4404	2.4396		2.4406	2.4394		2.4399	2.4392		2.4401	2.4389	
68	2.6772	2.6767	2.6766	2.6759	0 T / 13 T	2.6768	2.6756	2 L / 15 T	2.6761	2.6754	5 T / 18 T	2.6763	2.6752	3 T / 20 T
72	2.8346	2.8341	2.8341	2.8333		2.8343	2.8331	, ,	2.8336	2.8329		2.8338	2.8326	, ,
75	2.9528	2.9522	2.9522	2.9515		2.9524	2.9512		2.9517	2.9510		2.9519	2.9507	
80	3.1496	3.1491	3.1491	3.1483		3.1493	3.1481		3.1486	3.1478		3.1488	3.1476	
85	3.3465	3.3459	3.3458	3.3450		3.3461	3.3447		3.3453	3.3444		3.3455	3.3441	
90	3.5433	3.5427	3.5427	3.5418		3.5429	3.5415		3.5421	3.5413		3.5424	3.5410	
95	3.7402	3.7396	3.7395	3.7387		3.7398	3.7384		3.7390	3.7381		3.7392	3.7378	
100	3.9370	3.9364	3.9364	3.9355	0 T / 15 T	3.9366	3.9352	2 L / 18 T	3.9358	3.9350	6 T / 20 T	3.9361	3.9347	4 T / 23 T
110	4.3307	4.3301	4.3301	4.3292		4.3303	4.3289		4.3295	4.3287		4.3298	4.3284	
115	4.5276	4.5270	4.5269	4.5261		4.5272	4.5258		4.5264	4.5255		4.5266	4.5252	
120	4.7244	4.7238	4.7238	4.7229		4.7240	4.7226		4.7232	4.7224		4.7235	4.7221	
125	4.9213	4.9206	4.9205	4.9195		4.9208	4.9192		4.9198	4.9189		4.9202	4.9186	
130	5.1181	5.1174	5.1173	5.1163		5.1176	5.1161		5.1167	5.1157		5.1170	5.1154	
140	5.5118	5.5111	5.5110	5.5100	1 T / 18 T	5.5113	5.5098	2 L / 20 T	5.5104	5.5094	7 T / 24 T	5.5107	5.5091	4 T / 27 T
145	5.7087	5.7080	5.7079	5.7069		5.7082	5.7066		5.7072	5.7063		5.7076	5.7060	
150	5.9055	5.9048	5.9047	5.9037		5.9050	5.9035		5.9041	5.9031		5.9044	5.9028	
160	6.2992	6.2982	6.2984	6.2974		6.2987	6.2972		6.2978	6.2968		6.2981	6.2965	
165	6.4961	6.4951	6.4953	6.4943	21 / 42 7	6.4956	6.4940	EL (30 T	6.4946	6.4937	41.4247	6.4950	6.4934	1 T / 27 T
170	6.6929	6.6919	6.6921	6.6911	2 L / 18 T	6.6924	6.6909	5 L / 20 T	6.6915	6.6905	4 T / 24 T	6.6918	6.6902	1 T / 27 T
180	7.0866	7.0856	7.0858	7.0848		7.0861	7.0846		7.0852	7.0842		7.0855	7.0839	
190	7.4803	7.4791	7.4794	7.4783		7.4798	7.4780		7.4787	7.4776		7.4790	7.4772	
200	7.8740	7.8728	7.8731	7.8720		7.8735	7.8717		7.8724	7.8713		7.8727	7.8709	
210	8.2677	8.2665	8.2669	8.2657		8.2672	8.2654		8.2661	8.2650		8.2664	8.2646	
215	8.4646	8.4634	8.4637	8.4626		8.4640	8.4622		8.4630	8.4618		8.4633	8.4615	
220	8.6614	8.6602	8.6606	8.6594	3 L / 20 T	8.6609	8.6591	6 L / 24 T	8.6598	8.6587	4 T / 28 T	8.6601	8.6583	1 T / 31 T
225	8.8583	8.8571	8.8574	8.8563		8.8577	8.8559		8.8567	8.8555		8.8570	8.8552	
230	9.0551	9.0539	9.0543	9.0531		9.0546	9.0528		9.0535	9.0524		9.0538	9.0520	
240	9.4488	9.4476	9.4480	9.4468		9.4483	9.4465		9.4472	9.4461		9.4475	9.4457	
250	9.8425	9.8413	9.8417	9.8405		9.8420	9.8402		9.8409	9.8398		9.8412	9.8394	
260	10.2362	10.2348	10.2352	10.2340	41 / 22 T	10.2357	10.2336	01/267	10.2344	10.2331	ГТ / Э.4 Т	10.2348	10.2328	0 T / 35 T
270	10.6299	10.6285	10.6289	10.6277	4 L / 22 T	10.6294	10.6273	8 L / 26 T	10.6281	10.6268	5 T / 31 T	10.6285	10.6265	0 T / 35 T



obsmaxmaxmaxmaxmaxmaxmaxmaxmaxmaxmaxmaxmaxmaxmax10.0010.000 <td< th=""><th>BEARIN</th><th>g outside di</th><th>IAMETER</th><th></th><th></th><th></th><th></th><th>HOUS</th><th>NG BORE / RES</th><th>ULTING FIT (</th><th>0.0001″)</th><th></th><th></th><th></th><th></th></td<>	BEARIN	g outside di	IAMETER					HOUS	NG BORE / RES	ULTING FIT (0.0001″)					
0.0.naisn	mm	i	n	N	6		N	17		Р	6		Р	7	RESULTING	
300 11473 11474	0.D.	max	min	max	min	FIT	max	min	FIT	max	min	FIT	max	min	FIT	
300 11473 11474	280	11.0236	11.0222	11.0226	11.0214		11.0231	11.0210		11.0218	11.0205		11.0222	11.0202		
300 11810 11800		11.4173														
310 12.02 12.03						4 L / 22 T			8 L / 26 T			5 T / 31 T			0 T / 35 T	
320 12.98 12.590 12.597 12.590 12.596 12.596 12.596 12.596 12.596 12.596 12.596 12.596 12.596 12.596 12.596 12.596 12.596 13.380																
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370 14.569 14.569 14.564 14.564 14.564 14.563 14.564 <th></th> <td></td>																
380 14.966 14.999						6 L / 24 T			9 L / 29 T			4 T / 34 T			0 T / 39 T	
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480 18.876 18.895						7 / 26 T			11 / 31 T			4 T / 37 T			0 T / 43 T	
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60023.62023.62023.620323.61823.617223.617223.617223.617223.617224.0602						2 L / 35 T			2 L / 45 T			11 T / 48 T			11 T / 58 T	
620 24.409 24.407 25.871																
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780 30.7087 30.7067 30.7067 30.7067 30.707 30.7067 30.7087																
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95037.401637.397637.399437.397237.397437.397437.395837.397637.395437.395437.397637.395437.397637.395437.39763						17 L / 44 T			17 L / 57 T			0 T / 61 T			0 T / 75 T	
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1400 55.118 55.118 55.110 55.1120 55.110 55.1101 32 L / 81 7 55.110 55.1120 70.8594 70						23 L / 52 T			23 L / 67 T			2 L / 73 T			2 L / 89 T	
1600 62.9921 62.9858 62.9891 62.9801 62.9811 62.9811 62.9811 62.9811 62.9811 62.9816 62.9856 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 62.9866 62.9857 70.8594																
1800 70.8661 70.8583 70.8625 70.8589 $A_{1/727}$ 70.8625 70.8566 $A_{1/957}$ 70.8594 70.8558 $P_{1/1037}$ 70.8594 70.8						32 L / 61 T			32 L / 80 T			8 L / 86 T			8 L / 104 T	
2000 78.7402 78.7323 78.7365 78.7329 $4^{31} \lfloor 727 \\ 78.7365$ 78.7366 $4^{31} \lfloor 957 \\ 78.7365$ 78.7335 78.7378 $1^{21} \lfloor 703 \\ 78.7335$ 78.7335 78.7355 78.7376 $1^{21} \lfloor 726 \\ 78.7355$ <th +="" 126="" 78.73<="" \\="" th=""><th></th><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th>	<th></th> <td></td>															
2300 90.5512 90.5413 90.5469 90.5425 90.5475 90.5469 90.5469 90.5469 90.5400 90.5400 90.5435 90.5352 22 L / 120 T 90.5435 90.5366 22 L / 146						43 L / 72 T			43 L / 95 T			12 L / 103 T			12 L / 126 T	
55 L / 87 T 55 L / 112 T 22 L / 120 T 22 L / 146																
LJUV 20,4LJ4 20,4LJ4 20,4LJ4 20,4LUJ 20,4LUJ 20,4LUJ 20,4LUJ 20,4LUJ 20,4LUJ 20,4LJ4 2	2500	98.4252	98.4154	98.4209	98.4165	55 L / 87 T	98.4209	98.4140	55 L / 112 T	98.4175	98.4132	22 L / 120 T	98.4175	98.4106	22 L / 146 T	

TOLERANCE GRADES IT

Table 14 - Values of Normal Tolerance Grades IT

BASIC S	IZE (MM)	IT1	IT2	IT3	IT4	IT5	IT6	IT7	IT8	IT9
Over	incl					Tolerances (inch)			
	3	0.00003	0.00005	0.00008	0.00012	0.00016	0.00024	0.00039	0.00055	0.00098
3	6	0.00004	0.00006	0.00010	0.00016	0.00020	0.00032	0.00047	0.00071	0.00118
6	10	0.00004	0.00006	0.00010	0.00016	0.00024	0.00035	0.00059	0.00087	0.00142
10	18	0.00005	0.00008	0.00012	0.00020	0.00032	0.00043	0.00071	0.00106	0.00169
18	30	0.00006	0.00010	0.00016	0.00024	0.00035	0.00051	0.00083	0.00130	0.00205
30	50	0.00006	0.00010	0.00016	0.00028	0.00043	0.00063	0.00098	0.00154	0.00244
50	80	0.00008	0.00012	0.00020	0.00032	0.00051	0.00075	0.00118	0.00181	0.00291
80	120	0.00010	0.00016	0.00024	0.00039	0.00059	0.00087	0.00138	0.00213	0.00343
120	180	0.00014	0.00020	0.00032	0.00047	0.00071	0.00098	0.00158	0.00248	0.00394
180	250	0.00018	0.00028	0.00039	0.00055	0.00079	0.00114	0.00181	0.00284	0.00453
250	315	0.00024	0.00032	0.00047	0.00063	0.00091	0.00126	0.00205	0.00319	0.00512
315	400	0.00028	0.00035	0.00051	0.00071	0.00098	0.00142	0.00224	0.00350	0.00551
400	500	0.00032	0.00039	0.00059	0.00079	0.00106	0.00158	0.00248	0.00382	0.00610
500	630						0.00173	0.00276	0.00433	0.00689
630	800						0.00197	0.00315	0.00492	0.00787
800	1000						0.00221	0.00354	0.00551	0.00906
1000	1250						0.00260	0.00413	0.00650	0.01024
1250	1600						0.00307	0.00492	0.00768	0.01221
1600	2000						0.00362	0.00591	0.00906	0.01457
2000	2500						0.00433	0.00689	0.01102	0.01732
2500	3150						0.00532	0.00827	0.01299	0.02126



ZE (MM)	BASIC SI	IT18	IT17	IT16	IT15	IT14	IT13	IT12	IT11	IT10
incl	Over	Tolerances (inch)								
3		0.05512	0.03937	0.02362	0.01575	0.00984	0.00551	0.00394	0.00236	0.00158
6	3	0.07087	0.04724	0.02953	0.01890	0.01181	0.00709	0.00472	0.00295	0.00189
10	6	0.08661	0.05906	0.03543	0.02284	0.01417	0.00866	0.00591	0.00354	0.00228
18	10	0.10630	0.07087	0.04331	0.02756	0.01693	0.01063	0.00709	0.00433	0.00276
30	18	0.12992	0.08268	0.05118	0.03307	0.02047	0.01299	0.00827	0.00512	0.00331
50	30	0.15354	0.09843	0.06299	0.03937	0.02441	0.01535	0.00984	0.00630	0.00394
80	50	0.18110	0.11811	0.07480	0.04724	0.02913	0.01811	0.01181	0.00748	0.00472
120	80	0.21260	0.13780	0.08661	0.05512	0.03425	0.02126	0.01378	0.00866	0.00551
180	120	0.24803	0.15748	0.09843	0.06299	0.03937	0.02480	0.01575	0.00984	0.00630
250	180	0.28347	0.18110	0.11417	0.07284	0.04528	0.02835	0.01811	0.01142	0.00728
315	250	0.31890	0.20472	0.12598	0.08268	0.05118	0.03189	0.02047	0.01260	0.00827
400	315	0.35039	0.22441	0.14173	0.09055	0.05512	0.03504	0.02244	0.01417	0.00906
500	400	0.38189	0.24803	0.15748	0.09843	0.06102	0.03819	0.02480	0.01575	0.00984
630	500	0.43307	0.27559	0.17323	0.11024	0.06890	0.04331	0.02756	0.01732	0.01102
800	630	0.49213	0.31496	0.19685	0.12598	0.07874	0.04921	0.03150	0.01969	0.01260
1000	800	0.55118	0.35433	0.22047	0.14173	0.09055	0.05512	0.03543	0.02205	0.01417
1250	1000	0.64961	0.41339	0.25984	0.16535	0.10236	0.06496	0.04134	0.02598	0.01654
1600	1250	0.76772	0.49213	0.30709	0.19685	0.12205	0.07677	0.04921	0.03071	0.01969
2000	1600	0.90551	0.59055	0.36221	0.23622	0.14567	0.09055	0.05906	0.03622	0.02362
2500	2000	1.10236	0.68898	0.43307	0.27559	0.17323	0.11024	0.06890	0.04331	0.02756
3150	2500	1.29921	0.82677	0.53150	0.33858	0.21260	0.12992	0.08268	0.05315	0.03386





GENERAL INFORMATION	D3
SELECTING THE CORRECT LUBRICATION METHOD	
	D5
Properties	D5
Additives	D5
Consistency	D5
Oil Separation Rate	D5
Rust / Corrosion Protection	D7
Mixing Greases	D7
Grease Quantity	D7
Grease Replacement	D7
Replenishment Interval / Adjustments	D8
LUBRICATING OIL	D11
Properties	D11
Recommended Viscosities	D11
Comparative Viscosity Classifications	D11
Oil Temperature and Viscosity	D12
Selecting Lubricating Oils	D13
Methods of Oil Lubrication	D13
Oil Bath	D13
Drip Feed	D14
Splash	D14
Circulating System	D14
Jet	D15
Oil Mist	D15
Oil / Air	D16
Oil Replacement Intervals	D16
Mixing Oils	D16
MOLDED-OIL AND SOLID LUBE OPTIONS	D17

SECTION D:

LUBRICATION

Lubrication is essential to bearings to achieve the level of performance for which they were designed. Appropriate lubricant selection and methods employed will ensure reduced friction and wear inside the bearing, while allowing the bearing to perform optimally for the duration of its expected life. Primarily, lubrication serves the following purposes:

Reduction of Friction and Wear

Direct metallic contact between the bearing rings, rolling elements and cage is prevented by an oil film which reduces the friction and heat at the contact areas.

Extends Bearing Life

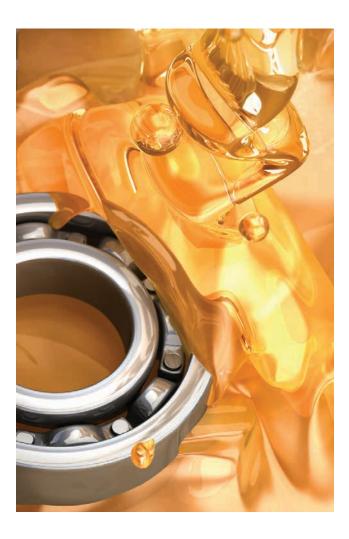
The rolling fatigue life of bearings depends in a large part on the viscosity and film thickness of the lubricant. A proper film thickness prolongs the bearing fatigue life.

Cooling

Circulating oil can be used to carry heat away from the bearing. A circulating system is normally used when excessive heat is generated by the bearing due to high speeds, high loads, or when heat from a source adjacent to the bearing can affect its operation. Oils deteriorate at high temperatures; therefore it is important to keep both the oil and the bearing cool.

Other Purposes

Proper lubrication also helps to prevent foreign material from entering the bearings, and protects against corrosion or rusting.





SELECTING THE CORRECT LUBRICATION METHOD

Lubrication can be accomplished by using either oil or grease. The most satisfactory bearing performance will be achieved by selecting the method most suitable for a specific application. This of course will also depend on the conditions under which the bearing will operate. Oil lubrication is superior in lubricating efficiency; however, grease lubrication allows a simpler structure around the bearings.

Table 1 illustrates the basic operating conditions tobe considered, and the relative suitability of oil andgrease lubrication.

Table 1 - Grease vs. Oil Lubrication

OPERATING FACTOR	GREASE LUBRICATION	OIL LUBRICATION	
Housing Structure and Sealing Method	Simple	May be complex. Careful maintenance required.	
Speed	Limiting speed is 65 % to 80% that of oil lubrication	High limiting speed	
Cooling Effect	Poor	Heat transfer is possible using forced oil circulation lubrication	
Fluidity	Poor	Good	
Full Lubrication Replacement	Sometimes difficult	Easy	
Removal of Foreign Matter	Impossible	Easy	
External Contamination Due to Leakage	Surroundings seldom contaminated by leakage	Often leaks without proper countermeasures. Not suitable if external contamination must be avoided.	

GREASE LUBRICATION

LUBRICATING GREASE

Grease is a semi-solid lubricant consisting of a base oil and a thickener. Other ingredients are sometimes added to impart special properties to the base. The main types and general properties of grease are shown in **Table 2**. It should be noted that different brands of the same type of grease may have different properties.

> Base Oil

Mineral oil or synthetic oils such as silicon or diester oil, are commonly used as the base oil for grease. The lubricating properties of grease are dependent on the characteristics of its base oil. The viscosity of the base oil is an important consideration when selecting grease. Usually grease made with a low viscosity base oil is more suitable for high speeds and low temperatures while grease made with high viscosity base oils is more suited for high temperatures and heavy loads. The thickener also influences the lubricating properties of grease, therefore selection criteria for grease are not the same as for lubricating oil.

Thickener

Several types of metallic soaps, inorganic compounds such as silica gel and bentonite, and heat resisting organic thickeners such as polyurea and flouric compounds are used as thickeners for grease. The water resistance properties of grease depend on the type of thickener. Sodium soap grease (or compound grease containing sodium soap) emulsifies when exposed to water or high humidity and therefore cannot be used where moisture is prevalent. Lithium soap grease, on the other hand, is recommended where moisture is present because of its resistance to wash off.

For applications where the operating temperature exceeds the limitation of common multi-purpose grease, greases having complex bases or non-soap bases are recommended. The grease used should also have a synthetic oil to withstand rapid deterioration at high temperatures. If the grease used in a high temperature application uses a mineral oil, it should be replenished frequently as deterioration of the oil will be accelerated at high temperatures.

ADDITIVES

Grease often contains a variety of additives such as antioxidants, corrosion inhibitors, and extreme pressure additives to give it special properties. Extreme pressure additives are recommended for use in heavy load applications. For long use without replenishment, an antioxidant should be added.

In heavy load or slow rotating applications, bearing life is a function of keeping the lubricant film thickness sufficient to separate the rolling elements from the raceway surface. In these cases lubricants with Extreme Pressure (EP) and Anti-Wear (AW) additives are used. As lubricant film thickness is also a function of temperature, careful consideration of the operating temperature is recommended to ensure use of the appropriate additive. AW additives are similar to EP additives in that their function is to prevent metal on metal contact by building up a protective layer on the surfaces. Some lubricants, intended for very low speed operation, include solid additives such as graphite or molybdenum disulphide (MoS2), and should be considered carefully as these particles may reduce bearing fatigue life.

CONSISTENCY

Consistency indicates the "softness" of the grease. **Table 3** shows the relationship between consistency and working conditions.

OIL SEPARATION RATE

During the normal operation of bearings with grease lubrication a small amount of oil is released. The rate at which this oil is released is referred to as the oil separation rate, or oil bleed rate. It is determined by testing, as described in JIS K2220 (5.7) or DIN 51817, and is expressed as a percentage. Typical oil separation rates fall in the range of 1% to 5%. Actual oil separation varies as it is a function of the base oil viscosity, the thickener type and amount, temperature, other additives and the processing.



Table 2 - Grease Properties

POPULAR NAME	Lithium Grease	Lithium Grease		Sodium Grease (Fiber Grease)	Calcium Grease (Cup Grease)	Mixed Base Grease	Complex Grease	Non-Soap Base	Grease
THICKENER	Li soap		Na soap	Ca soap	Na + Ca soap, Li + Ca soap, etc.	Ca complex, AI complex, etc.	Silica gel, bento black, polyurea compounds, hei organic compou	, flouric at resistant	
BASE OIL	Mineral Oil	Diester Oil	Silicone Oil	Mineral Oil	Mineral Oil	Mineral Oil	Mineral Oil	Mineral Oil	Synthetic Oil
Dropping Point (°C)	170 to 190	170 to 195	200 to 210	170 to 210	70 to 90	160 to 190	180 to 300	230	240 and above
Working Temp. (°C)	-20 to 110	-50 to 130	-50 to 160	-20 to 130	-20 to 60	-20 to 80	-20 to 130	-10 to 130	up to 250
Working Speed* (%)	70	100	60	70	40	70	70	70	40 to 100
Mechanical Stability	Good	Good	Good	Good	Poor	Good	Good	Good	Good
Pressure Resistance	Fair	Fair	Poor	Fair	Poor	Fair to Good	Fair to Good	Fair	Fair
Water Resistance	Good	Good	Good	Poor	Good	Poor for Na soap	Good	Good	Good
Rust Prevention	Good	Good	Poor	Poor to Good	Good	Fair to Good	Fair to Good	Fair to Good	Fair to Good
Comments	General purpose lubricant	Good low temperature and torque characteristics. Often used for small motor and instrument bearings.	Mainly for high temperature applications. Unsuitable for bearings under high speed or heavy load conditions or for sliding contact areas (roller bearings).	Long and short fiber types available. Long fiber grease is not suitable for high speeds or for sliding contact areas (roller bearings).	Not suitable for high temp. and heavy loads. Extreme pressure grease containing high viscosity oil and extreme pressure additive (Pb soap, etc.) is available.	Often used for roller bearings and large ball bearings.	Suitable for extreme pressures. Mechanically stable.	Medium and high temperature lubricant.	Recommended for special environments with very high and low temperatures, acids, alkalis, radioactivity, and exposure to flames.

Table 3 - Grease Consistency

	CONSISTENCY NUMBER (NLGI SCALE)					
	0	1	2	3	4	
Consistency (1/10 mm)	385 - 355	340 - 310	295 - 265	250 - 220	205 - 175	
Working Condition	For centralized oiling. When false brinelling is liable to occur.	For centralized oiling. When fretting is liable to occur. For low temperature.	For general use. For sealed bearings.	For high temperature. For general use. For sealed bearings.	For high temperature. For grease seals.	

Note: Consistency - depth into grease attained by a cone when pressed with a specified weight, indicated in units of 1/10 mm. The larger the value, the softer the grease.

GREASE LUBRICATION

RUST / CORROSIZON PROTECTION

Lithium complex, calcium complex and polyurea greases are typically considered to be good against wash out by water. No grease, however, is completely water resistant. The rate of ingress of water or wash out of the grease can be controlled somewhat by the grease fill amount, the relubrication interval, and the exposure to large volumes of water in the application.

MIXING GREASES

In general, grease of different types must not be mixed. Mixing grease with different types of thickeners may destroy the composition and physical properties of the grease. Even if the thickeners are of the same type, possible differences in the additives may cause detrimental effects.

GREASE QUANTITY

The quantity of grease to be packed in a housing depends on the housing design, grease characteristics, and ambient temperature. The bearings for the main spindle of machine tools - for example - where the accuracy may be impaired by a small temperature rise, require only a small amount of grease to reduce friction and heat.

Sufficient grease must be packed inside the bearing including on the cage guide surfaces. The amount of space inside the bearing and housing to be packed with grease depends upon the speed, as follows:

1/2 to 2/3 of the space - when the speed is less than 50% of the limiting speed

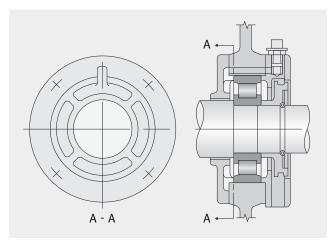
1/3 to 1/2 of the space - when the speed is more than 50% of the limiting speed

This is a general guideline for initial grease fill. It is important to carefully monitor bearing operating temperatures and adjust the grease fill accordingly. To determine the free space inside a specific bearing type contact your NSK application engineer.

GREASE REPLACEMENT

Typically, once a bearing and housing are properly packed with grease, replacement isn't necessary for an extended period. In applications with severe operating conditions, such as heavy loads, high speeds and/or elevated temperatures, grease should be replaced more frequently as grease deterioration is accelerated. In such cases, the bearing housing should be designed to facilitate grease replenishment and replacement. When replenishment intervals are short, provide replenishment and discharge ports at appropriate positions so deteriorated grease is replaced by fresh grease. For example, the housing space on the grease supply side can be divided into several sections with partitions. The grease on the partitioned side gradually passes through the bearings and old grease forced from the bearing is discharged through a grease valve (Figure 1). If a grease valve is not used, the space on the discharge side is made larger than the partitioned side so it can retain the old grease, which is removed periodically by removing the cover.

Fig. 1 – Combination of Partitioned Grease Reservoir and Grease Valve





REPLENISHMENT INTERVAL

Even if high-quality grease is used, there is deterioration of its properties with time; therefore, periodic replenishment is required. **Figure 2** and **Figure 3** show the replenishment time intervals (in hours) for various bearing types running at different speeds, and applies to bearings lubricated with highquality lithium soap-mineral oil grease, bearing temperature of 70°C (158°F) and normal load (P/C = 0.06 to 0.13).

REPLENISHMENT INTERVAL ADJUSTMENTS

For conditions other than those used to create **Figures 2** and **3**, adjustments may be made. Adjustments due to varied conditions can be compared to the results from **Figures 2** and **3**.

Bearing Load

For conditions where P/C varies from 10% of the dynamic load rating multiply the load factor from **Figure 4** by the result from **Figures 2** and **3**.

P = Applied Equivalent Bearing Load

C = Bearing Dynamic Load Rating

Where P/C exceeds 0.16 it is recommended that you consult with NSK engineering.

Fig. 4 - Load factor

P/C	≤ 0.06	0.10	0.13	0.16
Load Factor	1.50	1.00	0.65	0.45

Temperature

If the bearing temperature exceeds 70°C (158°F), the replenishment time interval must be reduced by half for every 15°C (27°F) bearing temperature increase.

Fig. 2 - Grease Replenishment Intervals for Radial Ball Bearings and Cylindrical Roller Bearings

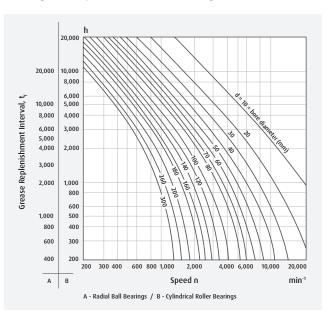
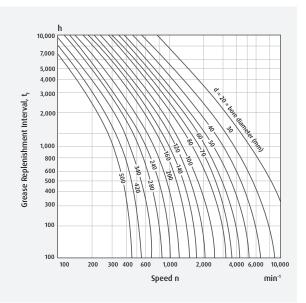


Fig. 3 - Grease Replenishment Intervals for Tapered Roller Bearings and Spherical Roller Bearings



GREASE LUBRICATION

REPLENISHMENT INTERVAL ADJUSTMENTS

Grease Type

In case of ball bearings especially, the replenishing interval can be extended depending on the grease type used. (For example, high-quality lithium soap synthetic oil grease may extend the replenishment time interval shown in **Figure 2** and **Figure 3** on **page D8** by two times.) The information provided is considered a general purpose guideline. Lubrication properties can vary significantly with a multitude of various operating conditions, of which, only a few are discussed in this document. It is advisable to consult with NSK engineering or lubrication manufacturer for questions about a particular grease life expectation.

High Speeds

Relubrication intervals for bearings used at high speeds or above the speed (n) in **Figures 2** and **3** should be carefully considered and consulted with NSK. In these cases continuous relubrication techniques, such as circulating oil, may be more suitable than grease lubrication.

Vibration

Moderate, typical vibration should not have a negative effect on grease life. However, high vibration and shock levels, such as those in vibrating screen applications, can cause the grease to "slump" more quickly, resulting in a churning effect. In these cases the relubrication interval should be reduced. If the grease excessively softens, a grease with a better mechanical stability or grease with higher stiffness (ex. NLGI 3) should be used. Vibration can also damage bearings during static conditions or in applications where there is minimal relative motion between the rings. In those cases certain greases can be selected to minimize this damage condition known as false brinelling.

Contamination

In highly contaminated environments, grease aging is usually not the primary concern, as compared to the contaminants on the bearing surfaces. Therefore, more frequent relubrication can reduce the negative effects of foreign particles on the grease while reducing the damaging effects caused by the particles. Fluid contaminants (water, process fluids, etc.) also call for a reduced interval. In case of severe contamination, continuous relubrication should be considered. There are no standard calculations to determine lubrication interval because of contamination. Therefore, experience is the best indicator of how often to relubricate. It is generally accepted that the more frequent the relubrication the better. However, care should be taken to avoid over greasing a bearing in an attempt to force out contaminated grease. Using less grease on a more frequent basis rather than the full amount of grease each time is recommended. Excessive regreasing without the ability to purge will cause higher operating temperatures because of churning.

Outer Ring Rotation

In applications where the outer ring rotates or where there is a rotating load, the speed factor should be based on the bearing outside diameter D instead of the dm. Also, the correct seals must be used to avoid grease loss due to purging (ex. use non-vented seals for ball bearings). For spherical roller thrust bearings with a rotating housing washer, oil lubrication is recommended.

Very Low Speeds

Bearings that operate at very low speeds (ex. Less than 20 rpm) and light loads require grease with low consistency. Bearings that operate at low speeds and heavy loads require a grease having a high viscosity, and if possible, good EP characteristics. Selecting the proper grease and grease fill is important in low speed applications. In some cases, 100% fills may be appropriate. In general, grease aging is not an issue for very low speed applications when bearing temperatures are less than 158°F (70°C). Therefore, relubrication is rarely required unless contamination occurs.



Vertical Shaft

An effective seal or retaining shield should be present below the bearing to prevent the grease from leaving the bearing cavity. Thicker consistency (ex. NLGI 3) greases may help reduce the amount of grease leakage. Consult with NSK for specific grease recommendations.

Very Heavy Loads

For bearings operating at a speed factor n x dm > 20,000 and with a load ratio C/P < 4, the relubrication interval should be reduced. Under these very heavy load conditions, continuous grease relubrication or oil bath lubrication is recommended. In applications where the speed factor n (inner ring rotational speed) x dm (bearing mean diameter) is < 20,000 and the load ratio C/P = 1-2, see information under **Very Low Speeds**. For heavy loads and high speeds, circulating oil lubrication (possibly with cooling and filtration) is generally recommended.

Very Light Loads

The relubrication period may be extended if the loads are light (C/P = 30 to 50).

Large-Size Bearings

For proper relubrication intervals for large roller bearings (d > 300 mm) a more iterative, hands-on procedure is recommended. In these cases it is advisable to relubricate possibly more frequently than needed by adhering to recommended calculated regreasing quantities. However, before regreasing, the appearance of the used grease and the degree of contamination due to particles and water should be documented. Additionally, the bearing component (seals, cages, etc.) should be checked for wear, damage and general operation. When the condition of the grease and associated components are found to be acceptable, the relubrication interval can be set.

Very Short Intervals

If the determined value for the relubrication interval is too short for a particular application, it is recommended to:

- > Check the bearing operating temperature.
- Check whether the grease is contaminated by solid particles or fluids.
- Check the bearing application conditions such as load or misalignment.
- > Consider more suitable greases. NSK can supply recommendations.

GREASE REPLENISHMENT

Frequent grease replenishment is required when operating conditions are severe such as in high ambient temperatures or where contaminants can enter bearing housings. Routine regreasing schedules should be established. In cases where extremely severe conditions exist or the bearings are in a remote area, the bearing housing should be designed to make replenishment and replacement as simple as possible. Automatic grease systems are available and should be used.

For normal operating conditions, it may be necessary to regrease the bearing periodically to replace any grease which has leaked from the housing and to eliminate any deteriorated grease.

For assistance with calculating appropriate grease replenishment intervals, visit NSK's NAVI-FOCUS portal at www.nskamericas.com

OIL LUBRICATION

LUBRICATING OIL

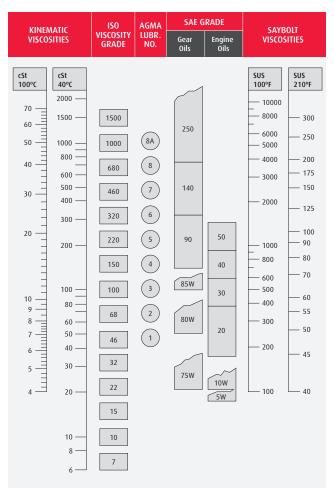
The lubricating oils used for rolling bearings are usually highly refined mineral oil or synthetic oil that have a high oil film strength and superior oxidation and corrosion resistance. When selecting a lubricating oil, the viscosity at the operating conditions is important. If the viscosity is too low, a proper oil film is not formed and abnormal wear and seizure may occur. On the other hand, if the viscosity is too high, excessive viscous resistance may cause heating or large power loss. In general, low viscosity oils should be used at high speed; however, the viscosity should increase with increasing bearing load and size.

Table 4 gives generally recommended viscosities for bearings under normal operating conditions. For use when selecting the proper lubricating oil, **Figure 6** shows the relationship between oil temperature and viscosity, and examples of selection based on load and speed are shown in **Table 5** on **page D13**. **Figure 5** shows the relationship between oil temperature and viscosity in ISO, AGMA and SAE classifications.

Table 4 - Recommended Oil Viscosity by Bearing Type

BEARING TYPES	PROPER VISCOSITY AT THE OPERATING TEMPERATURE
Ball Bearings and Cylindrical Roller Bearings	Higher than 13 cSt
Tapered Roller Bearings and Spherical Roller Bearings	Higher than 20 cSt
Spherical Roller Thrust Bearings	Higher than 32 cSt

Fig. 5 - Comparative Viscosity Classifications



NOTES

1) Viscosity can only be related horizontally

2) Viscosities based on 95 VI single grade oils.

3) ISO and AGMA viscosities are specified at 40°C. SAE 5W, 10W, 75W, 80W and 85W viscosities are specified at low temperature. Equivalent viscosities at 100°F and 210°F are shown.
4) SAE 90-250 (gear oils) and SAE 20-50 (engine oils) are specified at 210° F / 99°C.

For assistance with calculating kinematic viscosity at operating temperatures, visit NSK's NAVI-FOCUS portal at www.nskamericas.com



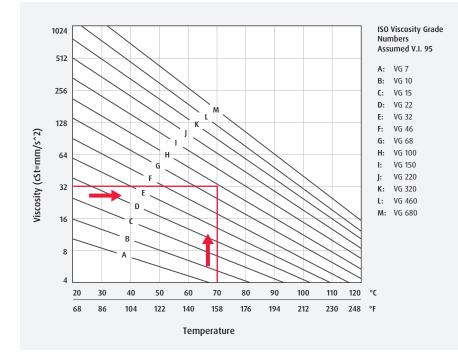


Fig. 6 - Oil Temperature and Viscosity

Figure 6 relates actual operating temperature to oil viscosity. To find an oil that satisfies the recommendation in (**Table 4**), draw a line upward at the operating temperature until it intersects a line that has the required viscosity. Then read the ISO VG grade according to the letter code on the line.

Fig. 7 - Estimate of Required Viscosity at Operating Speed

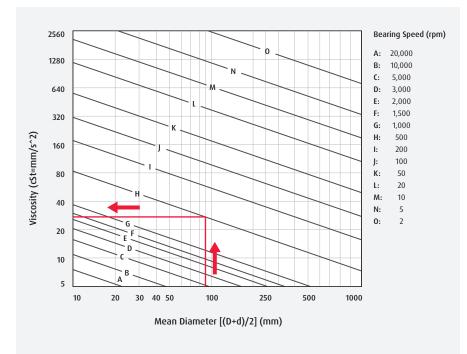


Figure 7 relates the bearing mean diameter ((D + d) / 2) to the estimated required viscosity at a given rotational speed. For example, a bearing with a pitch circle diameter of 90mm and rotating 500rpm, draw a line upward at 90 until it intersects line H (500rpm), then draw a line to the left to determine the viscosity of 30 cSt.

OIL LUBRICATION

Table 5 - Examples of Selecting Lubricating Oils

OPERATING TEMPERATURE	SPEED	LIGHT OR NORMAL LOAD	HEAVY OR SHOCK LOAD	
-30 to 0°C -22 to 32°F	$1 \text{ Less than limiting speed}$ 150 V_{0} 157737 (retrigerating machine oil)			
	< 50% of limiting speed	ISO VG 32, 46, 68 (bearing oil, turbine oil)	ISO VG 46, 68, 100 (bearing oil, turbine oil)	
0 to 50°C 32 to 122°F	50 to 100% of limiting speed	ISO VG 15, 22, 32 (bearing oil, turbine oil)	ISO VG 22, 32, 46 (bearing oil, turbine oil)	
	> limiting speed	ISO VG 10, 15, 22 (bearing oil)		
	< 50% of limiting speed	ISO VG 100, 150, 220 (bearing oil)	ISO VG 150, 220, 320 (bearing oil)	
50 to 80°C 122 to 176°F	50 to 100% of limiting speed	ISO VG 46, 68, 100 (bearing oil, turbine oil)	ISO VG 68, 100, 150 (bearing oil, turbine oil)	
	> limiting speed	ISO VG 32, 46, 68 (bearing oil, turbine oil)		
80 to 100°C 176 to 212°F	< 50% of limiting speed	ISO VG 320, 460 (bearing oil)	ISO VG 460, 680 (bearing oil, gear oil)	
	50 to 100% of limiting speed	ISO VG 150, 220 (bearing oil)	ISO VG 220, 320 (bearing oil)	
	> limiting speed	ISO VG 68, 100 (bearing oil, turbine oil)		

Note:

1) For the limiting speed, use the values listed in the bearing tables.

2) Refer to Refrigerating Machine Oils (JIS K 2211), Bearing Oils (JIS K 2239), Turbine Oils (JIS K 2213), and Gear Oils (JIS K 2219).

3) If the operating temperature is near the high end of the temperature range listed in the left column, select a high viscosity oil.

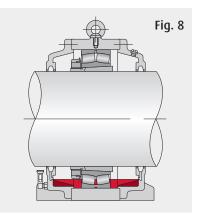
4) If the operating temperature is lower than -30°C or higher than 110°C, it is advisable to consult NSK.

METHODS OF OIL LUBRICATION

When the operating speed exceeds the grease limiting speed listed for the bearing, oil lubrication should be used. Oil features excellent flowability and heat dissipation capacity and is suitable for circulating and forced lubrication, two methods from which debris and abrasive particles are easily removed. It also has a positive effect on vibration and acoustic properties.

However, oil lubrication clearly adds complexity to the lubrication system and requires careful maintenance. Several methods are available and are described here. The best method to implement will depend on operating conditions.

Oil Bath Lubrication (Fig. 8) is a common method used where bearings are operating below the listed oil limiting speed. The static oil level should be set at the center of the lowest rolling element. An oil sight level gauge should be included in the system so that proper oil level can be quickly monitored.





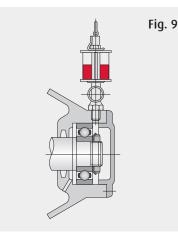
METHODS OF OIL LUBRICATION

Drip Feed Lubrication (Fig.9) is often used for small bearings operated at relatively high speeds. In the illustration, a visible oiler is used.

Splash Lubrication (Fig. 10) - In this lubricating method, oil is splashed onto the bearings by gears or by a simple rotating disc installed near bearings without submerging the bearings in oil. This method is commonly used in automobile transmissions, differentials and gear boxes. The illustration shows splash lubrication used on a reduction gear.

Circulating System Lubrication (Fig. 11)

is commonly used for high speed operation requiring cooling for the bearing, and for bearings used at high temperatures. Typically, oil from the supply pipe circulates through the bearings and exits to an external reservoir. After cooling in the reservoir it returns to the bearing through a pump and filter. In a circulating system, the oil outlet should be larger in diameter than the supply pipe so that an excessive amount of oil will not remain in the housing.



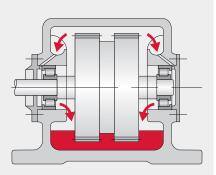
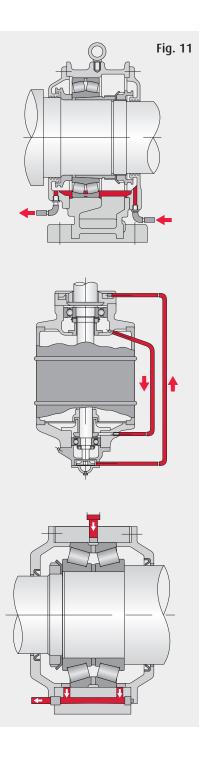


Fig. 10

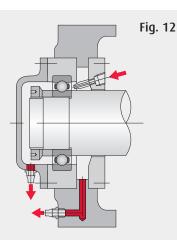


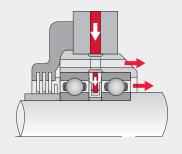
OIL LUBRICATION

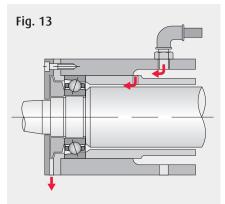
METHODS OF OIL LUBRICATION

Jet Lubrication (Fig. 12) - is often used for ultra-high speed bearings, with a dmn value (dm: pitch diameter of rolling element set in mm, n: rotational speed in rpm) exceeding one million. Lubrication oil is sprayed under pressure from one or more nozzles directly into the bearing. Figure 12 shows two examples of ordinary jet lubrication. The lubricating oil is sprayed on the inner ring and cage guide face. In the case of high speed operation, the air surrounding the bearing rotates with it causing the oil jet to be deflected. The jetting speed of the oil from the nozzle should be more than 20% of the circumferential speed of the inner ring outer surface.

More uniform cooling and a better temperature distribution are achieved using more nozzles for a given amount of oil. It is desirable for the oil to be forcibly discharged so the agitating resistance of the lubricant can be reduced and the oil can effectively carry away the heat.







Oil Mist Lubrication (Fig. 13) - also called oil fog lubrication, utilizes an oil mist sprayed into a bearing. This method has the following advantages: a) Because of the small quantity of oil required, the oil agitation resistance is small, and higher speeds are possible.

b) Contamination of the vicinity around the bearing is slight because the oil leakage is small.

c) It is relatively easy to continuously supply fresh oil; therefore, the bearing life is extended.

This lubricating method is used in bearings for the high speed spindles of machine tools, high speed pumps, roll necks of rolling mills, etc. For oil mist lubrication of large bearings, it is advisable to consult NSK.

Oil mist lubrication involves potential environmental hazards. Review OSHA requirements related to Oil Mist Systems.



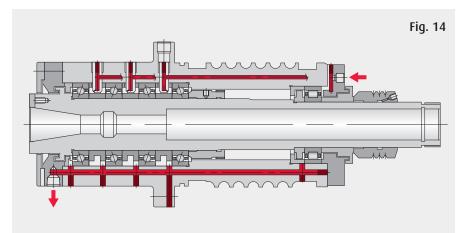
Oil / Air Lubrication (Fig. 14) - Using this method, a very small amount of oil is discharged intermittently by a constant-quantity piston into a pipe carrying a constant flow of compressed air. The oil flows along the wall of the pipe and approaches a constant flow. The major advantages of oil/air lubrication are: a) Since the minimum necessary amount of oil is supplied, this method is suitable for high speeds because less heat is generated.

b) Since the minimum necessary amount of oil is fed continuously, bearing temperature remains stable. Also, because of the small amount of oil, there is almost no atmospheric pollution.

c) Since only fresh oil is fed to the bearings, oil deterioration need not be considered.

d) Since compressed air is always fed to the bearings, the internal pressure is high, so dust, cutting fluid, etc. cannot enter.

For these reasons, this method is used in the main spindles of machine tools and other high-speed applications.



OIL REPLACEMENT INTERVALS

Oil replacement intervals depend on the operating conditions and oil quality. In those cases where the operating temperature is less than 50°C (122°F), and the environmental conditions are good with little dust, the oil should be replaced approximately once a year. However, in cases where the oil temperature is about 100°C (212°F), the oil must be changed at least once every three months. If moisture or foreign matter becomes mixed in the oil, then the oil replacement interval must be shortened.

MIXING OILS

Mixing different brands of oil must be prevented for the same reason given previously for grease.

MOLDED-OIL BEARINGS AND SOLID LUBE OPTIONS

NSK Molded-Oil bearings are uniquely designed to prevent the ingress of contamination that detrimentally impacts bearing performance, while providing a continuous and clean source of lubrication to the bearing. Oil-impregnated polyolefin resin serves as a barrier to water and dust, and slowly releases ample lubrication to the bearing with minimal risk of oil leakage.

FEATURES OF MOLDED-OIL BEARINGS

Excellent performance in water and dust contaminated environments

The bearings are designed to prevent liquids such as water (which can wash the lubricating oil out) and dust from getting inside the bearings. Sealed types can be used in environments exposed to water and dust.*

Environmentally friendly

Oil is released at the bearing surface only as needed, so little oil drips into the surrounding environment.

Low torque

The polymers in Molded-Oil do not interfere with the smooth rotation of rolling elements.

Optimal composition and molding methods enable highspeed operation of Molded-Oil Bearings

Optimization of composition and molding method of Molded-Oil improves strength and enables high-speed operation of Molded-Oil Bearings.

 * Water and dust dramatically accelerate bearing damage. In order to realize stable operation, NSK recommends using seals to prevent water and dust ingress.





Table 6 - Molded-Oil Bearing Types and Availability

BEARING TYPES	MOLDED-OIL TYPES	CAGE TYPES	LIMITING SPEEDS (d _m n)	SIZES (OUTSIDE DIAMETER, MM)
		Machined brass (CA)	< 60,000	70 to 250
Spherical roller bearings	For general use	Pressed steel (EA)	< 30,000	70 to 215
	For high-speed operation	Machined brass (CA)	60,000 to 100,000	70 to 215
	For general use	Pressed steel	< 150,000	19 to 250
Deep groove ball bearings	For high-speed operation	Pressed steel	150,000 to 200,000	19 to 215
Tapered roller bearings	For general use	Pressed steel	< 40,000	80 to 215

Note: $d_{mn} = [(Bearing bore diameter, mm + Bearing outside diameter, mm) ÷ 2] x inner ring rotational speed, min-1$

PRECAUTIONS FOR SELECTING

The following precautions should be considered to maintain the high performance of Molded-Oil Bearings:

- > For low-temperature applications to -10°F, Molded-Oil Bearings for general use are recommended.
- For the condition of high ambient temperature up to 250°F, Molded-Oil Bearings for high-speed operation are recommended.
- For proper operation, bearings must be under a radial load of at least 1% of the basic dynamic load rating to prevent skidding.
- Since Molded-Oil Bearings are lubricated by capillary action, the bearings cannot be used under the condition where the bearings are exposed to water directly for an extended period of time (the oil could be washed away). If the application requires such exposure, consider using extra seals.

SOLID LUBE OPTIONS

Augmenting our "available from stock" Molded-Oil bearings, NSK also offers an expanded range of Solid Lube formulations for a variety of application challenges including:

- extreme temperatures, with solutions for temperatures ranging from as low as -50°F to as high as 350°F
- heavy loads with low speeds, with high viscosity oil to accommodate heavily loaded roller bearings
- food grade solutions, including suitability for incidental food contact and food processing
- > high temperature wash down applications

These highly customized solutions can also be applied to a wider range of rolling bearing types including deep groove, angular contact and self-aligning ball bearings as well as spherical, cylindrical, tapered and thrust roller bearings.





SECTION E:

TROUBLESHOOTING / BEARING DAMAGE



BEARING HANDLING AND MAINTENANCE	E3
Mounting	E3
Check the Operation	E3
Maintenance	E3
Inspection Under Operating Conditions	
Inspection of the Bearing	E4
BEARING PERFORMANCE FACTORS	E5
Noise	E5
Vibration	E5
Temperature	E5
Effects of Proper Lubrication	E5
BEARING INSPECTION	E6
Evaluating the Bearing	E7
Running Traces and Applied Loads	E8
Ball Bearings	E8
Roller Bearings	E9
BEARING DAMAGE AND COUNTERMEASURES	E10
Flaking (or Spalling)	E11
Scoring	E13
Peeling	E15
Fracture	E16
Smearing	E17
Cracks	E19
Cage Damage	E21
Denting	E23
Pitting	E24
Wear	E25
Fretting	E26
False Brinelling	E27
Creep	E28
Seizure	E29
Electrical Erosion	E31
Rust and Corrosion	E33
Mounting Flaws	E34
Discoloration	E35
BEARING DAMAGE DIAGNOSTIC CHART	E36

BEARING HANDLING & MAINTENANCE

When a rolling bearing is damaged during machine operation, the entire machine or equipment may seize or malfunction. Since bearings that fail prematurely or unexpectedly cause unplanned downtime, it is important to be able to identify potential failures in order to avoid future risk.

Generally, bearing and/or application inspection can identify the cause of the problem. Often the cause is attributable to poor lubrication, improper handling, selecting the wrong bearing, or improper shaft or housing fits. Usually the cause can be determined by considering operation of the bearing before the failure, investigating the lubrication conditions and the mounting condition, and carefully observing the damaged bearing itself.

INSTALLATION PRACTICES

Careful consideration of bearing installation practices is important as it influences the bearing's running accuracy, life and performance. It is recommended that the mounting method includes the following considerations:

- > Clean the bearing and surrounding components
- > Check the dimensions and finish of related parts
- Carefully follow mounting procedure
- Verify the bearing is mounted correctly in the application
- Ensure the bearing is supplied with sufficient and correct lubrication

Since most bearings rotate with the shaft, the bearing mounting method is generally an interference (tight) fit for the inner ring and shaft while giving a clearance (loose) fit for the outer ring and housing.

CHECK THE OPERATION

After mounting the bearing, it is important to carry out an operating test to confirm that the bearing is mounted properly. **Table 1** indicates operating test methods. If irregularities are detected, immediately suspend the test and consult **Table 2** on **page E6** which lists appropriate countermeasures to specific bearing problems.

MAINTENANCE

It is necessary to periodically inspect and maintain the bearing and its operating conditions in order to maximize the bearing life. In general, the following method is adopted.





BEARING INSPECTION UNDER OPERATING CONDITIONS

To determine the appropriate bearing inspection interval and replenishment intervals for lubricant, investigate the lubricant properties and consider factors such as operating temperature, vibration, and bearing noise.

Be sure to inspect the bearing thoroughly during machine maintenance. If possible, check the raceway condition. Determine if damage exists. Confirm if the bearing can be reused or should be replaced.

Table 1 - Methods To Check Operation

MACHINE SIZE	OPERATING PROCEDURE	LIGHT OR NORMAL LOAD
Small machine	Manual operation. With the machine power off, rotate the bearing by hand. If no problems are detected, then proceed to operate the machine.	 Stick-slip (Debris, cracks, dents) Uneven rotating torque (Faulty mounting) Excessive torque (Error in mounting or insufficient radial internal clearance)
	Power operation. Initially start at a low speed and without a load. Gradually increase the speed and load until normal operating conditions are achieved.	Check for irregular noise. Check for bearing temperature rise, lubricant leakage, and/or discoloration.
Large machine	Idle operation. Turn ON power and allow machine to rotate slowly. Turn OFF the power and allow the bearing to coast to a stop. If no irregularities are detected by the test, then proceed to the loaded rotation testing.	Vibration, noise, etc.
Large machine	Power operation. Follow the same power operation testing as used for small machine testing.	Follow the same checkpoints as the small machine test.

BEARING PERFORMANCE FACTORS

Key bearing performance factors during operation are bearing noise, vibration, temperature, and lubricant condition. Please refer to Table 2 if any operation irregularities are detected.

BEARING NOISE

During operation, sound detection instruments (stethoscope, NSK Bearing Monitor, etc.) can be used to investigate the volume and characteristics of the bearing rotation noise. It is possible to distinguish bearing damage such as small flaking by means of its unusual yet characteristic noise.

BEARING VIBRATION

Bearing irregularities can be analyzed by measuring the vibrations of an operating machine. A frequency spectrum analyzer is used to measure the magnitude of vibration and the distribution of the frequencies. Analysis results can determine if the bearing is the source of the vibration, and can often determine defects in surrounding components. The measured data varies depending on the operating conditions of the bearing and the location of the vibration pick-up. Therefore, the method requires the determination of evaluation standards for each measured machine. It is useful to be able to detect irregularities from the bearing vibration pattern during operation.

BEARING TEMPERATURE

Generally, the bearing temperature can be estimated from the temperature of the housing outside surface, but a preferable way is to obtain direct measurements from the outer ring by a probe going through an oil hole. Usually, the bearing temperature gradually increases after the start of operation until reaching a steady state condition about 1 or 2 hours later. The bearing steady state temperature depends on load, rotational speed and heat transfer properties of the machine. Insufficient lubrication or improper mounting might cause the bearing temperature to rise rapidly. In such a case, suspend the machine operation and adopt an appropriate countermeasure.

EFFECTS OF PROPER LUBRICATION

The two main purposes of lubrication are to minimize friction and reduce wear inside bearings that might otherwise fail prematurely. Lubrication provides the following advantages:

Minimize Friction and Wear

Direct metallic contact between the bearing rings, rolling elements and cage, which are the basic components of a bearing, is prevented by an oil film which reduces the friction and wear in the contact areas.

> Extension of Fatigue Life

Properly selected lubrication viscosity and film thickness is essential to optimizing bearing fatigue life. A viscosity selection that is too light or excessively heavy can create operating conditions detrimental to bearing life.

> Dissipation of Frictional Heat and Cooling

Circulating lubrication may be used to carry away either frictional heat or heat transferred from the outside to prevent the bearing from overheating and the oil from deteriorating.

> Sealing and Rust Prevention

Adequate lubrication also helps to prevent foreign material from entering the bearings and guards against corrosion or rusting.



Table 2 - Causes And Countermeasures For Operating Irregularities

IRREGULARITIES		POSSIBLE CAUSES	COUNTERMEASURES							
		Abnormal load	Improve the fit, internal clearance, preload, position of housing shoulder, etc.							
Noise Lo Re	Loud Metallic	Incorrect mounting	Improve the machining accuracy and alignment of shaft and housing, accuracy of mounting method.							
	Sound	Insufficient or improper lubricant	Replenish the lubricant or select another lubricant.							
		Contact of rotating parts	Modify the labyrinth seal, etc.							
		Flaws, corrosion, or scratches on raceways	Replace or clean the bearing, improve the seals, and use clean lubricant.							
	Loud Regular Sound	Brinelling	Replace the bearing and use care when handling bearings.							
		Flaking on raceway	Replace the bearing.							
		Excessive clearance	Improve the fit, clearance and preload.							
	Irregular Sound	Penetration of foreign particles	Replace or clean the bearing, improve the seals, and use clean lubricant.							
		Flaws or flaking on balls	Replace the bearing.							
		Excessive amount of lubricant	Reduce amount of lubricant, select stiffer grease.							
		Insufficient or improper lubricant	Replenish lubricant or select a better one.							
Abnormal Temperature Rise	2	Abnormal load	Improve the fit, internal clearance, preload, position of housing shoulder.							
		Incorrect mounting	Improve the machining accuracy and alignment of shaft and housing, accuracy of mounting, or mounting method.							
		Creep on fitted surface, excessive seal friction	Correct the seals, replace the bearing, correct the fitting or mounting.							
Vibration (Axial runout)		Brinelling	Replace the bearing and use care when handling bearings.							
		Flaking	Replace the bearing.							
		Incorrect mounting	Correct the squareness between the shaft and housing shoulder or side of spacer.							
		Penetration of foreign particles	Replace or clean the bearing, improve the seals.							
Leakage or Discoloration of Lubricant		Too much lubricant; penetration by foreign matter or abrasion chips	Reduce the amount of lubricant, select a stiffer grease. Replace the bearing or lubricant. Clean the housing and adjacent parts.							

BEARING INSPECTION

When inspecting a bearing during periodic equipment inspections, operating inspections, or replacement of adjacent parts, determine the condition of the bearing and if its continued service is advisable.

A record should be kept of the inspection and external appearance of dismounted bearings. Take a grease or oil sample. Observe the lubricant appearance and volume, then the bearing can be cleaned and inspected. Once unmounted and cleaned, visual observations can be made of the rollers, rings, cage, and fitting surfaces for obvious signs of damage, elevated temperatures or other forms of distress. Refer to **Running Traces and Applied Loads (Page E8)** regarding the observation of running traces on the raceway surface.

When evaluating whether a bearing can be reused or not, the following points need to be considered: degree of bearing damage, machine performance, critical nature of the application, operating conditions, inspection interval. If the inspection reveals bearing damage or abnormalities, then try to confirm the cause and determine a countermeasure by referring to **Bearing Damage and Countermeasures (Page 10)** and then carry out the countermeasure.

If the inspection reveals any of the following evidence, the bearing should be replaced:

- > Excessive load
- > Misalignment
- Contamination (foreign debris)
- > Corrosion (water penetration)
- > Corrosion induced damage (pits, debris denting, spalling)
- > Incorrect shaft and/or housing fit
- > Excessive temperatures



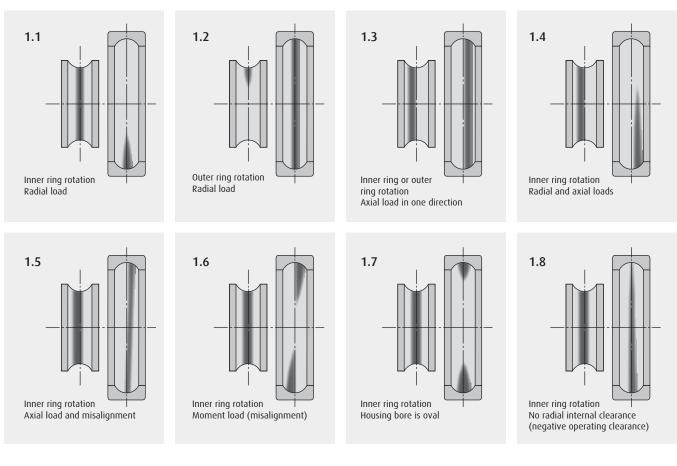


RUNNING TRACES AND APPLIED LOADS

As the bearing rotates, the raceways of the inner ring and the outer ring make contact with the rolling elements. This results in a wear path on both the rolling elements and raceways. It is normal for the running trace to be marked on the raceway. The size and the extent and shape of this running trace provides a useful indication of loading conditions. It is possible to determine from careful observation of the running traces whether the bearing is carrying a radial load, a large axial load, or a moment load, or if there are extreme rigidity variations of the housing. Unexpected loads applied to the bearing, excessive mounting error, or other operating issues can be determined, providing a clue to potential causes for bearing failure.

Representative running traces of deep groove ball bearings are shown in **Figure 1**. The **Figures 1.1** to **1.4**, show general running traces under radial load or axial load. The running traces vary according to whether the load is fixed to the inner ring or the outer ring, and according to load conditions. **Figure 1.5** shows running traces with a shaft inclined due to misalignment; **Figure 1.6** is a running trace under a moment load; **Figure 1.7** is a running trace in a housing which is elliptically shaped and has poor inner diameter accuracy; and **Figure 1.8** is a running trace in a bearing with insufficient internal clearance. Running traces in **Figures 1.5** to **1.8** often indicate specific causes of bearing failure and must be carefully observed.

Fig. 1 - Typical Running Traces Of Deep Groove Ball Bearings



BEARING INSPECTION

Fig. 2 - Typical Running Traces Of Roller Bearings

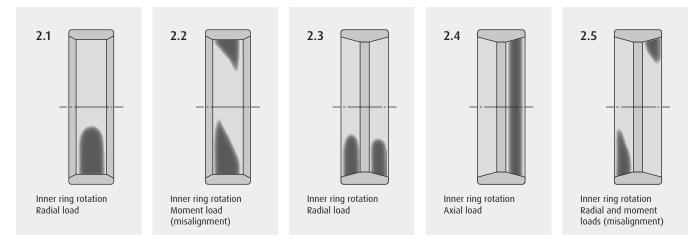


Figure 2 shows the running traces generated in roller bearings under various load conditions.

Figure 2.1 shows the outer ring running trace when a radial load is properly applied to a cylindrical roller bearing which has a load on a rotating inner ring.

Figure 2.2 shows the running trace in the case of shaft bending or relative inclination between the inner and outer rings. This misalignment leads to the generation of slightly shaded (dull) bands in the width direction. Traces are diagonal at the beginning and end of the loading zone.

For double-row tapered roller bearings where a single load is applied to the rotating inner ring. **Figure 2.3** shows the running trace on the outer ring under axial load while **Figure 2.4** shows the running trace on the outer ring under axial load.

When misalignment exists between the inner and the outer rings, then the application of a radial load causes running traces to appear on the outer ring as shown in **Figure 2.5**.

BEARING DAMAGE AND COUNTERMEASURES



In general, if rolling bearings are used correctly, they will survive to their predicted fatigue life. Bearings, however, often fail prematurely due to avoidable mistakes. In contrast to fatigue life, a premature failure is commonly caused by improper mounting, mishandling, poor lubrication, contamination or abnormal heat generation.

If all conditions are known for the times both before and after the failure, including the application, the operating conditions, and environment, then a countermeasure can be determined by studying the nature of the failure and its probable causes. A successful countermeasure will prevent reoccurrence of a similar failure. The following pages give examples of bearing damage and countermeasures. Please consult these sections when trying to determine the cause of bearing damage. The bearing diagnostic chart on page **E36** be useful as a quick reference quide.



BEARING DAMAGE AND COUNTERMEASURES FLAKING (OR SPALLING)

DAMAGE CONDITION

Flaking (sometimes referred to as spalling) occurs when small pieces of bearing material are split off from the smooth surface of the raceway or rolling elements due to rolling fatigue, thereby creating regions having a rough and coarse texture.

POSSIBLE CAUSE

- > Excessive load
- Poor mounting (misalignment)
- > Moment load
- > Entry of foreign debris, water penetration
- > Poor lubrication, Improper lubricant
- > Unsuitable bearing clearance
- Improper precision for shaft or housing, unevenness in housing rigidity, large shaft bending
- Progression from rust, corrosion pits, smearing, dents (Brinelling)

COUNTERMEASURE

- Reconfirm the bearing application & check the load conditions
- > Improve the mounting method
- Improve the sealing mechanism, prevent rusting during non-running
- > Use a lubricant with a proper viscosity, improve the lubrication method
- > Check the precision of shaft and housing
- > Check the bearing internal clearance



Part: Inner ring of an angular contact ball bearing

Observation: Flaking occurs diagonally along raceway

Cause: Poor alignment between shaft and housing during mounting

1.1



Part: Inner ring of deep groove ball bearing

Observation: Flaking of raceway at ball pitch

Cause: Dents due to shock load during mounting



Part: Inner ring of an angular contact ball bearing

Observation: Flaking of raceway at ball pitch

Cause: Dents due to shock load while stationary





Part: Outer ring of Photo 1.3

Observation: Flaking of raceway surface at ball pitch

Cause: Dents due to shock load while stationary



Part: Balls of Photo 1.3

Observation: Flaking of ball surface

Cause: Dents due to shock load while stationary



Part: Inner ring of a spherical roller bearing

Observation: Flaking of only one raceway over its entire circumference

Cause: Excessive axial load

1.4

1.7



1.6



Part: Outer ring of Photo 1.6

Observation: Flaking of only one raceway over its entire circumference

Cause: Excessive axial load



Part: Inner ring of a spherical roller bearing

Observation: Flaking of only one row of raceway

Cause: Poor lubrication



Part: Rollers of a cylindrical roller bearing

Observation: Premature flaking occurs axially on the rolling surfaces

Cause: Scratches caused during improper mounting

BEARING DAMAGE AND COUNTERMEASURES

DAMAGE CONDITION

Scoring is surface damage due to accumulated small seizures caused by sliding under improper lubrication or under severe operating conditions. Linear damage appears circumferentially on the raceway surface and rolling surface. Cycloidal shaped damage on the roller end. Scoring on rib surface contacting roller end.

POSSIBLE CAUSE

- > Excessive load, excessive preload
- > Poor lubrication
- > Particles are caught between surfaces with relative motion
- > Inclination of inner and outer rings
- Shaft bending
- > Poor precision of the shaft and housing

COUNTERMEASURE

- > Check the size of the load
- > Adjust the preload
- > Improve the lubricant and the lubrication method
- > Check the precision of the shaft and housing



Part: Inner ring of a spherical roller bearing

Observation: Scoring on large rib face of inner ring

Cause: Roller slipping due to sudden acceleration and deceleration

2.1



Part: Convex rollers of Photo 2.1

Observation: Scoring on roller end face

Cause: Roller slipping due to sudden acceleration and deceleration



Part: Inner ring of a tapered roller thrust bearing

Observation: Scoring on the face of inner ring rib

Cause: Worn particles become mixed with lubricant, and breakdown of oil film occurs due to excessive load





Part:

Rollers of a double-row cylindrical roller bearing

Observation:

Scoring on the roller end face

Cause: Poor lubrication and excessive axial load



Part: Inner ring of a spherical thrust roller bearing

Observation:

Scoring on the rib face of inner ring

Cause:

2.4

Debris, which is caught in surface, and excessive axial loading



Part: Convex rollers of Photo 2.5

Observation: Scoring on the roller end face

Cause: Debris, which is caught in surface, and excessive axial loading





Part: Cage of a deep groove ball bearing

Observation: Scoring on the pressed-steel cage pockets

Cause: Entry of debris

2.7

BEARING DAMAGE AND COUNTERMEASURES PEELING

DAMAGE CONDITION

Dull or cloudy spots appear on surface along with light wear. From such dull spots, tiny cracks are generated inward to a depth of 5 to 10 µm. Small particles fall off and minor flaking occurs widely.

POSSIBLE CAUSE

- > Unsuitable lubricant
- > Entry of debris into lubricant
- > Rough surface due to poor lubrication
- > Surface roughness of mating rolling part

COUNTERMEASURE

- > Select a proper lubricant
- > Improve the sealing mechanism
- > Improve the surface finish of the rolling mating parts



Part: Inner ring of a spherical roller bearing

Observation:

Round shaped peeling pattern occurs on the center of the raceway surface

Cause: Poor lubrication



Part: Convex rollers of Photo 3.1

Observation:

Round shaped peeling pattern occurs on the center of the rolling surfaces

Cause: Poor lubrication

3.1



Part: Outer ring of a spherical roller bearing

Observation:

Peeling occurs near the shoulder of the raceway over the entire circumference

Cause: Poor lubrication

BEARING DAMAGE AND COUNTERMEASURES



DAMAGE CONDITION

Fracture refers to small pieces which were broken off due to excessive load or shock load acting locally on a part of the roller corner or rib of a raceway ring.

POSSIBLE CAUSE

- Impact during mounting
- > Excessive load
- > Poor handling such as dropping

COUNTERMEASURE

- Improve the mounting method (Shrink fit, use of proper tools)
- > Reconsider the loading conditions
- > Provide enough back-up and support for the bearing rib



Part: Inner ring of a double-row cylindrical roller bearing

Observation: Chipping occurs at the center rib

Cause: Excessive load during mounting



Part: Inner ring of a tapered roller bearing

Observation: Fracture occurs at the cone back face rib surface

Cause: Large shock during mounting

4.1



Part: Inner ring of a spherical thrust roller bearing

Observation: Fracture occurs at the large rib

Cause: Repeated load

BEARING DAMAGE AND COUNTERMEASURES SMEARING

DAMAGE CONDITION

Smearing is surface damage which occurs from a collection of small seizures between bearing components caused by oil film rupture and/or sliding. Surface roughening occurs along with melting.

POSSIBLE CAUSE

- > High speed and light load
- > Sudden acceleration/deceleration
- > Improper lubricant
- > Entry of water

COUNTERMEASURE

- > Improve the preload
- > Improve the bearing clearance
- > Use a lubricant with good oil film formation ability
- > Improve the lubrication method
- > Improve the sealing mechanism



Part: Inner ring of a cylindrical roller bearing

Observation: Smearing occurs circumferentially on raceway surface

Cause:

Roller slipping due to excessive grease filling



Part: Outer ring of Photo 5.1

Observation:

5.1

Smearing occurs circumferentially on raceway surface

Cause: Roller slipping due to excessive grease filling



Part: Inner ring of a spherical roller bearing

Observation: Smearing occurs circumferentially on raceway surface

Cause: Poor lubrication





Part: Outer ring of Photo 5.3

Observation: Smearing occurs circumferentially on raceway surface

Cause: Poor lubrication



Part: Inner ring of a spherical roller bearing

Observation: Partial smearing occurs circumferentially on raceway surface

Cause: Poor lubrication



Part: Outer ring of Photo 5.5

Observation: Partial smearing occurs circumferentially on raceway surface

Cause: Poor lubrication

5.5



Part: Convex rollers of Photo 5.5

Observation: Smearing occurs at the center of the rolling surface

Cause: Poor lubrication

5.7

5.4

BEARING DAMAGE AND COUNTERMEASURES CRACKS

DAMAGE CONDITION

Cracks in the raceway ring and rolling elements. Continued use under this condition leads to larger cracks or fractures.

POSSIBLE CAUSE

- > Excessive interference
- > Excessive load, shock load
- > Progression of flaking
- Heat generation and fretting caused by contact between mounting parts and raceway ring
- > Heat generation due to creep
- > Poor taper angle of tapered shaft
- Poor cylindricality of shaft
- > Interference with bearing chamfer due to a large shaft

COUNTERMEASURE

- > Correct the interference
- > Check the load conditions
- > Improve the mounting method
- > Use an appropriate shaft shape



Part: Outer ring of a double-row cylindrical roller bearing

Observation:

Thermal cracks occur on the outer ring side face

Cause:

Abnormal heat generation due to contact sliding between mating part and face of outer ring



Part: Roller of a tapered roller thrust bearing

Observation:

Thermal cracks occur at large end face of roller

Cause:

6.1

Heat generation due to sliding with the inner ring rib under poor lubrication



Part: Outer ring of a double-row cylindrical roller bearing

Observation:

Cracks propagated outward in the axial and circumferential directions from the flaking origin on the raceway surface

Cause: Flaking from a flaw due to shock





Part:

Outer ring of a double-row cylindrical roller bearing used for outer ring rolling (outer ring rotation)

Observation:

Cracks occur on outside surface

Cause:

Flat wear and heat generation due to non-rotation of the outer ring



Part: Raceway surface of outer ring in Photo 6.4

Observation: Outside surface crack developing on the raceway



Part: Inner ring of a spherical roller bearing

Observation: Axial cracks occur on raceway surface

Cause:

Large fitting stress due to temperature difference between shaft and inner ring

6.4

6.7

Part: Cross section of a fractured inner ring in Photo 6.6

Observation: Origin is directly beneath the raceway surface



Part: Roller of a spherical roller bearing

Observation: Axial cracks occur on rolling surface

6.8

BEARING DAMAGE AND COUNTERMEASURES

DAMAGE CONDITION

Cage damage includes cage deformation, fracture and wear. Fracture of cage pillar. Deformation of side face. Wear of pocket surface. Wear of guide surface.

POSSIBLE CAUSE

- > Poor mounting (bearing misalignment)
- > Poor handling
- > Large moment load
- > Shock and large vibration
- > Excessive rotation speed, sudden acceleration and deceleration
- > Poor lubrication
- > Temperature rise

COUNTERMEASURE

- > Check the mounting method
- > Check the temperature, rotation, and load conditions
- > Reduce the vibration
- > Select a different cage type
- > Select a different lubrication method and lubricant



Part: Cage of a deep groove ball bearing

Observation: Fracture of pressed-steel cage-pocket



Part: Cage of an angular contact ball bearing

Observation:

Pocket pillar fractures from a cast iron machined cage

Cause:

7.1

Abnormal load action on cage due to misaligned mounting between inner and outer rings



Part: Cage of an angular contact ball bearing

Observation:

Fracture of machined high-tension brass cage





Part: Cage of a tapered roller bearing

Observation: Pillar fractures of pressed-steel cage



Part: Cage of an angular contact ball bearing

Observation: Pressed-steel cage deformation

Cause: Shock load due to poor handling



Part: Cage of a cylindrical roller bearing

Observation: Deformation of the side face of a machined high-tension brass cage

Cause: Large shock during mounting

7.4

7.7





Part: Cage of a cylindrical roller bearing

Observation: Deformation and wear of a machined high-tension brass cage



Part: Cage of an angular contact ball bearing

Observation:

Stepped wear on the outside surface and pocket surface of a machined high-tension brass cage

BEARING DAMAGE AND COUNTERMEASURES

DAMAGE CONDITION

When debris such as small metallic particles are caught in the rolling contact zone, denting occurs on the raceway surface or rolling element surface. Denting can occur at the rolling element pitch interval if there is a shock during the mounting (brinell dents).

POSSIBLE CAUSE

- > Debris such as metallic particles is caught between surfaces with relative motion
- > Excessive load
- > Shock during transport or mounting

COUNTERMEASURE

- > Wash the housing
- > Improve the sealing mechanism
- > Filter the lubrication oil
- > Improve the mounting and handling methods



Part: Outer ring of a double-row tapered roller bearing

Observation: Indentations on raceway surface

Cause:

Debris caught between rolling element and raceway



Part: Inner ring of a tapered roller bearing

Observation:

8.1

Small and large indentations occur over entire raceway surface

Cause: Debris caught between rolling element and raceway



Part: Tapered rollers of Photo 8.2

Observation: Small and large indentations occur over the rolling surface

Cause:

Debris caught between rolling element and raceway



DAMAGE CONDITION

The pitted surface has a dull luster which appears on the rolling element surface or raceway surface.

POSSIBLE CAUSE

- > Debris becomes caught in the lubricant
- > Exposure to moisture in the atmosphere
- > Poor lubrication

COUNTERMEASURE

- > Improve the sealing mechanism
- > Filter the lubrication oil thoroughly
- > Use a proper lubricant



Part: Outer ring of a slewing bearing

Observation: Pitting occurs on the raceway surface

Cause: Rust at bottoms of indentations



Part: Ball of Photo 9.1

Observation: Pitting occurs on the rolling element surface

9.1

BEARING DAMAGE AND COUNTERMEASURES

DAMAGE CONDITION

Wear is surface deterioration due to sliding friction at the surface of the raceway, rolling elements, roller end faces, rib face, and cage pockets.

POSSIBLE CAUSE

- > Entry of debris
- > Progression from rust and electrical erosion
- > Poor lubrication
- > Sliding due to irregular motion of rolling elements

COUNTERMEASURE

- > Improve the sealing mechanism
- > Clean the housing
- > Filter the lubrication oil thoroughly
- > Check the lubricant and lubrication method
- > Prevent misalignment



Part:

Outer ring of a spherical roller bearing

Observation:

Wear having a wavy or concave and convex texture on loaded side of raceway surface

Cause:

Entry of debris under repeated vibration while stationary



Part: Inner ring of a double-row tapered roller bearing

Observation: Fretting wear of raceway and stepped wear on the rib face

Cause:

10.1

Fretting progression due to excessive load while stationary



Part: Tapered rollers of Photo 10.2

Observation: Stepped wear on the roller head and face

Cause: Fretting progression due to excessive load while stationary

BEARING DAMAGE AND COUNTERMEASURES



DAMAGE CONDITION

Wear occurs due to repeated sliding between the two surfaces. Fretting occurs at fitting surface and also at contact area between raceway ring and rolling elements. Fretting corrosion is another term used to describe the reddish brown or black worn particles.

POSSIBLE CAUSE

- > Poor lubrication
- > Vibration with a small amplitude
- > Insufficient interference

COUNTERMEASURE

- > Use a proper lubricant
- > Apply a preload
- > Check the interference fit
- > Apply a film of lubricant to the fitting surface



Part: Inner ring of a deep groove ball bearing

Observation: Fretting occurs on the bore surface

Cause: Vibration



Part: Inner ring of an angular contact ball bearing

Observation:

11.1

Notable fretting occurs over entire circumference of bore surface

Cause: Insufficient interference fit



Part: Outer ring of a double-row cylindrical roller bearing

Observation: Fretting occurs on the raceway surface at roller pitch intervals

11.2

BEARING DAMAGE AND COUNTERMEASURES FALSE BRINELLING

DAMAGE CONDITION

Among the different types of fretting, false brinelling is the occurrence of hollow spots that resemble brinell dents, and are due to wear caused by vibration and swaying at the contact points between the rolling elements and raceway.

POSSIBLE CAUSE

- Oscillation and vibration of a stationary bearing during such times as transporting
- > Oscillating motion with a small amplitude
- › Poor lubrications

COUNTERMEASURE

- > Secure the shaft and housing during transporting
- > Transport with the inner and outer rings packed separately
- > Reduce the vibration by preloading
- > Use a proper lubricant



Part: Inner ring of a deep groove ball bearing

Observation: False brinelling occurs on the raceway

Cause: Vibration from an external source while stationary

12.1



Part: Outer ring of Photo 12.1

Observation: False brinelling occurs on the raceway

Cause: Vibration from an external source while stationary



Part: Rollers of a cylindrical roller bearing

Observation: False brinelling occurs on rolling surface

Cause: Vibration from an external source while stationary



DAMAGE CONDITION

Creep is the phenomenon in bearings where relative slipping occurs at the fitting surfaces and thereby creates a clearance at the fitting surface. Creep causes a shiny appearance, occasionally with scoring or wear.

POSSIBLE CAUSE

- > Insufficient interference or loose fit
- Insufficient sleeve tightening

COUNTERMEASURE

- > Check the interference, and prevent rotation
- > Correct the sleeve tightening
- > Study the shaft and housing precision
- > Preload in the axial direction
- > Tighten the raceway ring side face
- > Apply adhesive to the fitting surface
- > Apply a film of lubricant to the fitting surface



Part: Inner ring of a spherical roller bearing

Observation: Creep accompanied by scoring of bore surface

Cause: Insufficient interference



Part: Outer ring of a spherical roller bearing

Observation: Creep occurs over entire circumference of outside surface

Cause: Loose fit between outer ring and housing

BEARING DAMAGE AND COUNTERMEASURES

DAMAGE CONDITION

When sudden overheating occurs during rotation, the bearing becomes discolored. Next, raceway rings, rolling elements, and cage will soften, melt and deform as damage accumulates.

POSSIBLE CAUSE

- > Poor lubrication
- > Excessive load (excessive preload)
- > Excessive rotational speed
- > Excessively small internal clearance
- > Entry of water and debris
- > Poor precision of shaft and housing, excessive shaft bending

COUNTERMEASURE

- > Study the lubricant and lubrication method
- > Reinvestigate the suitability of the bearing type selected
- > Study the preload, bearing clearance, and fitting
- > Improve the sealing mechanism
- > Check the precision of the shaft and housing
- > Improve the mounting method



Part: Inner ring of a spherical roller bearing

Observation:

Raceway is discolored and melted. Worn particles from the cage were rolled and attached to the raceway

Cause: Insufficient lubrication



Part: Convex rollers of Photo 14.1

Observation:

Discoloration and melting of roller rolling surface, adhesion of worn particles from cage

Cause:

Insufficient lubrication





Part:

Inner ring of an angular contact ball bearing

Observation:

Raceway discoloration, melting occurs at ball pitch intervals

Cause: Excessive preload



Part: Outer ring in Photo 14.3

Observation: Raceway discoloration, melting occurs at ball pitch intervals

Cause: Excessive preload

14.3

14.4



Part: Balls and cage of Photo 14.3

Observation: Cage is damaged by melting, balls become discolored and melted

Cause: Excessive preload

BEARING DAMAGE AND COUNTERMEASURES ELECTRICAL EROSION

DAMAGE CONDITION

When electric current passes through a bearing, arcing and burning occur through the thin oil film at points of contact between the race and rolling elements. The points of contact are melted locally to form "fluting" or groove-like corrugations which are seen by the naked eye. The magnification of these grooves will reveal crater-like depressions which indicate melting by arcing.

POSSIBLE CAUSE

- > Electrical potential difference between inner and outer rings
- Electrical potential difference of a high frequency that is generated by instruments or substrates when used near a bearing

COUNTERMEASURE

- Design electric circuits which prevent current flow through the bearings
- > Insulation of the bearing



Part: Inner ring of a tapered roller bearing

Observation: Striped pattern of erosion occurs on the raceway surface



Part: Tapered rollers in Photo 15.1

Observation: Striped pattern of erosion occurs on the rolling surface





Part:

Inner ring of a cylindrical roller bearing

Observation:





Part: Balls of a groove ball bearing

Observation: Electrical erosion has a dark color that covers the entire ball surface



Part: Inner ring of a deep groove ball bearing

Observation: Fluting occurs on the raceway surface (high frequency)

15.4

15.5



Part: Outer ring of a deep groove ball bearing

Observation: Fluting occurs on the raceway surface (high frequency)

BEARING DAMAGE AND COUNTERMEASURES RUST AND CORROSION

DAMAGE CONDITION

Bearing rust and corrosion are pits on the surface of rings and rolling elements and may occur at the rolling element pitch on the rings or over the entire bearing surfaces.

POSSIBLE CAUSE

- > Entry of corrosive gas or water
- > Improper lubricant
- Formation of water droplets due to condensation of moisture
- > High temperature and high humidity while stationary
- > Poor rust preventive treatment during transporting
- Improper storage conditions
- > Improper handling

COUNTERMEASURE

- > Improve the sealing mechanism
- > Study the lubrication method
- > Anti-rust treatment for periods of non-running
- > Improve the storage methods
- > Improve the handling method



Part: Outer ring of a cylindrical roller bearing

Observation: Rust on the rib face and raceway surface

Cause: Poor lubrication due to water entry



Part: Inner ring of a spherical roller bearing

Observation: Rust on raceway surface at roller pitch

Cause: Entry of water into lubricant

16.1



Part: Rollers of a spherical roller bearing

Observation: Pit-shaped rust on rolling contact surface; corroded portions

Cause: Moisture condensation during storage

BEARING DAMAGE AND COUNTERMEASURES MOUNTING FLAWS



DAMAGE CONDITION

Straight line scratches on surface of raceways or rolling elements caused during mounting or dismounting of bearing.

POSSIBLE CAUSE

- Inclination of inner and outer rings during mounting or dismounting
- > Shock load during mounting or dismounting

COUNTERMEASURE

- > Use appropriate jig and tool
- > Avoid a shock load by use of a press machine
- > Center the relative mating parts during mounting



Part: Inner ring of a cylindrical roller bearing

Observation: Axial scratches on raceway surface

Cause: Inclination of inner and outer rings during mounting

17.1



Part: Outer ring of a double-row cylindrical roller bearing

Observation: Axial scratches at roller pitch intervals on raceway surface

Cause: Inclination of inner and outer rings during mounting



Part: Rollers of a cylindrical roller bearing

Observation: Axial scratches on rolling surface

Cause: Inclination of inner and outer rings during mounting

17.2

BEARING DAMAGE AND COUNTERMEASURES DISCOLORATION

DAMAGE CONDITION

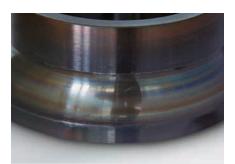
Discoloration of cage, rolling elements, and raceway ring occurs due to a reaction with lubricant and high temperature.

POSSIBLE CAUSE

- > Poor lubrication
- > Oil stain due to a reaction with lubricant
- > High temperature

COUNTERMEASURE

> Improve the lubrication method



Part: Inner ring of an angular contact ball bearing

Observation:

Bluish or purplish discoloration on raceway surface

Cause:

Heat generation due to poor lubrication



Part: Inner ring of an angular contact ball bearing

Observation:

18.1

Bluish or purplish discoloration on raceway surface

Cause: Heat generation due to poor lubrication

DAMAGE DIAGNOSTIC CHART



	LOCATION (PHENOMENON)	CAUSE													
		Handling		Bearing surrounding		Lubrication		Load			Speed				
DAMAGE NAME		Stock • Shipping	Mounting	Shaft Housing	Sealed device Water • Debris	Temperature	Lubricant	Lubrication method	Excessive load Impact load	Moment	Ultra small load	High speed, High acceleration & deceleration	Shaking • Vibration Stationary	Bearing Selection	REMARKS
1. Flaking (or Spalling)	Raceway, Rolling surface		٠	٠	•		٠	٠	٠	٠				٠	
	Raceway, Rolling surface		•	•	•		•	•	•	•		•			
2. Scoring	Bearing outside surface (Rolling contact)		٠		•		•	٠							
	Roller end face surface, Rib surface				•		•	٠			٠	•			
3. Peeling	Cage guide surface, Pocket surface			•*	•		•	٠							* Mating rolling part
4. Fracture	Raceway, Rolling surface	•	•	•					•	•					
5. Smearing	Raceway collar, Rollers				•		•	٠			٠	•			
6. Cracks	Raceway rings, Rolling elements		•	•		٠			•	•					
0. clacks	Rib surface, Roller end face, Cage guide surface (Thermal crack)			٠				٠	•	•					
7. Cage damage	Deformation, Fracture		•	٠					•	•					
	Wear		•		•		•	٠	•	•		٠			
8. Denting	Raceway, Rolling surface, (Innumerable small dents)				•			•							
	Raceway (Dents on the rolling element pitch)	•	•						•				•		
9. Pitting	Raceway, Rolling surface				٠		٠	٠							
10. Wear	Raceway, Rolling surface, Rib surface, Roller end face		•		•		•	•							
11. Fretting	Raceway, Rolling surface	•	•	٠			٠	٠	•			•	•		
Th. freeding	Bearing outside & bore, side surface (Contact with housing and shaft)		٠	٠					•						
12. False brinelling	Raceway, Rolling surface	•					•	٠					•		
13. Сгеер	Fitting surface		٠	٠		٠	•*	•*	•			•			* Clearance fit
14. Seizure	Raceway ring, Rolling element, Cage		٠	٠	•		•	٠	•	•		•		٠	
15. Electrical erosion	Raceway, Rolling surface		•*	•*											* Electricity passing through the rolling element
16. Rust and corrosion	Raceway ring, Rolling element, Cage	•	٠		•	٠	•	٠							
17. Mounting flaws	Raceway, Rolling surface		٠	٠											
18. Discoloration	Raceway ring, Rolling element, Cage					٠	٠	٠							



1



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SECTION F:

MAINTENANCE TOOLS / TECHNICAL SUPPORT

MAINTENANCE TOOLS	F3
TECHNICAL SUPPORT	F4
ENGINEERING SUPPORT	F4
NSK AMERICAS TECHNICAL CENTER	F4
TECHNICAL ON-SITE SUPPORT	F5
TECHNICAL ON-LINE SUPPORT	F5
TRAINING PROGRAMS	F6

MAINTENANCE TOOLS

The cause of premature bearing failure can often be diagnosed as a result incorrect handling and installation. Since rolling bearings are high precision machine parts, they must be handled accordingly. Their expected performance cannot be achieved if they are not handled properly. A simple precaution to observe is the consistent use of proper tools and equipment when handling bearings, avoiding the use of generalpurpose tools.

NSK offers a wide range of mechanical and alignment tools to assist with proper bearing handling and installation, including:

Mechanical Tools for Handling, Mounting and Dismounting

- > Induction heaters
- Pullers and pushers
- > Bearing lifting tools
- > Press plates
- > Fitting tools
- > Hydraulic nuts
- > Sine bars

Alignment Tools

- > Laser shaft alignment tool
- > Laser belt alignment tool

In addition to offering the tools and equipment, NSK will provide an on-site demonstration of appropriate use of the equipment.











TECHNICAL SUPPORT

ENGINEERING SUPPORT

Proper bearing selection can have a major impact on our customers' entire business, helping to achieve improvements in machine reliability, productivity and performance, all of which carry a tangible and measurable cost benefit. Identifying optimal solutions is an expertise of NSK's application engineers, who work hand in hand with our customers from the original machine design stage to the resolution of performance issues.

With a foundation of industry, machine, and operating condition experience, NSK application engineers support our customers with a range of services including:

- › Application reviews
- Machine design support
- > OEM part conversion
- Diagnostics
- Bearing condition analysis
- Failed bearing analysis
- › Lubrication analysis

Our engagement with our customers doesn't end with a report of our findings or recommended solutions. We monitor performance to ensure anticipated results and utmost performance are being delivered.

AMERICAS TECHNICAL CENTER

NSK's global network of research centers are linked together in our focus on the development of new technologies, and the continuous optimization of quality of NSK products. At the core of our research activities is the development of advanced material and lubricant technologies, simulation applications using a variety of analytical systems, and technological innovation in the field of mechatronics. At the heart of our work is absolute customer satisfaction with, and benefit from, NSK products.



The NSK Americas Technical Center, located in Ann Arbor MI, utilizes a variety of analytical systems and technological innovation to conduct considerable research, testing and analysis including:

- > Bearing test lab for fatigue life, seal testing, environmental simulation testing, as well as design and product verification
- > Visual analysis of failure and fracture using digital photography and measurement
- Metrology using dimensional, coordinate and form measurements
- Chemical analysis using scanning electron microscope, compound analysis and particle counting
- Metallurgical evaluation of the microstructure and macrostructure, as well as hardness measurements, case depth measurements, heat treatment verification, fractography and steel cleanliness evaluation
- Noise and vibration assessments using internally developed software and equipment, in addition to advanced analysis tools such as Fast Fourier Transform (FFT), enveloping, and bearing fault frequencies

TECHNICAL SUPPORT

TECHNICAL ON-SITE SUPPORT

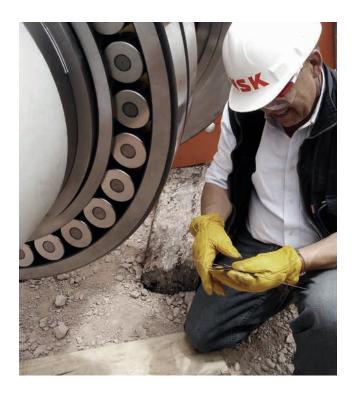
Improvement is a journey without an end destination. It never stops. And we never stop looking for better ways of supporting our customers in a comprehensive, collaborative, and continuous way. The focus of NSK industry specialists isn't simply on a quick-fix and immediate gain – it's about incremental and sustainable improvement to deliver longterm benefits.

When NSK is on-site, we're there to understand our customers' challenges and identify problems leading to frequent bearing replacement, breakdowns caused by poor specification, high energy costs from inefficient product selection and lost production because of downtime. We use our learning, knowledge and experience to collaborate with our customers to implement improvements that deliver measurable value in terms of performance, productivity and maintenance cost efficiency.

Our collaboration with customers is holistic, with a range of services and support that includes:

- › Process mapping
- > Inventory / critical spares management
- > Bearing installation and removal
- Scheduled maintenance programs
- Inspection and diagnostics
- > Best maintenance practice training

With NSK on-site support, our customers take a critical step forward in realizing improvements in equipment, productivity, people and financial performance.



TECHNICAL ON-LINE SUPPORT

For the technically self-sufficient and independent problemsolver, NSK offers extensive on-line resources to facilitate design, selection and troubleshooting including:

- Bearing selection catalog (including app)
- > CAD file download
- > Bearing calculation tools (including app)
 - > bearing life
 - > fits and clearances
 - > frequencies
 - > lubrication viscosities and intervals
- > frictional moment and speeds
- Troubleshooting (Bearing Doctor) app
- > NSK Verify app for machine tool bearings

Visit nskamericas.com.

TRAINING



TRAINING PROGRAMS

NSK offers a range of training opportunities designed to expand on the knowledge required in daily work and to contribute to optimizing NSK bearing performance, as well as machinery and equipment performance. Our programs include a large variety of well-proven courses that focus on the major learning needs of those involved in specifying, ordering and installing and maintaining bearings. Our instructors are application engineers, industry specialists and service engineers with vast technical expertise and an understanding of specific industry sector demands. The combination of theoretical and practical training ensures successful learning outcomes for our customers.

Training opportunities available from NSK range from the regular recurring **Bearing Boot Camp** programs held at our NSK Americas headquarters to customizable on-site training to our web-based **NSK Academy.**

> Bearing Boot Camp

is held each spring and fall at NSK Americas headquarters in Ann Arbor, MI. Basic and advanced programs are offered.

Bearing Basics - offers an introduction to bearing types, design features, performance characteristics and nomenclature. Effectively using available resources such as online bearing selection, calculation and lubrication tools is also included.

Advanced Class - is tailored to individuals working in a decidedly hands-on capacity with rolling bearings and includes an understanding of parameters for calculating bearing selection, shaft and housing fits, and lubrication fill and replenishment.

> On-Site Training

is typically defined by and designed to meet the needs of customers. The training is tailored specifically to the applications and products unique to their industry, and will typically include relevant:

- > Bearing types, design features, performance characteristics and nomenclature
- > Examples of bearing applications and mounted bearing arrangements
- > Bearing selection, lubrication, fits and calculations
- > Hands-on interaction with bearing installation demos and appropriate mechanical tools

> NSK Academy

is available on-line with a wide range of technical tutorials to introduce the user to basic bearing types, their design features and their performance characteristics as they relate to friction, torque, loads and other acting forces. Additional modules for bearing handling, troubleshooting and use of maintenance tools are also available.

Visit nskacademy.com.



IMPROVEMENT PAYS

END-TO-END SERVICE DELIVERS CUSTOMER SUCCESS

Improvement never ends. And we never stop looking for better ways to support our customers in a complete, collaborative and continuous way. The focus of NSK isn't simply on a quick fix for immediate gain – it's about incremental and sustainable improvement to deliver long-term benefits.

When NSK is on-site, we're there to understand our customers' challenges and identify problems contributing to frequent bearing replacement, breakdowns caused by poor specification, high energy costs from inefficient product selection and lost production because of downtime. We collaborate with our customers to institute an **Asset Improvement Program (AIP)** that encompasses process and maintenance management, diagnostic and educational support to deliver measurable gains in output and cost-efficiency.

With NSK, our customers embark on a critical path to realizing improvements in equipment, productivity, people and financial performance.





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